# Laser Geodynamic Satellite Thermal/Optical/Vibrational Analyses and Testing

# **Final Report**

Volume II
Technical Report

### Book 3

(NASA-CR-120565) LASER GEODYNAMIC N75-13905 SATELLITE/THERMAL/OPTICAL VIBRATIONAL ANALYSES AND TESTING. VOLUME 2: TECHNICAL REPORT, BOOK 3 Final Report Unclas (Bendix Corp.) 325 p HC \$9.25 CSCL 22B G3/15 05050

> DR No. MA-04 DPD No. 296

Contract NAS 8-30658

October 1974

Prepared for:

George C. Marshall Space Flight Center National Aeronautics and Space Administration Marshall Space Flight Center, Alabama 35812





Ann Arbor, Michigan

# Laser Geodynamic Satellite Thermal/Optical/Vibrational Analyses and Testing

## **Final Report**

Volume II
Technical Report

Book 3

DR No. MA-04
DPD No. 296
Contract NAS 8-30658

October 1974

Prepared for:

George C. Marshall Space Flight Center National Aeronautics and Space Administration Marshall Space Flight Center, Alabama 35812



Ann Arbor, Michigan

## **VOLUME II**

## BOOK 3

This Book 3 of Volume II contains Appendices R, S, T, U and V.

# LAGEOS Phase B Thermal/Optical Vibration Analysis and Test Program

- Test Plan -

## TABLE OF CONTENTS

				Page
1.0	INTRODUCTION :			1
2.0	SCOPE AND OBJECTIVES			2
2. 1	SCOPE			2
2. 2	OBJECTIVES			2
3.0	TEST PROGRAM DESCRIPTION			2
3.1	THERMAL/OPTICAL TESTS			3
3.2	VIBRATION TESTS	,	t t	9
4.0	TEST PROCEDURES			11
5.0	TEST PROGRAM SCHEDULES		:	

#### ILLUSTRATIONS

Figure		Page
3 - 1	Panel, Test Article LAGEOS	14
3-2	Assembly, Test Article LAGEOS	' 15
3 - 3	LAGEOS Test Set-Up-Thermal/Vacuum	16
3 - 4	Thermocouple Fixture, LAGEOS (Dwg. 2374466)	17
3-5	Installation, Thermocouple Fixture (Dwg. 2374459)	18
3-6	Thermal/Optical Test Fixture (Dwg. 2374460) (Sheet I of 3))	19
3-7	Thermal/Optical Test Fixture (Dwg. 2374460 (Sheet 2 of 3))	20
3-8	Thermal/Optical Test Fixture (Dwg. 2374460 (Sheet 3 of 3))	21
3-9	Laser Window Feedthrough (Dwg. 2374453)	22
3-10	Laser Field Angles and Retro. Orientation	23
3-11	Far-Field Diffraction Instrument Schematic	24
3-12	Laser Leveling Plate, LAGEOS TV Test (Dwg. 2374454)	<b>2</b> 5
3-13	Vibration Test Fixture	26
5-1	Thermal/Optical/Vibration Analysis & Test Program	27
5-2	Test Plan and Test Procedures	28
5 - 3	Test Article Design/Fabrication/Test	29
5-4	Far-Field Diffraction Instrument & Optical Window Schedules - Zygo Corporation	30
5-5	Test Fixtures - Design/Fabrication/Checkout	31
5-6	Test Equipment Need Schedule - Thermal/Optical	32
· ·	Vibration Tests	
	TABLES	
	11211111111111111111111111111111111111	
Table		·•
3-1	Test Conditions - Thermal/Optical Tests	12
3-2	LAGEOS Worst-Case Dynamic Test Environment	13

#### 1.0 INTRODUCTION

The Bendix LAGEOS Phase B Program is a 6-month effort devoted to Laser Geodynamic Satellite (LAGEOS) thermal/optical/vibrational analyses and testing. The purpose of this effort is to verify, through analysis and test, that the MSFC-defined design of the LAGEOS inherently provides a retro-reflector thermal environment which maintains acceptable retroreflector internal thermal gradients.

The specific study objectives are as follows:

- . Develop a LAGEOS thermal model and conduct thermal analysis, using this model, to predict retroreflector thermal behavior.
- . Procure and fabricate test hardware required to simulate the LAGEOS design for the purpose of conducting environmental tests.
- . Accomplish thermal, optical, and mechanical vibration tests to verify that the thermal model and thermal analysis predictions are representative of actual satellite performance.

This plan describes the test program which is intended to provide test results which will contribute to meeting these study objectives.

This updated version of the test plan reflects the decisions made at the First Program Review (17-18 April 1974) to select the circular-faced retroreflector configuration and to delete the Early Vibration and Early Thermal/Optical Tests and expand the Final Thermal/Optical tests. In addition, the plan update includes incorporation of MSFC-recommended test conditions and the changes in the test fixtures which are required to implement these test conditions.

#### 2.0 SCOPE AND OBJECTIVES

This section describes the scope and objectives of this test plan.

#### 2.1 SCOPE

This document establishes the overall plan for the Bendix LAGEOS Phase B Thermal/Optical/Vibration test program. The plan describes the objectives, methods, and conditions for each test and identifies the test article, test fixtures, test equipment and expendables, instrumentation and data to be employed. Schedules for the overall program; test procedures and tests; design, fab and assembly of the test articles and test fixtures; and the need dates for test equipment and expendables are also included.

#### 2.2 OBJECTIVES

The objectives of this plan are to describe the overall plan for accomplishing the various tests required to achieve the program objectives and tasks of the Bendix LAGEOS Phase B Program, as defined in the revised Study Plan, LAGEOS-8, (Rev. B), dated 6-28-74. The requirements for each test are identified for the purpose of program review (to ensure that program objectives are to be met), for the design and fabrication of the required test article and test fixtures, for the allocation of test facilities, equipment and expendables and for the generation of the detail test procedures by which the specified data will be obtained at specified test conditions. The plan includes the current detailed Bendix internal test program schedules, by which the various individual preparatory subtasks are to be accomplished to ensure that the individual tests will be conducted within the time period required to meet Phase B program objectives.

#### 3.0 TEST PROGRAM DESCRIPTION

The Bendix LAGEOS Phase B test program consists of thermal/optical tests, a vibration test, and post-vibration thermal/optical tests.

#### 3.1 THERMAL/OPTICAL TESTS

#### 3.1.1 Test Objectives

The objective of these tests is to obtain optical performance data for the LAGEOS retroreflector under isothermal conditions and for various thermal gradients, including predicted orbital worst-case thermal gradients. Optical performance data will be obtained for various laser field angles and retro-reflector orientations. Optical performance data will be obtained prior to, and after, subjecting the test article to the LAGEOS worst-case dynamic environments.

#### 3.1.2 Test Article

The LAGEOS test article will be utilized to support the LAGEOS retroreflectors under conditions which simulate those of the LAGEOS satellite. The configuration of the Test Article panel, in which the retroreflector is to be mounted, is shown in Figure 3-1; the configuration of the total Test Article assembly, with the retroreflectors in place, is shown in the assembly drawing, Figure 3-2.

The criteria for the design of the test article are as follows:

- a. Provide the test conditions necessary to simulate the factors which affect the retroreflector thermal/optical performance, when installed in the LAGEOS satellite. The following factors are represented in the test article or the test conditions to correspond directly to those presently defined for the satellite:
  - 1. Retroreflector mount design
  - 2. Cavity design
  - 3. Retroreflector recession (lmm)
  - 4. Retroreflector design
  - 5. Mount retainer ring surface finish (machined aluminum)

- 6. Cavity inside surface finish (machined aluminum,  $\epsilon = 05$ )
- 7. Solar heating of the retroreflector and mount
- 8. Earth IR heating of the retroreflector and mount.

Since the effects of the satellite spherical shape, cavity pattern and outside surface finish can be represented directly only by providing the total spherical satellite (with a retroreflector in each cavity), the net effect of these factors, as determined by analysis, is provided in terms of the cavity core (test article structure) temperature level.

- b. Provide mounting for 6 LAGEOS retroreflectors procured for this test program. The retroreflector configuration selected for LAGEOS is the circular-faced tab-mounted configuration.
- c. Provide a cavity pattern which locates the retroreflectors in two (2) rows of three (3) each. This permits the sequential alignment of the three retroreflectors in the laser beam by the thermal/optical test fixture (i. e., linear motion along the axis of rotation for each test set-up) and provides an acceptable target for the solar simulation lamp. The arrangement also provides close proximity of the six test retroreflectors to a pair of ALSEP retroreflectors instrumented with thermocouples and mounted on the test fixture. The arrangement also results in a reasonably-sized test article which does not impose difficult design requirements on the test fixture used to support the test article in the thermal/vacuum chamber.
- d. Provide cavity spacing of .060 minimum to simulate the minimum cavity spacing on the satellite.
- e. Provide sufficient tie-down bolt holes to ensure no relative motion of the test article during dynamic tests, with respect to the vibration test fixture. This is to ensure that the intended LAGEOS dynamic environment is imposed on the retroreflector/mount assemblies.

- f. Fabricate the test article from the same type of material as selected by MSFC for the satellite. The satellite outside surface coating characteristics are represented by the test article structure temperature and thus no coating is required on the test article outside surface.
- g. The overall dimensions of the test article panel were determined early in the program to support test fixture design and Early Test Article design (now deleted). At the time, the configuration of the LAGEOS retroreflector had not been selected and both the circular-faced (ALSEP-type) and hexagonal-faced (GEOS-type) configurations were being considered. The front face dimensions are based on the cavity diameter required for the circular-faced retroreflector, an assumed maximum cavity spacing and tie-down considerations. The test article height is based on requirements for the hex-faced retroreflector mount and maximum recessing of 1 cm.
- h. Provide threaded holes in the cavities for orientation of the retroreflectors as shown in Table 3-1 for each test condition. It is planned to provide two sets of threaded holes in two of the cavities and to change retroreflector orientation as shown in Figure 3-2.

#### 3.1.3 Test Method

The test arrangement for the thermal/optical tests is shown in Figure 3-3.

The LAGEOS Test Article is to be mounted in the Thermal/Optical Test Fixture for the Thermal/Optical Tests.

Thermal control of the test article is provided by a thermal control shroud on the test fixture, consisting of heat exchanger coils, a copper base-plate and a multilayer insulation blanket. A liquid heat transfer medium is pumped to the coils from the heat exchanger outside of the Vacuum Chamber. The Test Fixture will provide the means for controlling the LAGEOS Test Article angular orientation about the horizontal axis-of-rotation, which is in line with the front faces of the

retroreflectors, to vary the incident laser beam field angle. The Test Fixture will also provide the means for placing any one of the three retro-reflector cavity locations, on the rotational axis, in-line with the laser beam at the chamber center-line. Control of angular orientation and longitudinal location will be accomplished manually from outside the chamber. Each group of three retroreflectors is manually set-up on the rotational axes prior to their respective tests.

Thermal data is to be obtained by means of thermocouples mounted on the Test Article panel and on ALSEP retroreflectors and mounting hardware installed in a small panel (Figure 3-4) mounted on the test fixture, as shown in Figure 3-5. Thermocouples, utilizing #40 gage Chromel-constantan wire, will be mounted at the apex, front-face center and tab outer edge on each ALSEP retroreflector and on its mounting rings. Thermocouples, utilizing #30 gage Chromel-constantan wire, will be mounted on the front-face of the Test Article panel. Thermocouples will be bonded in place, utilizing Eastman 910 adhesive and on the retroreflectors will, in addition, be covered by a small patch of reflective mylar insulation to better simulate the non-instrumented retroreflectors. Thermal data will also be obtained at various locations on the vacuum chamber as shown in Figure 3-3.

A solar radiometer is to be mounted on the fixed arm of the thermal/optical test fixture to provide intensity data for the solar simulator beam at the test article. A separate radiometer is mounted on the fixture to provide intensity data for the IR simulator mounted at the laser end.

The Test Fixture will rotate the Test Article to face the solar simulator and the earth IR simulators. Solar incidence angles will be varied, by rotating the Test Article in the Test Fixture, to vary retroreflector absorbed heating and retroreflector temperature gradients. The Thermal/Optical Test Fixture design is shown in Figure 3-6 through 3-8.

In addition to the thermal control shroud, thermal conditions (i.e., temperature gradients) in the test retroreflectors are to be achieved by the combination of vacuum chamber cold-walls, simulated solar heating in the beam from a Generaco solar lamp outside the far end of the chamber and two earth-IR simulator lamps, one mounted at the laser end of the chamber and one mounted at the solar lamp end of the chamber.

An optical-quality window is required at the Far-Field Diffraction Instrument (FFDI) end of the vacuum chamber to permit the laser beam to be transmitted to the test article and the retro-reflected return beam to enter the FFDI. Requirements for this optical window, fabricated of BK-7 glass, are defined in Requirements Document LAG-2 and the window is being procured from Zygo Corporation. The optical window is installed in the vacuum chamber as part of the optical window assembly. Thermal control of the optical (laser) window is required to maintain the window BK-7 glass at isothermal conditions. A shield, designed to have an L/D of 4.0 and to include a heater, thermal control coating and aluminized mylar insulation, will provide the necessary thermal control. The resulting design is shown in Figure 3-9.

Test conditions for these tests are summarized in Table 3-1 and Figure 3-10. Test data and the means for obtaining this data at each test condition are described in Section 3. 1.4. Optical performance data is to be obtained for each LAGEOS retro-reflector. The ALSEP retroreflectors and mounting rings on the test fixture are to be instrumented to obtain temperature gradient data for correlation with the optical performance data. In addition, the laser polarization angle is to be controlled as specified in Table 3-1. The tests to be conducted after the vibration tests are identified in Table 3-1 and are limited to those required to identify any residual effects of the exposure to the LAGEOS worst-case dynamic environment.

The total number of test conditions has been expanded from those originally proposed, and from those identified in the initial issue of this test plan (and in the Program Review). These conditions reflect the changes described in the Study Plan (Rev. B), ECP Bx-LA-2, dated 6-28-74.

#### 3.1.4 Test Data and Instrumentation

Optical performance data will be obtained, at each test condition, using the Bendix Far-Field Diffraction Instrument (FFDI). Requirements for the FFDI are defined in Requirements Document LAG-2 and the FFDI is being fabricated by the Zygo Corporation. This instrument is depicted schematically in Figure 3-11 and is mounted on the leveling plate shown in Figure 3-12. It contains the necessary equipment for generating a

linearly-polarized laser beam and projecting the beam at the test article. It accepts the return beam from the test article and provides a visual display of the far-field diffraction pattern, provides a photograph of the pattern and provides a means of measuring the relative intensity of the return pattern, in a selected annular region. It also measures the relative intensity of the transmitted beam and provides a measure of the ratio of the return beam intensity to the transmitted beam intensity. The orientation of the linearly polarized beam may be controlled and a circularly-polarized beam may also be selected for transmission to the test article. The test data is then in three forms: (1) a visual display, (2) a Polaroid photograph and (3) relative intensity data, for each test condition in Table 3-1. Test article orientation, for laser field angles, is read directly from the Test Fixture.

Thermocouples will be mounted at the apex, the front-face center and the tab-outer edge of the ALSEP retroreflectors, on the mounting rings and on the Test Article, as described in 3.1.3 above. Thermocouples will be mounted at various locations on the vacuum chamber as shown in Figure 3-2.

A pair of solar radiometers mounted on the fixed arm of the Test Fixture will provide data on the intensity of the solar simulator beam and the IR lamp output at the Test Article.

#### 3.1.5 Test Fixtures, Equipment and Expendables

The requirements for these tests are summarized as follows:

- a. LAGEOS Thermal/Optical Test Fixture
- b. Optical Window and Shield Assembly
- c. Far-Field Diffraction Instrument (FFDI)
- d. FFDI Support Plate
- e. Support Table
- f. Thermocouples #40 gage and #30 gage (chromel-constantan wire)

- g. Thermal-Vacuum Chamber and control system
- h. Genarco Solar Simulators
- i. Hycal Radiometers
- j. Tenney Heat Exchanger
- k. Data Acquisition System
- 1. Optical Alignment Instrumentation
- m. Polaroid camera and film
- n. Earth IR simulator lamps
- o. Liquid N2
- p. Carbon Rods

#### 3.2 VIBRATION TESTS

#### 3.2.1 Test Objective

The objective of these tests is to subject the LAGEOS Test Article to the LAGEOS worst-case dynamic environment. The residual effects are to be identified by a comparison of optical performance, obtained before and after the Test Article has been subjected to the dynamic environment and by a visual inspection.

#### 3.2.2 Test Article

The LAGEOS Test Article will be utilized for these tests. The configuration is the same as described in Section 3.1.2 and Table 3-1.

#### 3.2.3 Test Method

The test article, as described in 3.1.2 above, will be mounted on the LAGEOS Vibration Test Fixture, tied-down by six 1/4-inch cap-head bolts. The Vibration Test Fixture has provisions for threaded holes

to accept these six tie-down bolts and additional 3/8 dia. through-holes for attaching the Vibration Fixture to the Bendix vibration test system shaker head and slip plate. The through-hole pattern is compatible with the existing threaded-hole patterns on the shaker head and slip plate. The Vibration Test Fixture is shown in Figure 3-13.

The test article, mounted on the vibration shaker head for the vertical axis and on the slip plate (driven by the shaker) for the lateral axes, shall be subjected to the sinusoidal and random vibration spectra as defined in Table 3-2.

#### 3. 2. 4 Test Data and Instrumentation

A control accelerometer will be mounted on the Test Article and oriented in the axis of the input vibration to monitor the input for control purposes.

The signal from the control accelerometer will be recorded and displayed in real-time on an x-y plotter. During sinusoidal excitation, the real-time plot will consist of an analog plot of input G-peak versus frequency. During the random excitation, the real-time plot will consist of an analog plot of a sampled scan of power spectral density (G<sup>2</sup>/H<sub>Z</sub>) versus frequency output from the ASDE-80 Equalizer/Analyzer. A T-RMS meter will be used to measure g-rms input.

A visual inspection will be made after each vibration exposure for each axis.

#### 3.2.5 Test Fixture, Equipment and Expendables

The requirements for these tests are summarized as follows:

- a. LAGEOS Vibration Test Fixture
- b. Bendix Vibration Test System
- c. Endevco accelerometer (1) (Model #2221)
- d. Polaroid camera and film.

#### 4.0 TEST PROCEDURES

Separate test procedures will be prepared for each of the two (2) tests described in Section 3.0. The test procedures will describe the test objectives; identify applicable documents, required participants, and required fixtures, equipment and instrumentation; and describe the procedure to be followed, including instrumentation locations, test conditions and data to be recorded.

A master copy of the procedure will be used during the test to record the equipment identification nomenclature, the accomplishment of each step of the procedure and additional notations to reflect how the test was actually run. This "as-run" procedure, together with the recorded data, will become a documented record of the test.

Test procedures shall be approved by cognizant LAGEOS program personnel, as defined by the LAGEOS Program Manager, prior to the start of tests. Test procedures will be released for record purposes. Variations to the test procedures may be made by, or with the approval of, the same cognizant LAGEOS program personnel. Back-up approval authority will be provided to minimize test delays while the tests are in-process.

#### 5.0 TEST PROGRAM SCHEDULES

This section includes the Bendix internal overall program schedule and detail schedules for the test plan and test procedures, the test article, the FFDI and optical window, the various special test fixtures and the test equipment and expendables need dates. These schedules are normally updated weekly and distributed separately to program personnel. Updated schedules will only be incorporated in this test plan at the time of updated plan issuance.

Table 3-1

# THERMAL/OPTICAL TEST CONDITIONS

Test	Description			Orientation 0	T	Vac Chamber Press (Torr)	Test Article Temperature	Chamber Cold Temperature	Solar Condition	Total Laser Field Angles (w) Per Test
. 1	Iso/Amb	0	90 0	)		Amb.	Amb.	Amb.	N/A	8++
2	Iso/Vacuum	0	90 60			1 x 10 <sup>-6</sup>	Amb.	Amb.	N/A	15***
3	Thermal/Vacuum	0	90 80			1 x 10 <sup>-6</sup>	+30°C	-185°C	No Sun (No IR)	
4	Thermal/Vacuum	0	90 80			1 x 10 <sup>-6</sup>	+30°C	-185°C	l Sun Normal (No IR)	ORIGINAL PAGE I
5	Thermal/Vacuum	0	90 80	•		1 x 10 <sup>-6</sup>	+30°C	-185 <sup>0</sup> C	1 Sun +50 <sup>0</sup> (No IR)	PAGE IS
6	Thermal/Vacuum	0	90 80			1 × 10 <sup>-6</sup>	+30°C	-185 <sup>0</sup> C	No Sun 1 Earth IR	. •: · · · · · · · · · · · · · · · · · ·
7	Thermal/Vacuum	0	90 80	<b>)</b>		1 x 10 <sup>-6</sup>	-30°C	-185°C	No Sun (No IR)	POOR
8	Thermal/Vacuum	0	90 80	•		1 x 10 -6	-30 <sup>°</sup> C	-185 <sup>0</sup> C	l Sun Normal (No IR)	
9	Thermal/Vacuum	0	90 80		: .	1 x 10 <sup>-6</sup>	-30°C	-185°C	No Sun l Earth IR	B**
10	Iso/Amb			60 40	20	Amb	Amb	Amb	N/A	400
11	Iso/Vacuum		•	60 40	20	1 x 10 <sup>-6</sup>	Amb	Amb	N/A	8.00
12	The rmal/Vacuum			60 40	20	1 x 10 <sup>-6</sup>	+30°C	-185°Ç	No Sun (No IR)	15***
VIBRAT	ION TEST			:				v.		
13	Iso/Vacuum	<u> </u>	. *	60 100	20	1.x.10 <sup>-6</sup>	Amb	Amb	N/A	8**
14	The smal/Vacuum			60 100	20	1 x 10 <sup>-6</sup>	+30 <sup>©</sup> C	-185°C	No Sun (No IR)	11****

Laser Polarization: Linear in Laser Field Angle Plane (Vertical Plane)

A, D: α = 0, +30, +15, -15, -30

\*\*\*A, B, C, D, E, F:

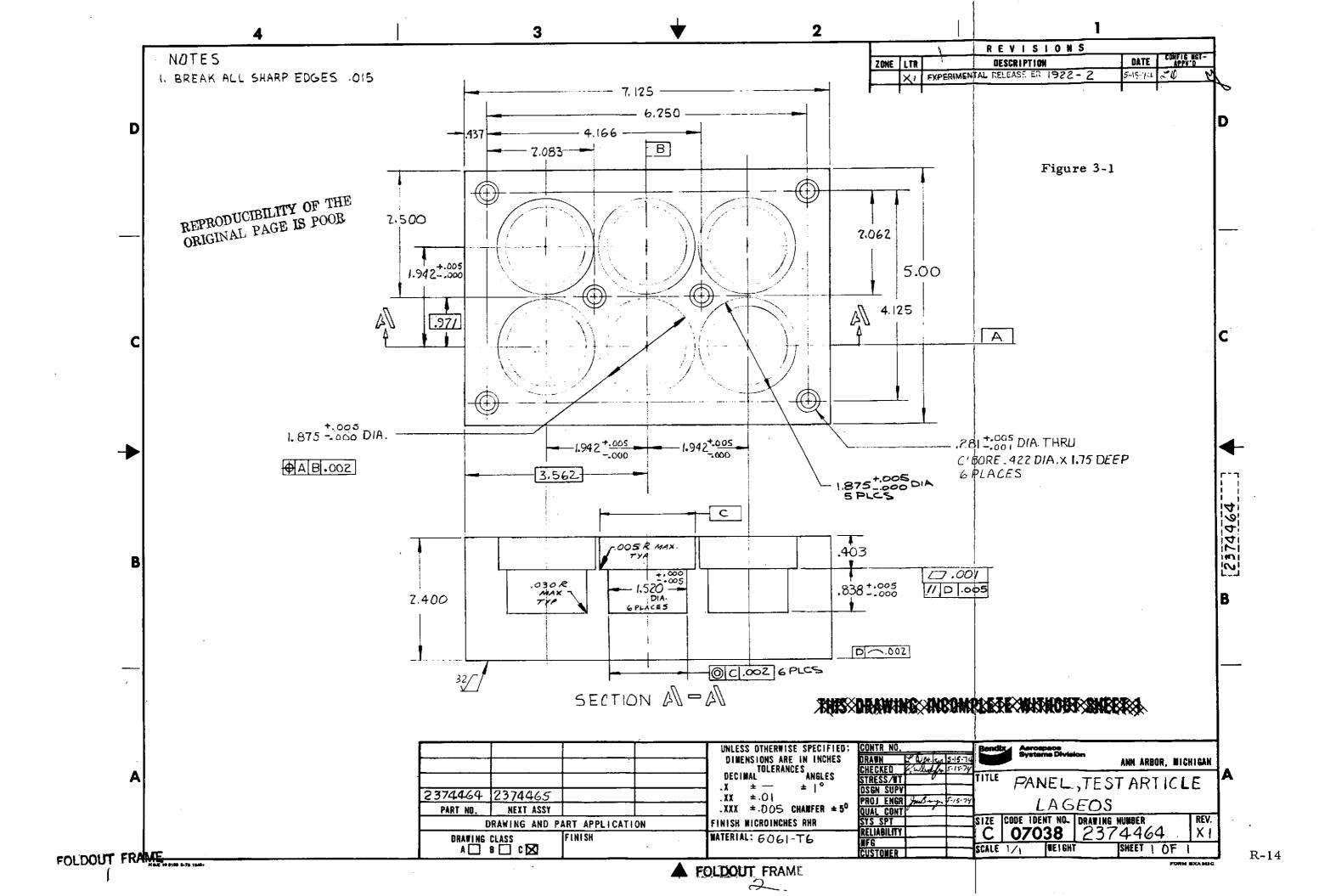
α = 0, +30, +15, -15, -30

B. E: a = 0, +15 C. F: a = 0

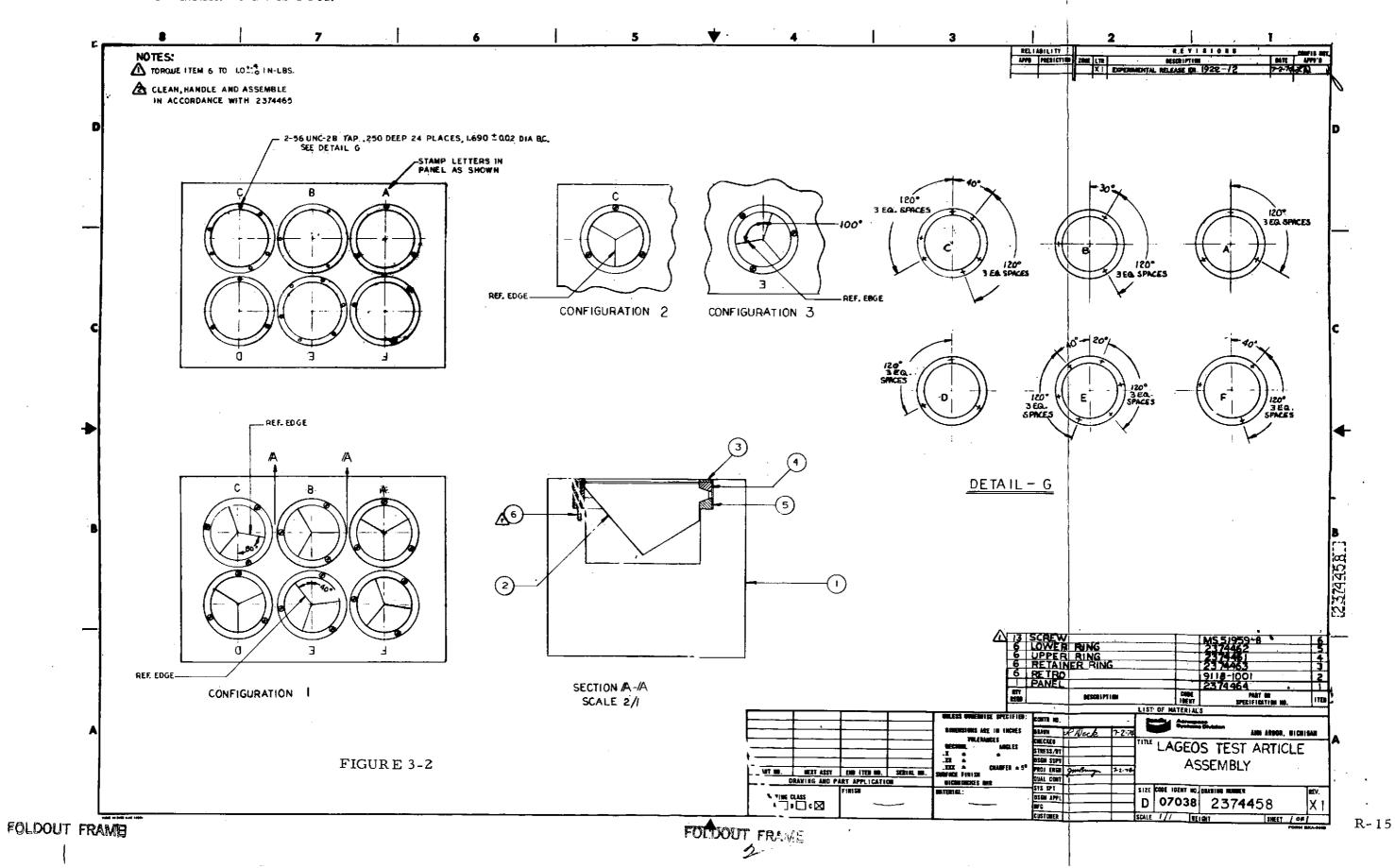
Table 3-2

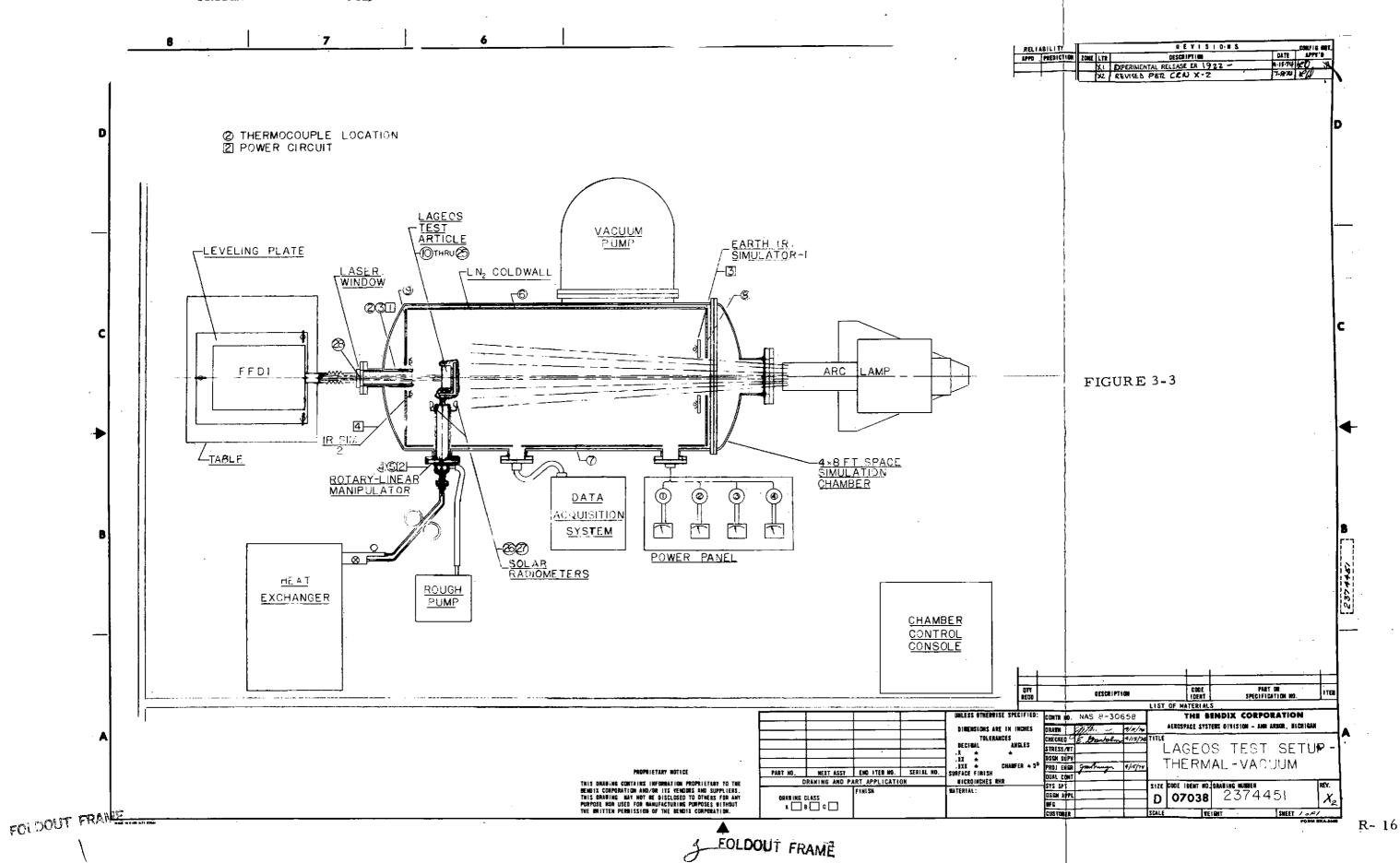
LAGEOS TEST PROGRAM WORST-CASE DYNAMIC ENVIRONMENT

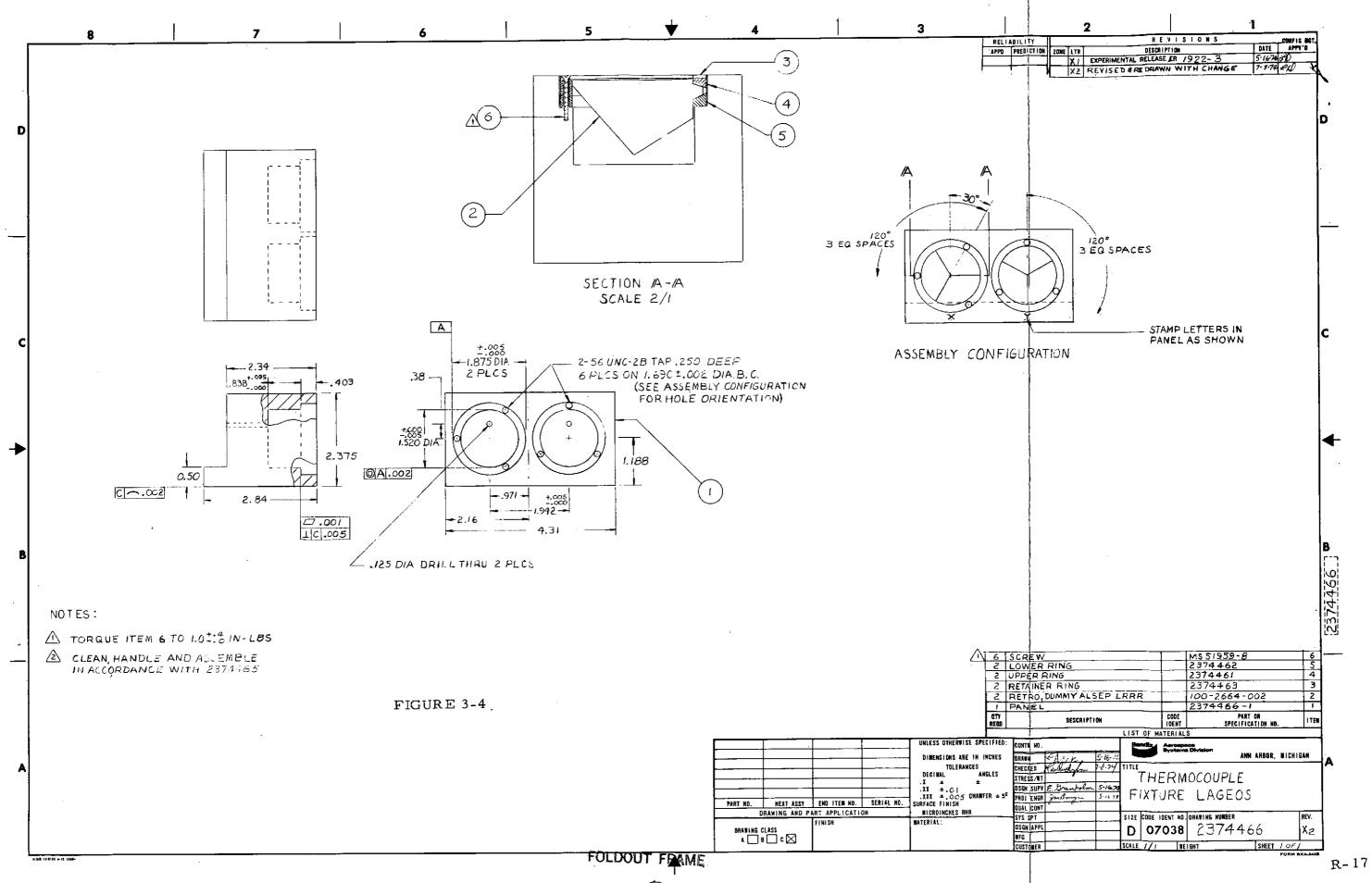
Sinusoidal	Vibration	(2 Oct/Min)	(Three Axes - One Sweep per Axis)
5-16 Hz 16-22	2.3 g-Peak 6.8		
22-100	2.3	•	
199-200	2.3	Equivalent Shock E	n <b>vi</b> ronment
200 - 2000	5.0 )		
Random Vi	bration	Duration: 2 min.	(Three Axes)
20-300 Hm 300-2000 H	+3 dB/Oct. z 0.05 G <sup>2</sup> /Hz	9.8 g-rms	



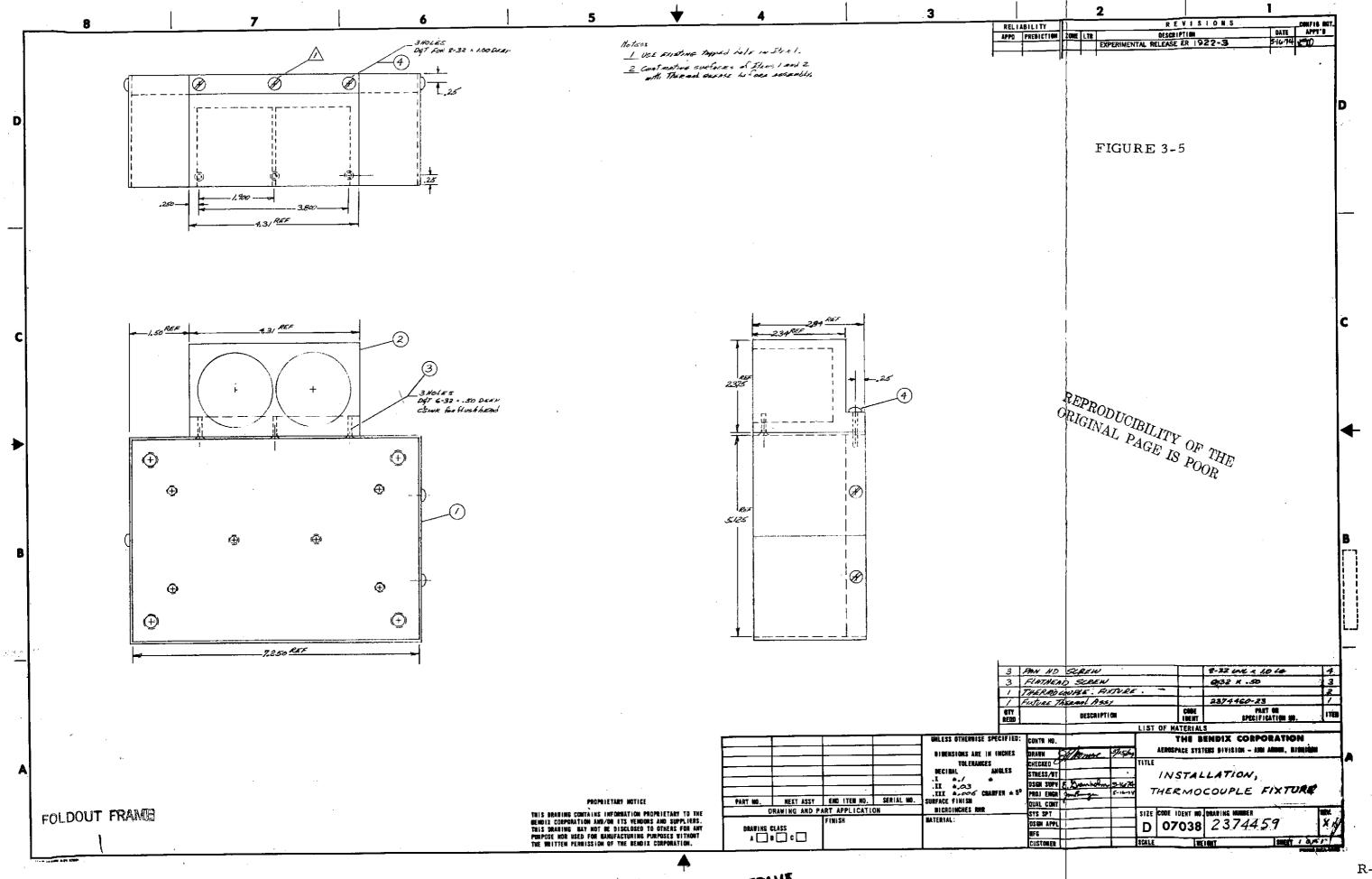
# REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR



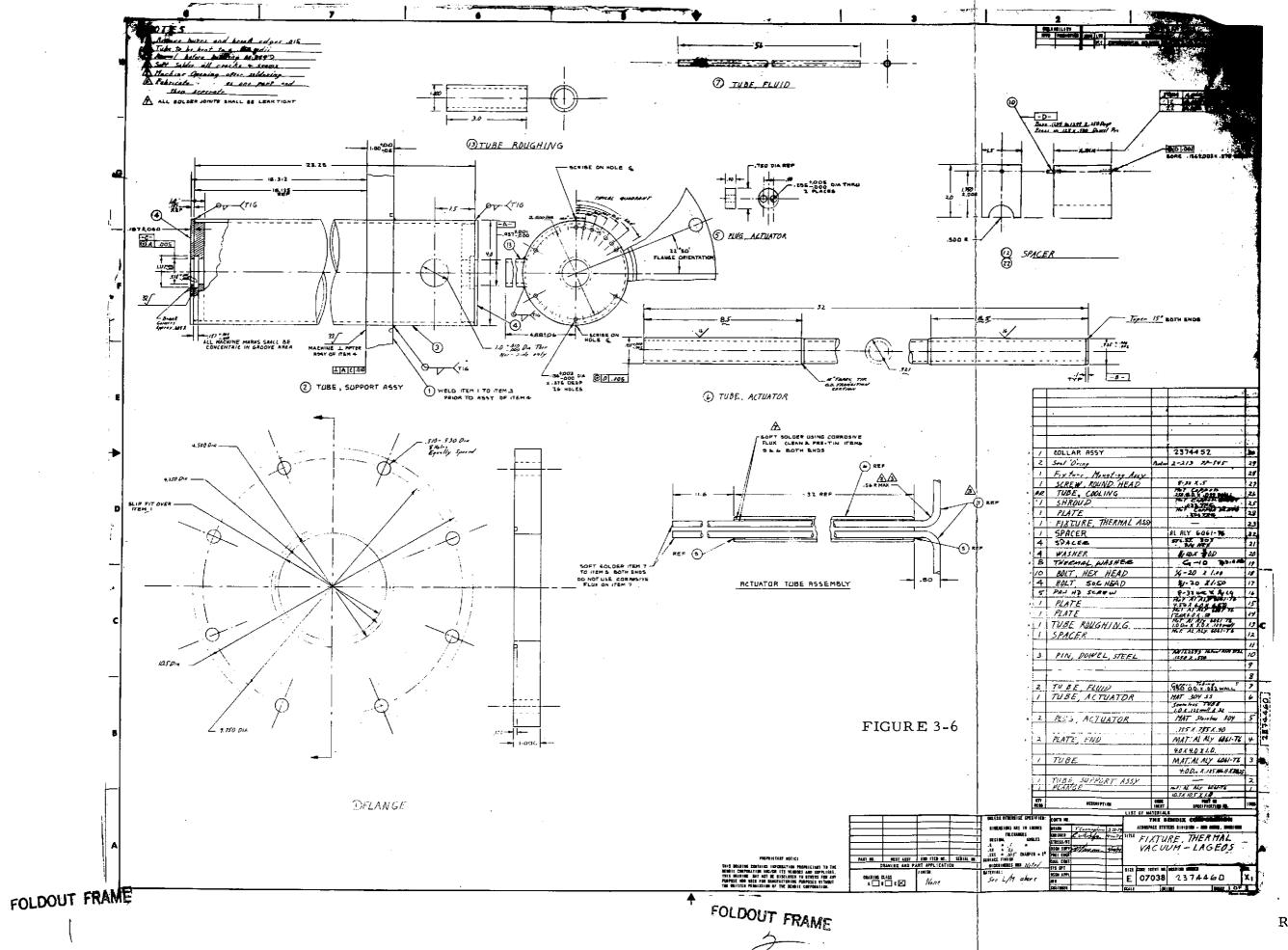


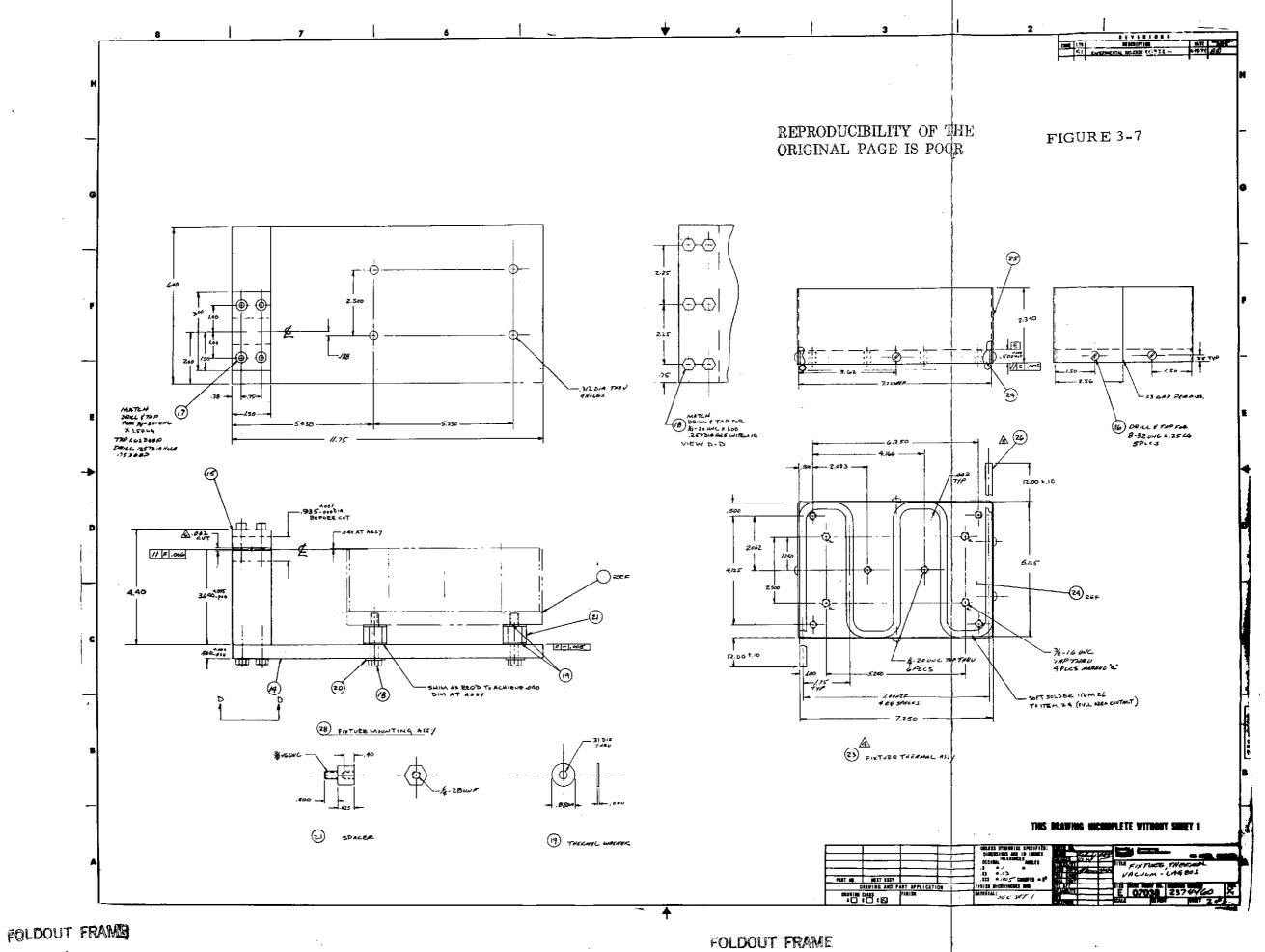


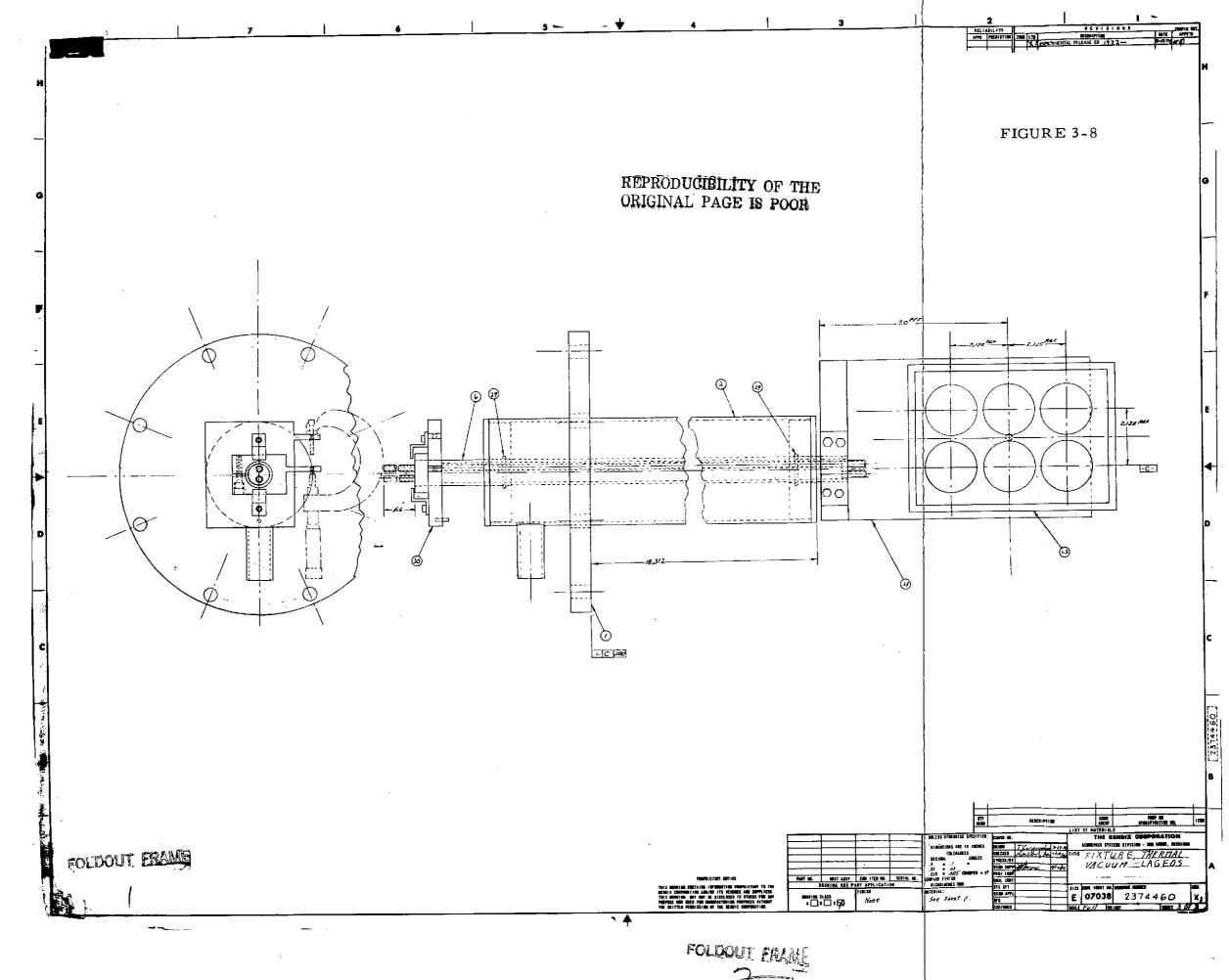
FOLDOUT FRAME

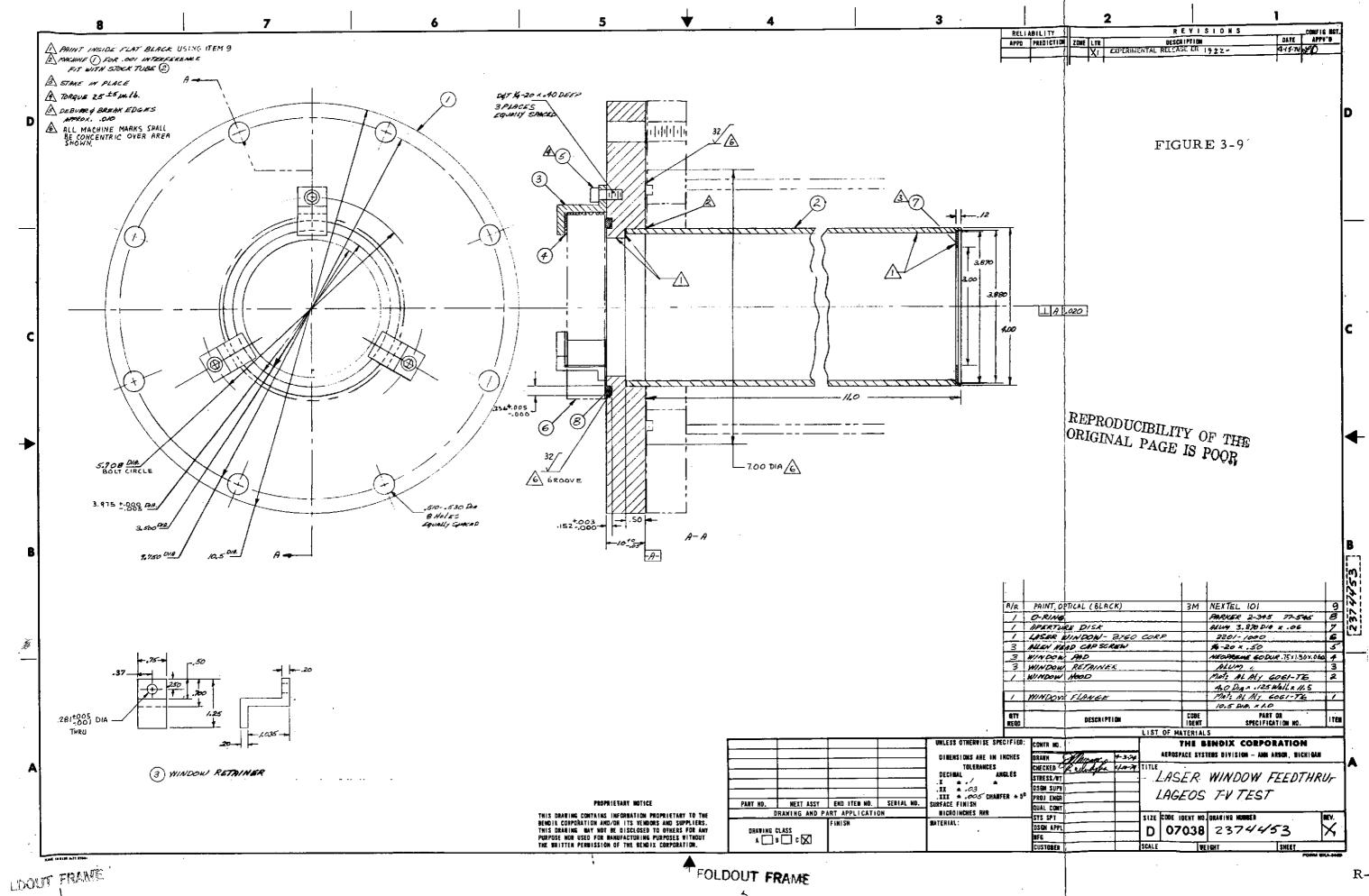


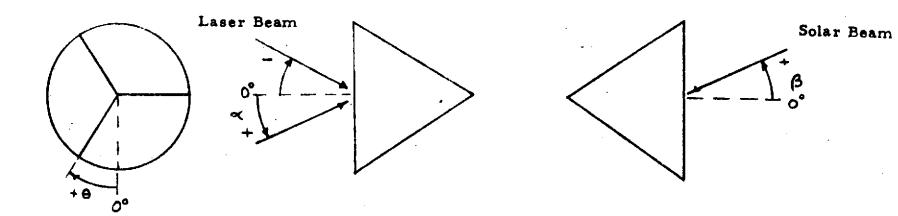
FOLDOUT FRAME









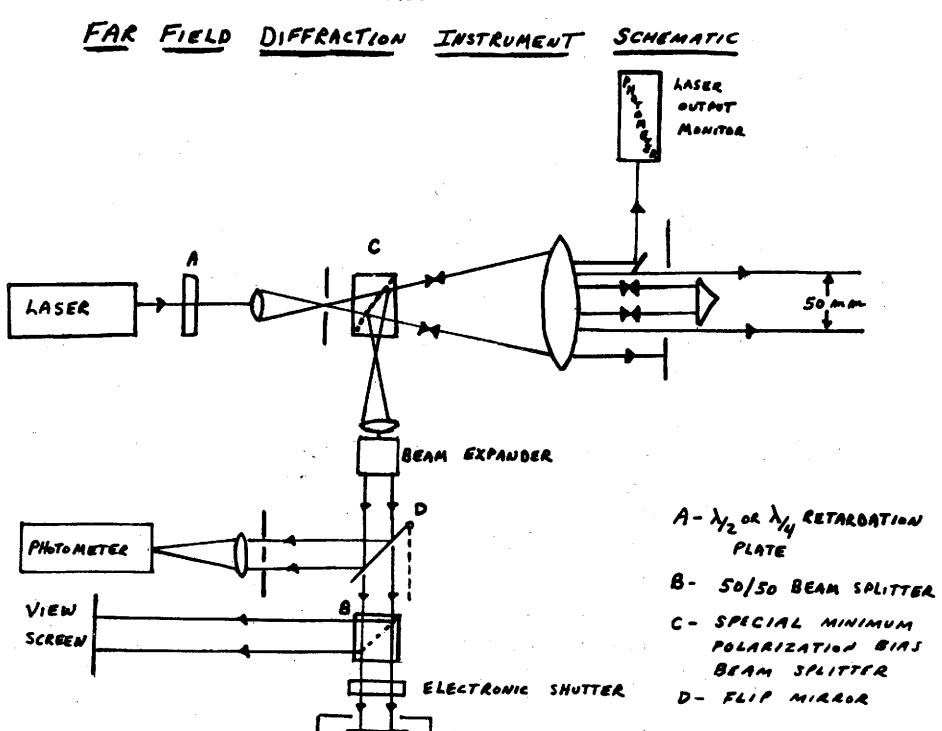


Viewed from Laser Optical Window

Viewed from Solar Simulator

## FIGURE 3-10

SOLAR AND LASER FIELD ANGLES AND RETROREFLECTOR ORIENTATION



MASTER SCHEDULE

THE LAGEOS PHASE 8

Mfg Dopt Mfg Prog

Revision Ne:

to the river talling (takes of \$10.)

AGE

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

	Arraman Chatan	MASTE	R	8	CH	E	UC	LE				Ti	tle	7					- 4									٠.			_		_		2. 3		<u>L</u>	wie:				_
													•		- 4		41	ر م	-				• '	,,,	,,,	•	• •				1	8 64	ed (	)ai		$\Box$	Up	odal 7	-34	ō	Ē	1
	••- <u>·</u>	1977		-	"		М	AC	Τ	4	A	T	24	47	Т	J.,	16	T	772	<del>,</del>	Ī	Au	•	T	-						•						<u> </u>		7.5	-7	<u>*</u>	-
١.	· jtem		2	:	16	2	16	1	•	15	27	1 4	1	25	٠,	1 4	12	<b>`</b> 6		-1	71	17	,		1	l				,												
FIN	AL TELT ARTICLE		$\Pi$	1	П		T	44	┪	П	10	A:	y ka	7	T	Δl	٥l	т	-	17	╅		$\vdash$	╈	T	$\vdash$	_	1 1	-	T	T		_	П	~	1	-		~	_	_	-
Ĺ.	DIFINE REATS.		П	Ι			មរបា	Jim	11117	11.	ijij,	t of	J.		7	Tf	_	1		Ħ	+	Ħ	Ħ	╈	Ħ	1	╈	H	-	╈	╆┪	+		++	+-	╁┼	$\dashv$	┿	+	⊬	-	
	PASL. MOUNT BITHS		П	Τ	$\Box$			$\Pi$	$\mathbf{I}$	П	143	ĪΤ	┰╴	П	7	M		1	$\vdash$	1	+	1	۲t	+	1		+	H		t	Ħ	+	+-	<del>   </del>	+	₩	-+	┿	+-	₽	┝	4
	Cooks, morn's strike		FΤ	1	$\prod$			$\Pi$	Т	П	$\top$	Lil.	10	TT	7	Ħ	. 1	П	1		_		-	+	1	$\vdash$	十	Ħ	$\dashv$	✝	11	7	╅╴	Н	+	₩	-+	╼	+	₩	┢╼	-
	CAUSTY DESIGN ESTAVA			$oldsymbol{ol}}}}}}}}}}}}}}$	П	$\mathbf{I}$		$\mathbf{I}.\mathbf{I}$	1.	$\Pi$	$\top$	TΔ	T	77	7		- I	1 2		Т	7	1-1		+	17		+	H		T	11	+	┪~	╁┼	十	H		+	┿	₩	+-	-
	PESIEN - PINAL TES	PARTICLE ASSY	П	$\top$		$\mathbf{T}$		П	1	П		T	1	11	75		71	ء ارد	-	1"	+	1-1	1	+	1	$\vdash$	+	H	-	╈	╅┪	+	+	╅╌╅	+-	++	┌┼	┰	╁	╀	⊢	-
	PANEL		$\Gamma\Gamma$				П.,	П	Т	П	7		5		7"	1"1		77		1	_	+	1	+	1		╈	11	-	+-	11	-	+-	H	+	++	<u>-</u>	+	╆	₩	┢	4
<u> </u>		رعب و دوربر سرندن و وو	E	$\Box$	$\Box \Box$	$\Box$	$\Box$	П	$\perp$	П		$\Box$	T	$\sqcap$	_	Tt		כד	$\vdash$	11	_	$\top$	-	十	+-	1	+	11		✝	Н	+	+-	+-+	+	╁	-+	╃-	┿	₽	┢╾	٦
		OWER RINGE	П	Ш				$\Pi$	L	$\Pi$	$\mathbf{T}$	П	11.5	$\mathbf{I}$		П	$\top$	ŦŪ.	ret	1	_		$\vdash$	1	$\top$	<u> </u>	╈	11	-	┪~	1-1	+	+	╅	-+-	++	_	+	+-	₩	┢	Н
<u> </u>	RETAINE		ĻĹ	Į.		Ш	$\Box$	$\Box$	$\perp$	$\prod$		_	亚	A.	74.	$\Box$	$\Box$	$\Gamma$		$\mathbf{T}$	1			┪	$\top$	1	+	11	$\vdash$	1	1-1	-	+	⇈	+	++	_	+	+	₩	-	۲
		AFFE - SELECTIO		4_	$\sqcup$	1	1	11		П	٦.	1[	43	$\prod$	$\perp$	$\prod$	$oldsymbol{\mathbb{L}}$	$\mathbf{I}$		П		П			Г		╅	П	1	T	11	十	1	11	+	1-1	$\dashv$	+	十	₩	-	7
<del> </del>	PASTENIAL-AS	y til biwaystic	11	1_	Ш	$\perp$	Ш.	+	1	П		11/2	4	$\prod$	$\Gamma$	A	$oldsymbol{\mathbb{I}}$	$\Gamma$	$\square$	$\Gamma$		Γ		.]	Ι	Π	T	17		T	П	$\top$	1	Ħ	_	11	_	+	+	Н	一	4
<del>  `-</del>			╀	+-	₩	44	1	#	+	₩	4	11	1	H	1.	$\Box$			-	-		E				77	·I			I	$\Box$	_†	.1	17	+	11	+	+	十	H	H	1
├~	FAB / ASEY - PINAL!	SIF ARTICLE	₩.		₩	╄	4-	44	4	14		1-1	1	니	_الالا	Ш			c	1	4	4	21 6	11 11	1		Ι	$\prod$		Γ	$\Box$		1	1 1	+	1,1	_	+	†	۲	H	4
<u> </u>	PANEL	t provest registeries	╁┼	-├	⊢∔	4-	4-	╂╌┞	+	<b>↓</b> ↓	_	+	ننا	1"."	<u>:   c</u>			L	$\perp$	$\Box$	$\perp$	$\Gamma$		$oldsymbol{\Gamma}$			$\mathbf{I}$			Г	П		1	$\sqcap$	1	П	1	+	+	Н	Γ	-
-	UPPER RA		╌		₽₩	4-	_	₩		11	4	<del>↓ ↓</del>	╌	$\sqcup$	1	Ш	_	1		$\mathbf{L}$	Ι			1			I	П		Т	П	7	1	П	$\top$	$\Box$	$\neg$	┪-	+	╆┙	┢	٦
	LOWER RI		╂╌╂	┿	₩	+	4-	++		11	4	1-1	<u>≥</u> ‡"!	\$1 <b>4</b>	┩-	1.4	_4_	1.	100								Ι	$\prod$		Τ	П	T	Т		1	$\Box$	_	+	+	۳	-	7
<del></del>		RINE (4)	₩	+-	╀	4-	-	₩	-	1-4	4-	+	<u>- }</u> [:	<b>9111</b> .	1	Н	_	٠.,	-	1	I	Ц	Н		$\Box$		Ι			Τ	П	7	T	$\Box$	7	11	$\neg$	+	十	Н	г	1
	ADUNT SE		╅┷┼	+	╌		-	++	+-	╀╌┼		₩.	_ J):	<u> </u>	νÆ	H	_	٠.	ᆜ	1	_	L	Ц.	$\perp$	L		L	П		Т	П	Т	Т	П	+	$\mathbf{H}$		1	+	Н	-	1
		, , , , , , , , , , , , , , , , , , , ,	╂╼╉╌		₽	-}	-	╁┼	+	₽		##	14	1	<u>4°</u>	1	_	4	Ц.	1	_	Ш	ш				Ι	$\Pi$		Γ	П	П	Т		1	П		十	1	H	Γ.	1
<del></del> -	RETARRESEE	VA T (6) 1/c	12 1	٠,	┨	+-	+	╁┼		₽₩	+	╁╼╄	-	Ļ.	<u> ا۔</u>	14		44	LĻ,	Ц	4			┸			Ι	$\Box$		Γ	٠.		T		Ţ	П	$\neg$	_	†	Ħ	Г	1
<del></del>		A114 FIE DIEN	150	<del>. [</del> .	↤	-	-	╅┽	┿	╂┷╂	4	┺	-	Fľ	4:	1.1	¥	4		1	ΔĽ	1	4	_1_				П		Γ	$\Pi$	Т	Т	П	Т	П	$\neg$	7	+	М	Г	1
<del>  `</del> -			1.1.	7	$\vdash$	┰	-	┾┿		1+	<del></del>	╁┧	┸	₩	٦	IA.	命.	4-4		1	-4-	L	Ш		L	Ш	L	$\Box$		Ι	П		Ţ	П	T	П	1	1	1	Г	Г	1
	FINAL THELLIL JUS	CA. 7657	H	+-	╀	-		++	+-	₩	-	╁╌╂	- -	Н	4	1-4	4	44	1	1	4		Ц.	1.		Ц	Ĺ	$\Box$		Ι	$\prod$		Т	П	T	П	┲	$\top$	†	Г		1
<del></del>	PRE- 418 T/0		╂┼	┰	╂┈┼	╂		++	+-	╂╌╂	+	╁┼	4-	₩	-	┦┤	4	+-	Ц.	┺	_4_	$\perp$	$\sqcup$	1	Ц	Н	$\mathbf{L}$	П		$\mathbf{L}$	П	Т	1	П	1	П	$\neg$	_	1	Н	Г	1
<del> </del>	VIE 7/111		<del>!  </del>	┰	╀	╅┥	-	₩		╂╼╂	+	+ +	+	₩		14	4	1	Н	44	_#	44	1	┸	1	Ш	┸	L			П	$\Box$	. [	П	$\top$	П	Т	$\top$	T	П	Г	1
<del></del>	P.ST- 418 1/0	TESTS	┰	+-	╂╼╋	-	-1-	╂╂		1-1	+	╁╂	┸	1-1		1-1	_	$\perp$	┵	L		4	n L	1	L	$\Box$		П		Γ	П	П	T	П	Т	П	T	7	$\top$	П	г	1
		, ,	╂╾╉╍	┰	Η	++		╁╌╂	+	╂╌╂	+	1-1	+	╁╅	-	1-4	-	1		14	_	44	JI.	_ _	Ш		L	П		Τ	$\Pi$		Т	П	Т	$\Pi$	一十	7	$\top$		Г	1
	OFFICAL TEST INSTR.	FIOS ANAM DULE	₩	+	┯		+	╁┼		╂╼╂	-+-	┽╃	4	╁╁		₽		-	Ļ∔.	L	<del>.</del>	Щ		Į.	$\perp$	Ш		П		$\mathbf{L}$		$\Box$	I	П	Т	П	T	$\top$	T		_	1
	SET- UP THI AWAL APPT		<del>   </del>	+	1	+		┿	+	++	+-	+ +			_	<b>*</b> ***	4411	•	14		싀-	1	Ш		Ш	Ш		$oldsymbol{\perp}$		L	H	$\Box$	T	П	Т	П	Т	$\top$	T	М	Г	1
	EMRLY THEEMAL POPER		OF.		<u> </u>	Н	+	╁┪	-+-	╂╌╅	+	╃╃	<b>-</b> }-	<b>         </b>	Щ	╁╌╏	-	+-	11	444		19	30	-	4_	Ш	1		Ц.	L	П	$\Box$	1		I	$\square$	$\mathbf{T}$	I	Т	Г	Г	1
			1		<del>   </del>	++	+	╅╉	╁┈	╅		11	┰	H	╌┞╴	₽₩	4	1-	┝┩╼	1		┺	$\vdash$	+	4	<b>.</b>	┸	П	$\Box$	L	$\Box$		I	$\Pi$	I	П	$oldsymbol{\Box}$	I	Τ	Г	Г	1
Ĺ.			1 +	+	┪	╅┥		<del>[  </del>	╅	╅┽	+	<del>   </del>	╁	╁┼		₽		+	┝╌┼╾	-		+	⊢-	+	1	1	4	Ш	LL	1	П		$\perp$	П	$\perp$	П	$oldsymbol{oldsymbol{oldsymbol{\Box}}}$	$\perp$	$oldsymbol{\perp}$	$\Box$	Г	1
745 K	MASSIFIE FIXTURE (1	74466)	1 +	T		╅┥	-	1-1	┿	╁┪	+	+ 1	1-	╁┼	+-	₽	- -	+-	┝╌┡	+	+	$\bot$	$\vdash$		4	Щ.	4	Ш	$\perp$	$\perp$	Ш	$\prod$	$\perp$		$oldsymbol{\perp}$	$\coprod$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{\Box}}}$	1	Γ		Γ	J
	DESIGN		$\vdash$	T	Γ†	┰	+	╁╅	+-	H	+	╅╂	7.	121	┿	H	1881	+-	┢		<del>.   .</del>	1	⊢∔	+	4	⊢∔	4	┦	H	4.	Ш	$\Box$	Į.	$\Box$	$\perp$	$oxed{\Box}$	$oldsymbol{\perp}$	$\perp$		$\Box$	Ĺ	J
	EAR IASSY		1	+-	<del>   </del>	+-	+	╁┼	+	H	+	╅╅	-#4	+~+	+	╁╌┦	Щ.		W)	"	<del>(,</del>	f	┝╌┡	+	┺	┡	╄.	┦	$\sqcup$	4	ĻÌ	$\perp \Gamma$	L	$\Box$	$\perp$	П	$\Box$	$\perp$	$\perp$	$\Gamma$	Г	J
	820616		++	+	╅	+1	┪.	+	+	╁┼	┰	╁╂	+-	<del></del>	<del>.   .</del>	╁╌	-1	4	<del>- ["</del>	1	-	+	┝	+	+	Н	4-	┯	╙	Į.	Ш		1	$\Box$		$oldsymbol{\perp} oldsymbol{I}$	$\perp \Gamma$	$\perp$	Γ	$\Box$	Ĺ	_]
	U1962 Rm6 (2)		t-+		┱	┰	-+-	╂┈╂	+	++	+-	╅╌╂	╁	) H	4	₩		4-		Н	+	+	$\vdash$	4	1	Н	4	Ш	Щ	1	Ш			П	$\perp$	$\Box$		$\perp$	$\perp$	$\Box$	Ĺ	J
	C EA E-4 (2)		┪	+	┢	╅┪	-	╅	-+-	₩	+	╅╌╋	┿	₩	+	•	til ,	-	-#-			+-	-		$\bot$	Н	:	Ш	$\sqcup$		Ш		$oldsymbol{\mathbb{L}}$		I	П	$\Box$	$\perp$	$oldsymbol{\Gamma}$	$\Box$	$\Gamma$	
	Aftervalle Rout (	1)	H	+	┢	╅┤	-	╁╾╁	+	₩	┪~	┿	-+-	╁┼	+	ţ٠	Щ.	4	-	$\mathbf{H}$	+	+-	$\vdash$	+	+	Н	4	H	$\perp$	I	$\Box$	I	$\perp$	$\Box$	$\perp$	П	$\Box$	$\perp$	Ι	$\Box$	匚	_1
	SC RF - F		H	+	<b> </b>	╁┤		1 1	+	┯		╁┼	╁	╁┼	7:	<del>].  </del>	-	+	⊢∔	₽	+	+-	╌	╄	₽-	Н	+	₩	Ц.	1	Ш	$\Box$	L	П		$\perp \perp$	$\perp$	$\perp$	$\perp$		$\Box$	
	KILL ALFACTOR (		Η,	4-	٦.	.  -	<u> </u>	1 1	╁	H		╅	╅	╅╅	7.	<del>[                                    </del>	+	Н	$\vdash$	╂┤	+-	₩	⊢∔	+-	+-	<b> -</b> -	╄.	╄┦	$\vdash$	1	$\sqcup$	1		Ш	1.	$\perp \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \!$	1	1	1	L		_
	MATCH DELLOW THIS P.		$\vdash$	⇈	1	╅	7	1 /	+-	+ +	+-	╅┽	╅	╅┪	+-	┿┪	щa	+	$\vdash$	╂┥	+	₩	⊢∔	+	╄	┝╁	+	₩	$\vdash \downarrow$	4	Ш	4	$\perp$	Ш	L	L	1	L	1	$\perp$	L	J
			<del>                                     </del>	+-	$\vdash$	++	+	1-+	+-	† †	+	╅╅	+	╁┼	┿	╁	44 5	Ή	$\vdash$	Н	┿	+-	+	+	-	H	<del>-</del>	┦	┟┷	4.	H	4	Ŧ.	Ц	┵	ш	Ц	_L	1	F	Ĺ	_
ma rie	F C. # (	8 DW 4-74-74 IL	4			+++		•	Η-	<del></del>		4*	٠.	r.L	+		-	+		1		╁	Ļ	⊥	4	Ш	1	ш	ᄔ	1.	Ц	Ц.		Ш	丄	ப	4	止	┸	ட	L	_
	terrander of access	## / 1 # 4 7 1 4 \$ \$ 4 7 1 4 5 6 14 6 6 6 7 7 7 7 7 7	1.0 m m 1	•••				•••.	L										l				911	1:15	- [				N	e×ī	H	ghe	: r	5c he	dul	c N	io		ŀ,	Age		
37.7	*** ***************	·#· < • > • • / • • • · · .		٠.				•	-	hhe		T	Te	.,	Τ.	Mf=	$\overline{}$		Mf			1	₩		-1				-								J	,	ŀ		,	
× .	3) 24 . 4 . 7 A 6 ! A . A . 7 . 7 .	(at all the	<del></del> -										• •		i_'	X	- 1/5	P 1	with	•	: 7g	1	Εn	gr	ı	Pro		Lon	4							7	- 1	_	_	ч.		_

See 1979 FEB MALE MALE MAY WORK SET TO SET T	EDULE  TILLO PAR-FIELD DIPPRACTION INSTRUMENT NO GAPITAL TOUR RAVISION FOR CONTROL TOUR PROCESSION	
THE STATE OF THE STATE STATE OF THE STATE OF	4 · 2 - 74 Update	d Oni
ACTION OFFICE TOWN OF THE PROPERTY OF THE PROP	2,   12,   1,	2 / 1
ACT CONTROL OF THE PROPERTY OF	2 16 16 13 27 17 21 8 22 6 20 3	
Statistical State (1980)  Delical  Leaver College (1980)  Delical  Leaver College (1980)  Delical  Delic		
ATT OFFICE WINDOW  OFFICE STATES AND ATT OFFICE STATES ATT OFFICE		┷╁╢
THE STATE OF THE PROPERTY OF T	***************************************	┵┵┦
Detect  Assert-Continuing Againsts  Layer Continuing Againsts  Detect  Layer Continuing Against   Detect Continuin	<del>▞░▗▝▗▗▄▗</del> ▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗	┿╌┥
ACTIVE CONTINUES PROPERTY DESIGNATION OF THE PROPERTY OF THE P		+ + +
After Denomal and Control (Control (Con		╼╂╾╂╼╏
Between State Column Ministralia  Michigan State Column Ministralia  Methods and a State Column Ministralia  Ministrali	▗▗▎▗░░▘▎▗░░▞░▜░▜▝ <del>▀▍▘▜▘▀▋▀▍▘▍▗▐▗▗▍▗▊▄▐▃▗▍▗▐▗▄▋</del> ▃▋▃▋▃▋▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▍▗▋▗▋▗▋▗▋▗▋	╼╅╾╂╾┧
Serial and Alles 1986  Serial conditions of 1986  Passing of the Part  Passing of the Pass		┵┿┪
SETABLISHE STIFF CHAPT  PASISHED CHEER CHEER CHAPT  PASISHED CHEER CHEER CHAPT  PASISHED CHEER CHE		╼╂╼╅╌╏
THE MATERIAL MATERIAL AND STATE OF THE STATE		╼┾╌┦
General State Stat		╼╊═╂
General State interval Description (1911)  Description State (1911)  Description File (1911)  Title  OFFICAL MINISTER  If Advisor Adams, Description (1911)  If Constitution (		╼╂╼╂╌ჽ
Desire of the state of the stat		╍╂╌╂╌┧
District Triple (111)  Title  Officer window  If the office of the first of the fir	<del>▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗</del> ▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▄▗▗▄▗▄▗▄▗▄▗▄▗▄▗	╼╄╼╂╌╂
THE AMERICAN PRICE STRUCTURE (SES)  THE AMERICAN WINDOW  THE CONTROL MENT OF THE STRUCTURE  ME OF AMERICAN STRUCTURE  THE CONTROL MENT OF THE STRUCTURE  CONTROL THE STRUCTURE  CONTROL TO THE STRUCTURE  THE CONTROL THE STRUCTURE AND THE STRUCTURE  THE CONTROL THE STRUCTURE AND THE STRUCTURE AND THE STRUCTURE  THE STRUCTURE THE STRUCTURE AND THE STRUCTURE AN	▗▕▗▕▗░▊░░▊▆▆▆▆▆▆▆▆▆▆▆▆▆ <del>▊▀▍▃▍▃▍▃▍▃▋▃▋▃▋▃</del> ▋▃▍▃▋▃▋▃▋▃▋▃▋▃▋▃▋▃▋▃▋▗▋▗▋▗▋▗▋▗▋▗▋▗▋▗▋▗▋▗	╌┾╾╁╺╉╵
DITICAL NUMBER  MICHAEL NUMBER  MICHAEL STREET  STATE OF STREET  CANTING STREET  DELIVER TO SERVER  PROPERLY TO SERVER  PROPERLY TO SERVER  PROPERLY THE SERVER  SERVE		╌╂╌╂
DITICAL NUMBER  MICHAEL NUMBER  MICHAEL STREET  STATE OF STREET  CANTING STREET  DELIVER TO SERVER  PROPERLY TO SERVER  PROPERLY TO SERVER  PROPERLY THE SERVER  SERVE		╅╅
OPTICAL WINDOW  Micentant Mate, Official Signature  I fall Discover  State Discover  We go Antao  Committe Office  Fronce Material  Mate	<del>╡╛╛┪┪┪╬╬┪┪┪┩╒╒┩╬┦╃┩╚</del> ┞╀╀╀╀	╼╁╼╁╌╅╏
AT LOUTING HOUSE SALE DESIGN FROM AT LOUTING	┱┇╌╏╌┇╼╀╼╏╌╏╌╏╌╏╌╏╌╏╌╏╌╏╌╏╌╏╌╏ <del>╒╏</del> ╇╙╜╠╵ <b>╬</b> ┇╏┈┆┈╏╌╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈	╼╋╼╂
ME-CONTROL MAIN BETWEET SAW RETION  I MALO OF THE DESTRUCT SAW RETION  W. GO-ANTAGE  FRONTE DETAGE  FRONTE DETAGE  FRONTE TO THE SAME SAME SAME SAME SAME SAME SAME SAM	┱┇╌┦╌┩╌┩╌┩╌┩╌╃╌╃╌┦╌┦╌┦╌┦╌┦╌┦╌┦╌┦╌┦╌┦┈ <b>┦┆┩╏┩╏┩┼┈┦┈╌╌</b> ╒┼╌┩╌┩╌┩╌┪╌┪╌	╅╅╬
MINITED SECRET SON SEVERY  MYC GO-MATAO  GANTATO  GANTATO  GANTASTO OFFICE  FARALCATE  CARTING (SEVERIMAN)  CARTING (SEVERIMAN)  CARTING (SEVERIMAN)  CARTING TO BENDY  DELIVE TO BENDY  PROPRIET JALEN, SIMPLE OFFI, MINISTER, MI	┪ <del>┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍┍</del> ┍╌ <del>╒╒╒╒╒╒╒╒╒╒</del>	╅╅
All Supplies to the state of th		╅┿╬
SCHIEF OFFICE  FRONTE		4-1-1
Contribute Office 116 116 116 116 116 116 116 116 116 11	<b>⋒</b> ┊┇┇┪┪╫┼┧┧ <del>┇╏┪╣╒╏┍┼┼┪┪┋╏╏╒╃╄╚╏┋</del> ╒┦ <del>╒┋╒</del> ╀╒╄╃┩┞╏╚╏╚╏╚╏┇╏┆╏╏╒╏╒╬	1-1-1
PROTECTION OF THE PROTECTION O		<del>++++</del> ;
FARRICATE  CANTING (STYPHOOD)  CONTENION OF THE CONTENION		<del>1 1 1</del> 7
CANTING (STUFFIRM)  CALCULATING (STUFFIRM)  CALCULATIN		<del>+++</del>
CATCH-OUT \$ 17 17  Decine 2 To 86 NO 19  Tyco 86 NO 1, 10 10 10 10 10 10 10 10 10 10 10 10 10		<del>1-1-1</del> 7
DELINE E TO BENDIX  PROPERTY, SHAME OFF, with ANY Property and a second		<del>111</del>
Price field a factor of the state of the sta		111
	▗▘▗▗▗▗▗▗▗▗▗ <del>▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗</del> ▗ <del>▗</del> ▗▗▗▗▗▗▗▗	
		7 17
	<del>╵</del> ┸┦┸╏┸┸╫╫┸╫╫┸╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫╫	
THE PROOF SALE OF LAND CONTRACTOR	<del>╵</del> ╸╸ <del>╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>	
PARTIE WE SOURCE COLLEGE COLLE	<del>┆┆┆┊┆</del> ┊╚┆┆╚┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆┆	$\Box\Box$
Parks & Sarra Ottos Vicina States Control Cont	<del>┦╒┩╒</del> ╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╫╒╇╇╒╇╇╒╇╇	$\perp \perp \uparrow \uparrow$
Parks & Course Course Course Selection Course Cours	<del>┦╎╏╎╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏╏</del>	$\Box\Box$
Parks & Acres office Come Substitute (1997)	<del>┦┆┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩┩</del> ╇┪┪┪┪┩┪┩┪┩┪╇┪┩┪╇	
Parks # Rewise Carre officer from Endage Contracts	╀┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼	$\perp \Box$
Parks # SCWSS CALLS OFFICE FROM STATE STAT	<del>╃╏╏┩╒╏╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>	$\perp \Box \Gamma$
Parks # Starts Dates Com States C	<del>╬╍╏╌╏╌╏╶╏╶╏╶╏╒</del> ┇ <del>╒</del> ┇╒┇╒┇╒┇╒┇╒┇╒┇╒┇╒┇╒╬╌╂╌╂╌╂╌╂╌╂╌╂╌╂╌╂╌╂╌╃╌╏╌╏╌╏╌╏╌╏╌┼┼	+ $+$ $T$
Marks # REWSE BACIE DELIGA FRIM GIACULOUS FOLDALETO	<del>┆╒╏╸╏╶╏┊╒╏╶╿╒╒╏╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>	$+\Pi$
200 - 100 miles in the control of th	<del>╎╸┡╸┩╸┩╸┺╸┸╶┙╶┪╸┸╸┇┈╏┊╏╶╏</del> ┎┇┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎┎	++1
To LINEARLY-POLARIZED BEAM SHOWLY SHO		44
Men Bent Constant Agent agent agent Schodule No Cher Test Mig Dept Mig Prog Engr Prog Cont	1 Mary 10gher Schedule No.	N.F

ndb	Aerospace Proteons Division	MASTE	R	91	. H	FF	11	1 F				I	itle		74		- /				-0	151	€ ~/	10.	16	10	<b>4 5</b>	ek,	ادر	_	_		14			1	levi	ilos	No	21	
```		BIAUIL			y 11							1				_	1	<i>58</i>	<i></i>					_							100	9	9	11 7 Y		ľ	Upda	y : /	Ö	74	,
	Bern	. 1974		F	18	_1_	49.	AR		A	*	Т	A,	44	Т	J.	M	Τ	771	7	Ţ.	Av	4	Т																	•
	Trees			2	16	Z	16		·-	13	27	7	//	35		7	22	6	1	•	7	17	,	1	- 1		1	1		1	1		ı	1	1		ı	1	ſ	ı	
740	CMAL POPLIAL TEST FIX.	rud <b>e</b>		$\Box$	$\Box$	П	Τ.	$\Pi$	T		Τ	$\mathbf{L}$		$\Box$		T	Ι.			Т			П	Т		${f I}$	Τ	$\Box$	Ι			Т		7	11	Т	T	╈	o	t	•
	ottwe Klass.		$\Box$	1,515	$\Box L$		7	Αľ	7		$\perp$	$\Box$		$-\Box$		$\mathbf{T}$	$\Box$				П	$\mathbf{I}$		$\mathbf{I}$	$\Box$	$\perp$	$\Pi$		I			Τ.	П	7	11	T	11	_	17	忄	•
	DESIGN		$\Box$	$\Box$	$\perp$		1	35.	1.14	Ш	$\mathbf{L}$		2.	46	rr.	115	$\prod$	J		Ι	П	$\mathbf{I}$	П	$oldsymbol{\perp}$	$\Box$				$\perp$	П			П		11	┰	$\Box$	7	1	t	•
	FAO PARTE		$\coprod$	$\Box$	$\perp$	$\Box$		П	$\perp$		1			IJ	1112	ijЩ	14		П		П	$\mathbf{I}$	П	$\perp$	$\Box$	$\Box$	$\Gamma$		Π.	П	$\Box$	T			П	1	17	_	1	†	•
	ASSY & CHEEK-BUT		$\Box$	П		$\coprod$	I	$\Box$		П	$\perp$	ш	111	$\Gamma$		$\mathbf{T}$	133	$\mathbf{p}_{\mathbf{p}}$	Œ	Τ.	$\Box$	T			$\Pi$			$\Box$	$\mathbf{I}$	П		Т	П		П	1		7	$\mathbf{T}$	忊	•
CPT	TONE WHOSE & SHIPLS.	ATCY	П	$\Box$	$\Box$	$\Gamma$		Ш			L	$\mathbf{L}$	$\Box$	$\coprod$		Ι.		L		Ι	П		$\Box$	1.		$\perp$				П		Ι	$\Pi$	$\mathbf{I}$	П	1	П	7	1	T	•
	DITIMI ALASS.		$\Box$	77	$\Box$	To (	14	$\cdot \Box$		${\mathbb P} \Psi$	4	$\Box$	$\Box$	$\mathbf{L}$		<b>1</b>	$\Pi$	$\mathbf{I}$	$\Box$	L	П		$\Box$	I	П	I	Г	П	Τ			T	П		П	┰	$\mathbf{T}$	+	1	t٠	٠
	DES. AN		$\coprod$	$\Box$		$\mathbf{L}$		Ы	2.	114	c					Ι	$\Pi$	$\mathbf{I}^{-}$	П		П		$\Pi$		П	$\Box$		П	Ι	П	$\Pi$	Т	П	1	П	1	$\Box$	7		T	1
	EAB PARTS			$\perp$		L	$\perp$	Ш			_	7,11		-			П	$\Gamma$	П	1	$\Box$	7	4-1	5441	•		П	П	Т	П		I	П	T	П		$\mathbf{T}$	7		+	-
	WINDOW DALIVERS		П		$\Box$		$\perp$	$\prod$			4	1	AL.	L			П	$\mathbf{L}$	I.I	1	Ы	1	-/ (		$\Box$	T	П	П	Τ	$\Box$	$\Box$	I.	П	Т	П	7	П	$\top$		1	
	ASSY.   CHICKOUT	W T/J CHAMBER	$\prod$		$\Box \Gamma$				$\perp$	Ш	$\Gamma$	.)U	Ш	Щ	П	$\perp$	$\Box$			1	1941	$\perp$	$\Box$		П	$\perp$		$\Box \Gamma$	$\int$	$\prod$		I		$\mathbf{J}$		T	$\Box$		1	T	•
			П	Ш		$oldsymbol{\perp}$	L	$\perp$ I		Ш	$\perp$		Ц.	$\perp$		$\perp$	П	Ŀ	$\prod$	$\perp$	П			$\perp$	$\square$	$\perp$			$\perp$			I		$\perp$	П	T	ΠŤ	T	Т	T	٠
			П	Ш		$\Box$	T.	$\Box$	$\perp$	П	$\perp$	ļ.,	П	$\Box$	Ц	$\perp$	П	L	$\Box$	I	$\Box$	$\perp$	П	$\perp$	$\Box$	I	$\Gamma$	$\Box$	J	$\Box$	$\Box$	Ι		$oldsymbol{\mathbb{T}}$		J			Т	T	•
FF			Ш	44		Ш	┵	11		Ц	Д.	1	Ц	Ш	Ш		Ш		П		ш	L	Ш	L	Ш		L	$\Box$		$\mathbf{L}$	$\Box \Box$	Ι.	П	Ŧ	П	Т	$\Pi$	$\top$	Т	T	•
FF	DI SUPPORT PLATE	<del></del>	Ш	┸	Ц.	┙		$\perp$		Ш	$\Gamma$		Щ				$\Pi$		$\coprod$	$\perp$	П		$\prod$	$\perp$	П	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{I}}}$	$\Gamma$	U	T	$\Box$		Τ	П		П	1	TT		Т	T	٠
	DEFINE REBUIRE	MENTS	Ш	Ţ,		14	794	<u> + I</u>	1.4	1	174 L	· [_]	Ц	$\mathbf{L}^{2}$	$\Box$	$\mathbf{I}$	$\Box$	I	$\coprod$	T	$\coprod$	I	П	I	П	$\Box$	Ι	П	Τ			Τ	П	<b>T</b>	T	┪	1-1	$\neg$	1	t	•
	DESIGN		$oldsymbol{\perp}$	Ш	$\sqcup$	┵		$\perp 1$	1.	Ľ,	۲,	_[_	П	$\perp$		$\mathbf{I}$	$\Box$	$oldsymbol{\perp}$	П	$oldsymbol{\mathbb{I}}$	$\Box$	$\mathbf{I}^{-}$	$\Box$	$\mathbf{I}$	$\prod$	$\mathbf{I}$	I	П	T	П	П	T	П		П	Т	$\Box$	$\top$	7	T	•
	FAB IASSY		Ш	$\perp$			1	Ш	$\perp$			2 3			Ш	$\Box$	$\mathbf{I}$	.1.	П		П	T	П		$\Pi$		Т	П	Т	Т	П	T	П		Ħ	1	11		+-	+	-
	FIT-CHEEE ON FRE	2		$\perp$	Ш	Ш	L	Ш			$\perp$	J		Π.		L	П	1	П			'nΓ	П	$\Gamma$			Т	П	7	П	П	T	П	T	П	7	$\Box$		1	†	•
			$\Pi$	$\Box$	$\Box$		$\perp$	$\Box$	$\Box$	П	J	Ι	$\Box$	$\perp$	П	Ι	$\prod$	$\perp$	$\prod$	$\mathcal{I}$	$\prod$	T	$\prod$	T	П	T	T	П	1	П	П	Т	П	┰	11	1	71	1	+	+	-
4.6	RATION TEST FIRT	V# 6	$\Box$	$\perp$			$\perp$	П	T	$\Box$	$oldsymbol{\mathbb{I}}$	10		ے او	$\prod$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{ol}}}}}}}}}}}}} $	$\Pi$	$\Box \Box$	$\square$	I		$\Gamma$	$\Box$	T	$\prod$	T	1	$\Box$	T	П	1	1.	П	T	11	┪	$\top$	<u>_</u> †_	1	+	-
	PETING REATS.		П				$\perp$	$\Box$	$\perp$		40	) [		400		floor	IJ	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{\Box}}}$	$\square$	T	$\Box$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{\Box}}}$	П		$\Gamma$	$\Box$	Т		1	Т		7	П	┰	11	+	H	$\sqcap$	1	†	
	011.44		ш	Ш			$\perp$	$\Box$	$oldsymbol{\mathbb{L}}$	$\square$	$oldsymbol{\mathbb{T}}$	Ι	uu	11	$\prod$	]	C	J	П	T		T	П	$\Box$	$\prod$	1	T		丁	Т	17	T	П	1	11	╅	77	$\sqcap$	1	+	
	FAB		$\coprod$		$\Box$	П		$\Box$	I	П	$oldsymbol{\mathbb{I}}$	1	$\Box$		int	I	711	۵	$\Box$	T	П	I	П		П		Т	TŤ	_	Т	$T^{\dagger}$	1	17	1	11	+	11	一十	+	+	-
	FIT- CHELK ON VI		$\coprod$	Ш	Ш			П	$\perp$	$\square$	$\perp$	$\perp$	П			III	$\coprod$	•1	14	۲	$\Box$	I		Ι.	П		Т	П	Т	Т	П	Т	П	1	11	1	7	$\sqcap$	T	T	•
	FIT-CHEER WITH	TEST ARTICLE PA	1-	Ш	Ш			$oxed{\Box}$	$\perp$	口	$\perp$	$\perp$	$\prod$	$\perp$	╚	111		7.	1	$oldsymbol{\mathbb{T}}$	$\prod$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{ol}}}}}}}}}}}}} $	$\prod$	J	П			$\Gamma^{\dagger}$		Ι		T	$\Gamma$				11	$\sqcap$	1	十	-
			П		Ш			$\Box$	$\perp$	П	$oldsymbol{\mathbb{I}}$	$oxed{\Box}$	П		Ⅱ	T	$\coprod$		$\Box$	T	$\prod$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{\Box}}}$	$\prod$	J	П		]	$\Gamma^{\dagger}$			1	T	T	Т	77		$\mathbf{T}$	<b>—</b>	1	†	•
			$\Box$		Ш	Ľ				$\Box$	$\perp$	Ι	П	$\perp$	$\Box$	Ι	$\Box$	$\perp$	$\prod$	Ι		$\perp$	$\prod$	$\Box$			Τ	$\Gamma^{\dagger}$	1	1	П	T	Π	T	11	1	7.7	$\sqcap$	1	Ϯ	-
TH	CA-AL BOTHER TEST S	TTOP (REF)	$oldsymbol{\perp}$	$\perp$	1.1					$\Box$	$\perp$	Ι	$\Box$	$\perp$	П	Ι	П	$\perp$	1 4	nii	:111	$\Gamma$	$\prod$	$oldsymbol{\perp}$	$\Box$		T			Т	П	1	П	┪	11	1	7		1	十	•
<u> </u>			1_[		Ш	ــــــــــــــــــــــــــــــــــــــ	$\Box$	$\Box$		$\Box$	$\perp$	$\mathbf{I}$	П		$\Box$	$oldsymbol{\perp}$	$\prod$	Τ	$\prod$	$\perp$	$\prod$		П	$\Box$	П		T	11	1	Τ	П	1	П	寸	$\sqcap$		71	$\sqcap$	1	†	•
745	AMAL SEPTIME TESTS	(REF)	1.		Ш	1		_[_]		П	$\perp$	T	П	$oldsymbol{oldsymbol{oldsymbol{\square}}}$	П	Ι	$\Box$	$\Box$	$\prod$	$\perp$	$\Box$	iit i		$\Box \Gamma$	Π		T	1.1	1	Τ	11	1	$T^{\dagger}$	$\Box$	$\top$	$\Box$	71	$\sqcap$	_	†	•
			$\prod$		Ш	L	Ш			$\Box$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{I}}}$	$\perp$	П	$\perp$	П	$oldsymbol{\Gamma}$		$\Box \Gamma$	$\Pi$	$oldsymbol{T}$	$\Pi$		$\prod$	╗	П		Т	11	$\top$	T	11	$\top$	Ħ		77	1	77	$\sqcap$	1	T	-
٧.	EMATIN TEST	(R67)	Ш	$\bot$	LΙ	1		$\Box$		$\Box$	1	T		$\mathbf{I}$	$\prod$	$\Box$	$\Pi$	$\Box$	$\Box$	$oldsymbol{\mathbb{I}}$	$\prod$	$\perp$	Ĭi.		П	$\sqcap$	Т	17	1	1	$\sqcap$	$\top$	П	T	┱┪	1	J	一十	7	T	-
-			Ш		Щ			$\sqcup$		Ш	$oldsymbol{\perp}$	$\perp$	$\coprod$	J	$\Box$		$oldsymbol{\Box}$	$\Box$		I	$\prod$	$\Box$	П		П	П	┰	$T^{\dagger}$	T	T	1 1	7	77	T	77		77	$\sqcap$	7	T	•
	,		Ш		$\Box$		Ш	┰	LL.	$\prod$	$\Box$	$\perp$	П	$\perp$	П	$oxed{\Box}$	$\mathbf{I}$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{\Box}}}$	$\Pi$	Τ	$oxed{\Box}$		П	1	Г	ΠŤ	丁	11	7	1	11	┪	T		7 1	$\sqcap$	$\top$	$\sqcap$	7	1	
<b>i</b>			П		Ш		Ш			$\Box$	$\Box$	I	П	$\perp$	$\square$			$\Box$	$\mathbf{I}$	I		$\perp$			T	$\Box$	Т	11	T	1	$\sqcap$	$\top$	77		11		$\top$	П	T	1	
<u></u>			$\Box$		ப	$\perp$	$\square$			$\Box$	$oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{oldsymbol{ol}}}}}}}}}}}}} $	$oldsymbol{\mathbb{L}}$	П	$\perp$	$\prod$		$\prod$			T	П	Ţ			T		丁	11	1	1	11	1	П	П	77		$\top$	$\sqcap$	1	+	
			$\Box$	$\perp$	$\Box$	$\perp$						$\perp$	П	$\mathbf{I}$	$\prod$			T		I	$\Box$				1	$\sqcap$	1	17		Τ	17	┪	77	T	77	П	$\top$	$\sqcap$	$\top$	Ť	•
<u> </u>			П		$\prod$		$\Box$			$\Gamma$	$\Box$	$\perp$	П	$\Box$	$\Box$		$\Box$	$\Box$	I		$\Box$	$\Box$	П		1	П	┪	11	1	1	11	十	П	П	$\sqcap$	П	$\top$	$\Box$	T	7	-
<u> </u>	<u> </u>		$\Box$				П					I	П	I	$\square$			$\Box$				$\Box$			Т	$\Box$	┱	11	$\neg$	$\top$	11	1	1				7	$\sqcap$	1	1	-
<b>.</b>			$\coprod$				$\prod$					Ĺ	П	I	$\Box$		$\mathbf{L}$	$\mathbf{I}$			$\Box$				T	П	1	77	$\Box$	Т	1	T	$\top$		11	П	T	$\Box$	T	T	•
<b> </b>			$\perp$ I								П		П	I	$\Box$		$\mathbf{L}^{\mathbf{I}}$	$\mathbf{I}$		$\Box$	$\mathbf{I}$				T	П	7	77		十	77	7	11		$\neg \neg$	П	Т	П	T	7	-
<u> </u>					$\Box$		$\Box$		$\Box \Box$	1	$\Box$		П	I	$\prod$		$\mathbf{I}$	$\Box$							T	1	T	7-1	$\sqcap$	+	11	1	77	$\sqcap$	1	П	T	П	1	Ť	ĺ
<b>.</b>			$\prod$		Ш				Ш		$oldsymbol{oldsymbol{oldsymbol{\square}}}$		П	$\perp$			$\mathbf{L}$				$\Box$		Γ		1	$\Box$	1	77	$\sqcap$	1	11	1	Т	П	$\Box$		T	$\Box^{\dagger}$	T	7	ĺ
			$\perp$ I	1	LI			L	L.I.	$\mathbf{L}$		1	$\coprod$	$\perp$								$\Box$	$\Gamma$		T		1	111	1	$\top$	7 1	7				П	T	IT	T	7	į
	CAUITY STACIAL	. impacri tiali af		( ) , ,	· .	ا د 1 و	• •					_[								_		T	الإ	115.					T	CAL	16	give	1. 3	sc he	dule	N	۰		1.15	<u> </u>	•
	chie 12 Fac to previet to se e ; Pat walk par Modif warn									^-		7	-				fg I	<b></b>	1.	· · ·	D	1	٠.,		┪			Con	4								1	,			,
	<u> </u>				. <del></del>					Oth	e r		- 1	l'est		e M	100	ar nt	1.01		PT.	a 1		nge	1	n			. 1								1 -				,

FIGURE 5-6

	Aerospines Bysterie Olvielen	MASTE	R	80	HE	DI	JLE			T	ilie	700	6 T	14J.	# A 4 4	NT .	uppe,	ۍ دمرينر	CHP KA	10.	. A 114	rien	77.	17	_	0 100	4 0	K 3		L	ision		
				-		,		·, ·		-		- 1			1		_	*	. т						_1_	*	. 2	,4		Ļ.	7-1:	/	_
	Item	1974		//		1 1	HAA	•	APR			۲		200	١,٠	71 ¥	Ι.	101	١,														
			2	1 /	<u>د ا</u>	<u> </u>	16 1	ا دا	<u> </u>	7 /	// 3	15	8		6	20	4_	17	31		<del> </del>	┷,	┵.	_		_	<del>  _ </del>	┷	┷				
712	r layithedt			14	$\perp$				$\perp$	-1-1	$\perp$		Щ	╀	Н	11	Ц.	H	<del>]  </del>	┵	₩.	44	₩.	╁╼┼	44		₩	┿	₩	+	₩	<del>↓</del> .↓.	4
	THERMAL VACTOR	E 4 14 6/2 (4 2 8)	19	44	┷		$\vdash$	-		╌┨╌┤	44	$\vdash$	Н-	##	Ħ	ЩЩI	шш	μщ	4-+	┿	╂╌╂	4-4	┝╋	╁╁	+	+	╁╁	++	┿		╄┾	┢╌╁	-
	GENALE & SILAR SI		44	11			$\vdash$	1-1			-1-1	H	⊢	<del>     </del>	<del>L</del> L	<del>. [_]</del>	<del>   </del>	<del></del>	:}{	+	╂┼	╌┼╌┤	╌╂╼	╅╼╂	+-1		╆┽	+-+	╅	+	₩	╂╼╂	┥
	CHICKEN		1717	<del>T ~ 1</del>	1	-	1 P 7	77	++	7	┽┤	┝╅┥	╫	+	<del>} -</del> }''	<u>चेल्य</u> ा	<del>pupi</del>	րոր	<del>"   </del>	┿	╅╅	╌┞┤	H-	╁╅	+1	+	+	++	++		╆╆╸	╁	٦
		1 x (0.00.0)	110	<del>, , , ,</del>	اردا.		<del>       </del>	.,,		<del>,,,   </del>	-H	H	╁┼	╆╂	╀╏,	ibuli	1	ti ti	11-1	+-	<b>† †</b>	$\top$	+	H	11	-	11	11	77		<del> -</del>  -	t-t	ᅥ
	HYCAL RADIOMICS	~ (7.74.0)	H	7	+			1		4	+	Н	<del>     </del>	Ħi.	i #	aruu.	111111	***	"	十	11	1		Ħ	+		+	11	++	_	++	H	ᅥ
	HEAT EXCHANGE	4	10	力力		-	1	++	++		+		1	1.1.	† †	min	tolo	titi	ᇜ	1		17	1	Ħ			1	11	++		$\vdash$	${\sf T}$	ᅥ
			Ħ	11	-1-1		┞╌╂╼┆	$\dashv \dashv$	-1-1	-11	-	$\vdash$	$\vdash$ $\vdash$	$\dagger$	17	*****	""i"	fΤ	77	_	17	$\top$	П	П	7		T	$\Box$	77	$\sqcap$	$\sqcap$	171	- 1
	CAYAWALL STREET A	REICE INSTA.	$\Box$										$\Box \Gamma$	$\Pi$	IJ		$\Box$	$\Box$		I	$\Box$	$\mathbf{T}$	Ш	$\coprod$	$\perp$		$\Pi$	$\Box$	IJ		$\Box\Box$		
	THERMSCOL	a# 3	# 7					$\Box$	$\Box \Box$		id L	$\Box$	$\Box$	$\Pi$	$\Box$ i	uluit	duku	1110	шП	$\perp$	$\Box$		$\Box$	П			П	$\Box$	$oldsymbol{\square}$	$\Box$	$\prod$	$\Box$	
	Asirilaini	11/11	4	3)		$\Box$		$oldsymbol{\square}$				$\Box$	$\Box$	$\Pi$	$\Box$		<u> </u>	վափ	ЩП		$\coprod$	$\perp$	Ш	П		Ш	Ш	$\Box$	П	$\perp \Gamma$	$\Box$	$\Box$	_
			$\Box$	Ш	$\perp$		Ш	$\perp$					П	$\Pi$		$\perp$	Ш-	$\sqcup$			44	4_	Ш	Н	┸	Ш	11	44	Ш		Ш	П	_
	DATA ACQUISITION	ZY55/41	44.	42	ш	Ц.	Ш	ш	$\perp$	ш	ш	Щ	⇊	1:1	1	mata	ици	١Ш	щ	-1-	14	┵	$\sqcup$	₩	4	LL	$oldsymbol{+}$	44	44	╙	₩	11	_
			H	44	$\dashv$		Ш	44	-1-4	$ \square$	<b></b>	₩.	₩	44	4-4	1		1.1.	4	-	++		┝	14	╇	1	4-4	44	44		┺	1.1	_
	OPTI-NE ALIENST	UP IN ETAJACUTATION	1	44	44	┝╁╌	$\sqcup$		+	$\Box$		<b>}</b> ├	╁╌╂╾	┵	╂┼	4040	ффu	ĮΨį	Щ		++		<b>}-</b> ∔-	╀		⊢⊢	1	44	-4-1	┝╌┡	₩	₩	_
			1,1		-14	$\vdash \vdash$	╁╌┨╌┤			-		╁╌╁╌	╁╌╂╴	1.+	+-1.	1.	1.1.	1.1			╁╃	+-	₩	┦┤	+	<del>}</del> }-	++	-4-4	4-1	┵	₩	╁╾╁	_
	SUPPORT TARKE	<del></del>	117.		-44	┝╼╂┈	-	-+-				╂═╂╼	╁┼	╅╌╁╴	┿╫	mim	փոփո	ֆոդ	₩-4		╅╾╂	╅	╀	┨┪	┿	₩	╅╾╁	┿	-1-1	┢	╂╼┿╌	╁┼	_
	PO-Adora CAME	4.1	(40	<del>.Ы</del>	+		HH	┰		H	┝┼╾	╁╆╴	╀┤	<del></del>	+ 1,	ш	1::	t.k		+	╁╅	┰	╂╂	╅╉	┽	<del>   </del>	+-+	++	╼┾╌┦	┢╾╋╼	╉╌╋╸	╁┼	_
	/ 52 / 54 - 54 - 54 - 54 - 54 - 54 - 54 - 54	,	154	74	+	Н	╀╂┥	+	+	-	┝┿╾	╂-	╂╼╊	╅	╍┢╾╌┦ <sup>╏</sup>	rrinish)	րար	ΨI¶	╨╂╌┤		╅╅	╅	╂╂	╂╂	╅	╂╌╂╴	╂╉	-+-	╌╂╌┦	╌	╁╂	+ +	_
	WIRRATION TEST	IYEFAM	100	47	-	$\vdash$	$H^-$	$\dashv$	H	$\vdash$	$\vdash$	+-	++	++	<b>†</b> †	++	<del>i k</del> e	kuti	10	-	++	+	<del>     </del>	++	┰	H	++	+	++	-	╫	+ +	,
	<del></del>		11	11	$\dashv$		11		ш		Н-	11	11	11	11	11	11"	1"1		$\top$	17		$\vdash$	11	十	H	+	$\top$	$\top$	$\vdash$	11	11	j-
	EARTH IR SIMUL	Taks	(41)	2.64	444							1 1	П			11:11:	dinda	iid	Ш		11	7	П	17	7	11	11		7		71	11	_
			$\coprod$				$\Pi$						П	$\coprod$	$\Box$	$\Box$	$\Pi$	$\prod$			$\prod$		$\Pi$	П	$\perp$	$\prod$	$oldsymbol{\Pi}$	$\Box$		$\Box$	П	$\Box$	ī
			П	$\perp$			$\prod$				$\Box$	$\coprod$	П.	$\Box$	$\Box$		$\perp \perp$	Ш			$\square$	$\Box$	$\Pi$		$\perp$	П	Ш	$\Box$	$\Box$	$\Box$	П	$\Box$	Ξ
			$\bot \bot$	ш		Ш	11	1		Ц.	Щ.	Ш.	Н	11	44	-11	11	11		Ц	11		П	П	1.	Ш	IJ	Ш	$\perp$		$\Box$	$\sqcup$	Ĺ
			1.1	1.1		11	$\bot \!\!\! \bot$	LL.	Ц.	L	Ц.	<b>↓</b> ↓	11	44.	44	44	11	44		ш	11	1	Ш	11	$\perp$	П	$\perp$	Ш	لنلب	Ш	11	11	<b>.</b>
├──			11	-		╁╁	₩	Ц.	- -	<del>     </del>	╀	11-	$\bot \bot$	-4-4-	4-4		11	11	-	Н	╜		₩.	44		╁	44	44	لبلبا	⇊	11	11	$\vdash$
			11	-	-	₩	₩	╙	╀	₩	1	11	╁╁	++	+	-	₩	╁╂	-	<b>├</b> ┼	+-1		H	44	-	1	44	44	لسلما	╁┼	++	4-4	⊬
	THOMELT ITEM	,	╂-┼	-	Н-	╌	╀╌	⊢┼┈	┨╌╂╌	╂╾╁╼	╁╅╾	╂╼╂╼	╁╁	++	╌┼	-1-1	╀╃	┧	-	┰	1-1	-	11	+1		╂╼╊	╌╂╼┤	$\dashv$	┢╌╄╌┤	┿	++	┥┥	⊦
		AVAILABLE	1,1	110.	<del>,</del>	<del>   -</del>	++	⊢+-	┪	┼-┼-	╅╌╉╌	╅╼╋╾	╅╅		┪╼┫	239 384 7	1.1.	+		╀	-{-{	+	╅╅	┿	+-	╊╼╋	┿	4		╆╌╂╴	++	+-+	H
<del> </del>	FIGUIA NA	4,4,54,4.	#7	$\rightarrow$	$\vdash\vdash$	++	++	+	┪	<del>                                     </del>	++-	++-	+ +	-	+-1	18 BE	الزلاب	44	-	╁┼	╅┥	+	╁╼╁	┿┥	-	╂╌┼	╌╂╼┥	-+-	┟┼┼	╆┿	++	╅	۲
	CALLOW PIOL	AUDILAUIT	╁╌┼	770.	-	╅╾╅╴	+	<u></u>	111(1)	1711	<del>   </del>	<del>   </del>	╁╁	++	+1	idat		1	-	<del> </del> −†∙	-1-1	-	++	╫	-	1 1	++	-+-		++	++	+-	r
			++	+	$\vdash$	1 +	<del>                                     </del>	11	TT.	11	1-1-	<del>                                     </del>	1-1	<del>     </del>	+-	THE PERSON NAMED IN	4	444	<b>""</b> —	<b>†</b> †	+-	-	1 +	+	+	† †	++	1	十	++	++	+-1	۲
	MAGNITIC TAPE	AURICABLE	╁╅	77.	1	11	11			1 1	<b>T</b> -T-	1	††	-+ +	1-1	+	1-1.	Ė	118	H	+		††	$\top$		++	+-	-	$\vdash$	††	11	-†!	۲
			† †	十	$\vdash$	††	11	<del>                                     </del>	$\sqcap$	11	11.	11	11	11	$\top$	11	1 1	7"	<u> </u>	††	4-4	1	11	$\top$	$\vdash$	11	++	_	<u> </u>	##	11	11	T
	POLAROID PILL	AUA	1-	2 14	4	$\sqcap$	11					$\Gamma$	11	11	_	9 11	161111	Kiii	11.6	T	-	$\Box$	11	. T	7	11	+	$\sqcap$	$\sqcap$	T	11		ľ
			11			$\Pi$	Ш	$\coprod$		$\Pi$	П		П		$oldsymbol{\square}$		$\prod$									11		$\Box$	П	П	П	. []	i.
			IJ			$\prod$	$\Box$	$\Box$	П		$\prod$	$\Box$	$\Box$	$\perp \Gamma$	$\Box$	$\Box \Box$	$\Box$			П	$oldsymbol{\perp}$		IJ	$oldsymbol{\mathbb{L}}$		$\prod$	$\Box$		$\prod$	$\Box$	$\Box$	_[_]	Į.
						П	$\downarrow \bot$	$\perp \Gamma$	$\perp$	$\perp$	$\Box$	+1	11		$\Box$	-	+	Щ	Ц.	Ц	$\Box$	$\Box$	$\prod$	Г	$\Box$	$\Box$	$\bot$	L	Ш	$\downarrow \downarrow$	$+$ $\Box$	4	Ļ
			11		H	+1	44	<b>↓ ↓</b>	₩	₽	₩	╁┼	┵┵	┵			44	$\perp$	Щ.	Н		$oldsymbol{\perp}$	$\downarrow \downarrow$	1	$\sqcup$	$\coprod$	╜	-	₩	₩	4	<b>_</b>	1
<b> </b>			1-4	-1-	⊢-	╁┼	+-	╁┼	╂╌╂╌	╁╌╂┈	++	++	+ +	-1-1		┝╌╂╼╅	╌╂╼╂	-4-4	<del>├</del> ─ <del>┟</del> ─	╀		₽₽	4-4	4-	<b>∤</b>	1		<b>├-</b> ├-	╁┼╴	<del>+</del> i	-	-}	į
		Lance 5	1,1		ᄔ	1-1-	1.1	┯┸┈	4	┵┵╁	11	1.1	╅┸			┝┸┩		┪╌	Ц_	ш	┰	<u> </u>	11	1	Ш	بب	لسلسا	حلبا	ـــــــــــــــــــــــــــــــــــــــ	₩	44		÷
1179 1 7	AD: C ATHICAM							t		Į									•	•				*·	×1 1	in gh	. r, S	e live	lute	No.	ì		
								_				rst	_		i pt			+-						4						. [	4		

				REL	IAB	ILITY			R	EVIS	10	NS		_CONFIG MGT
			,	APP	0 71	EDICTION	·			DESCRIPT			DATE	APPV'D
					+			XPERIM	ENTAL	RELEASE	ER/	922-16	7-11-74	SEN .
					-1				APPI	ENDIX S	_	O		
														· · · · · · · · · · · · · · · · · · ·
		,					7	rable	OF CO	ONTENTS				
										•			Page	<u>.</u>
			٠.		1.0	PURI	POSE C	F TES	r		•		1	
	<del>,</del>	·			2.0	SCOF	E OF	TEST	•				1	
					3.0	APPI	LICABI	LE DOC	UMEN	ITS .			1	•
	- 85				4. 0	PAR	MCIPA	NTS					1	
TI ON	SERIAL	NIN			5.0	EQUI	PMEN'	T REQU	ЛRED	-			S	
	S				6. 0	PRE-	TEST	VERIF	CATIO	ON			3	
	_	1			7.0	TEST	SET (	JP AND	ALIG	NMENT	•		6	
ICAT	€	4/14			8.0	THE	LAMS-	OPTICA	AL PR	OCEDURI	E		<b>V1</b> ".	
,	I TEM				9.0	POST	-VIBR	ATION	T-0 P	ROCEDU	RE		18	·
AP	2				10.0	DATA	SHEE	TS.	r	. :	i .		29	,
ART		<u> </u>			11.0	PROC	EDUR	E VARI	<b>ATION</b>	<b>1</b> S	-		47	
U P	λS	3			12.0	SIGN	OFF 9	HEET	-				48	
A	r AS							•		9.	•			-
NG.	NEXT													
DRAWING										<b>1</b>	TEC	T DATE.	<	
<u> </u>							•	. *			, ,		o 8-14-7	<b>4</b>
	ž	5 4 5 55									•			•
	PART	4							-			•		
		23									• .			
LIMI				VISE		MINIC NO.		20550		THE BI	INDI	X CORP	ORATIO	٧
SPE	CIF	IED	DII	IEN-		DRAWN CHECKED			AEROS	PACE SYST	EMS D	IVISION -	ANN ARBOR	MICHIGAN
\$10	NS /	ARE	IN	INCH	£3.	TRESS/WT			TITLE		. =			
MAT	ERI	AL:				DSGN SUPY PROJENGR		2-9-74	7	HERMAL		GEOS PHA PICAL TE	ASE B EST PROC	EDURE
	٠					JUAL CONT			SIZE					
	. 101		11 4 6			SYS SPT ISON APPL			A	0703	`	DRAWING N	A	REV X
'DR			ilas B	] ] c[	₩ [	NFG Customer			SCALE	<u> </u>	WEIG	TP 237	AU	of 48
				14 × 1 ( <sub>pr.</sub> 1	;	AND I DIETA	. , ,	<del></del>		·	1	<del></del>		S-1



J HO.	,	REY. HÓ.
TP23	74455	[ 
PAGE .	1	or <u>48</u>
 DATE	9 July	1974

#### 1.0 PURPOSE

The purpose of this test is to: (1) determine the optical performance of the LAGEOS Retroreflectors under simulated orbit environment conditions and (2) to verify that the results obtained from previously-conducted thermal/optical analyses are representative of retroreflector orbital performance.

#### 2.0 SCOPE

This document specifies the procedures and equipment necessary to perform the thermal-optical tests. A series of test sequences will be performed under varied conditions of atmospheric pressure, coldwall and test article temperature, and Earth IR and solar radiation, while observing, photographing and measuring intensity of retroreflector far field diffraction patterns. Selected conditions will be repeated after vibration testing to assess the effects of the dynamic environment on retroreflector performance.

#### 3. 0 APPLICABLE DOCUMENTS

LAGEOS Thermal/Optical/Vibrational Analyses and Testing Study Plan (Rev. B)

LAGEOS Phase B T/O/V Test Plan (Rev. B)

2374458 LAGEOS T/O/V Test Article

STM 1036 Operating Procedure for NRC 4x8 Vacuum Chamber

STM 1005 Tenny-Kold Pak Operating Procedure

STM 1019 Operating Procedure for Solar Simulator

STM 1017 Operating Procedure for HP Data Acquisition System

STM 1008 Operating Procedure for NesLab Temperature Control

--- Operating Manual for Zygo Far Field Diffraction
Instrument

#### 4.0 PARTICIPANTS

LAGEOS Engineering Representative Environmental/Quality Test Conductor E/QT Thermal-Vacuum Engineer E/QT Instrumentation Engineer



<b>.</b>	NO.		REY. HO.,
	TP237	4455	
٠.	PAGE	2	or <u>48</u>
	DATE	9 Jul	y 1974

#### 5. 0 EQUIPMENT REQUIRED

		•	. 1
	Part No.	*Serial	*Calib.
Manufacture	r or Model	No.	Dat 🗲
NRC	1/0	8509894	NB
=	C44-82-62		12-10-74
_			12-29-24
			1-12-25
mb	7.	•	N/A
RI Controls			5-22-75
			NA
•	NIA	NID	N/A
Genarco	ME-6	MA	N/A
BxA		N/A	N/A
BxA	2374453	•	N/A
BxA	2374454		N/A
BxA	N/A		N/A
Hy Cal			NIA
Hy Cal	544-1-02-NZ	44/95	MA
NA	14/19		N/A
EOA	P-104	403	N/A
NRC	751	50627	7-13-24
Buf	NA	MA	n/p
Supp.on	BSD-10886	· N/D	9-5-74
	<u> </u>	<u>~//8</u>	7-3-74
	-		
<del></del>			
	NRC Tenney HP Sanborn FI Controls Neslab Zygo Genarco BxA BxA BxA BxA BxA Hy Cal Hy Cal Hy Cal NRC	Manufacturer or Model  NRC Tenney HP Sanborn H-P RI Controls RJ4081 Neslab Zygo Genarco BxA 2374460 BxA 2374453 BxA Carrella N/A Hy Cal Hy Cal Hy Cal Hy Cal FOA NRC RICOM ME-6 P-104 NRC RICOM ME-6 RJ4081 R	Manufacturer   Or Model   No.

<sup>\*</sup>To be completed prior to testing. Equipment substitutions and additions shall be listed above.



m	NO.		REV.	HO.
(4)	TP23	74455		
, ,	PAGE .	3	OF	48
* * .	04.75	9 July	v 19	 74

,		
6.0	PRE-TEST VERIFICATION	
6. 1	Test Setup	7/2474
6.1.1	Install the No. 2 Earth IR Simulator in the 4x8 chamber as shown in Figures 1 and 7.	
6.1.2	Install the thermal-vacuum test fixture, 2374460, in the 4x8 chamber at the location shown in Figure 1 and in	
	accordance with Figures 2, 3 and 4. Do not install the LAGEOS Test Article.	
6.1.3	Connect the fixture thermal assembly cooling lines to the actuator tube.	~
6.1.4	Perform helium leak check of entire fixture cooling circuit.	
6.1.5	Install window feedthru assembly, 2374453, on port at rear of chamber. The Zygo window will not be installed at this time.	v
6.1.6	Install a standard chamber window on the window feedthru. This window is to have a thermocouple, #28, attached to its inside surface at the approximate center.	
6. 1. 7	Connect the following thermocouples, via a feedthru to the outside instrumentation: window hood TC, manipulator tube TC, window TC, thermal assy TC, Coldwall TC's.	
6.1.8	Connect the window hood and manipulator heaters to their respective power sources.	
6. 1. 9	Install the (2) radiometers, as shown in Figures 1 and 7. Connect their cooling lines, thermocouples, and signal leads per 10.1 Instrumentation Summary.	
6.1.10	Install the No. 1 Earth IR Simulator as shown in Figures 1 and 7.	
6. 1. 11	Install the Coldwall door panel and connect its thermo-	V



#### LAGEOS

#### THERMAL-OPTICAL TEST

6	HO.   REV. H	10.
(3)	TP2374455	
•	PAGE OF	48
	DATE 9 July 197	<b>-</b>

6.1.12	Connect roughing pump to the fixture roughing port.	
6.1.13	Connect the Tenney heat exchanger to the fixture cooling circuit.	<u> </u>
6. 1. 14	Connect the Neslab temperature controller to the radio- meter cooling circuit. Connect radiometer signal outputs to the outside instrumentation.	<u>`</u>
6. 2	Verification Procedure	
6. 2. 1	Start fixture roughing pump and chamber vacuum pumps per STM 1036.	
6. 2. 2	When the chamber is sufficiently evacuated, start the Tenney heat exchanger, the Neslab temperature controller, and the chamber coldwall.	V
6. 2. 3	Adjust the Neslab temperature controller to maintain the radiometer sink temperatures at $38 \pm 2$ °C.	1240,/25/7
6. 2. 4	Adjust the Tenney heat exchanger, per STM 1005, to stabilize the fixture thermal assembly at $-30 \pm 5$ °C.	~
6. 2. 5	Apply power, via Variac #1, to the Window Hood heater and adjust as necessary to maintain the window thermocouple, #28, reading at 24 ± 2°C.	~
6.2.6	Apply power, via Variac #2, to the manipulator tube heater and adjust as necessary to maintain the manipulator tube temperature at $24 \pm 2^{\circ}$ C.	V
6. 2. 7	When all environmental parameters have stabilized, record the following data:	
	Chamber pressure Window Temperature Window Heater Manipulator Temperature Manipulator Heater Thermal Assy Temperature Coldwall Average Temperature	
	7/25/7	<b>'</b> H



1 NO.	REV. NO.
TP2374455	
PAGE 5	of <u>48</u>
DATE 9 July	1974

6.2.8	Obtain background readings for the radiome	eters.	
	Padiometer No. 1 45 ( ) 2 71	.76	
	111V	150	

6.2.9 Apply power, via Variac #3, to the No. 1 Earth IR simulator. Adjust so that radiometer No. 1 indicates 0.5 mv (1/20 S.C.) radiant input from the simulator. Record the simulator voltage. Turn off the IR simulator.

61.76 VAC

6.2.10 Apply power, via Variac #4, to the No. 2 Earth IR simulator. Adjust so that radiometer No. 2 indicates 0.5 mv (1/20 S.C.) radiant input from the simulator. Record the simulator voltage. Turn off the IR simulator.

34.08 VAC

6. 2. 11 Return all environmental parameters to ambient conditions.

TILA 4 PER SIMIOBE.

CAUTION: Maintain Tenney and Neslab operation until the coldwall warms up to avoid freezing of internal lines.

7/25/54

- 6. 2. 12 Remove the instrumented window from the window feed thru.
- 6. 2. 13 Remove the fixture thermal assy and the fixture mounting assy. (items 23 & 28, Figure 3) from the test setup.

7/29/74



HO.		REV. NO.	
TP23	74455		
PAGE .	6	of <u>48</u>	_
DATE	9 July	v 1974	

**	7.0	TEST SETUP AND ALIGNMENT	•
7 TEM 17	7-1	- Install Zygo window on the window foodthou-	1/
	7. 2	Install alignment targets on the Zygo window and on the chamber door center window. See Figure 5.	0/34
	7.3	Set up the boresight laser.	
÷	7.4	Adjust the boresight laser positioning so that its beam is centered on the center aperture of both alignment targets.	-
·	,	NOTE: After positioning is complete, avoid disturbing the setting of the boresight laser.	
	CAUTION:	PROTECT PERSONNEL FROM DIRECT OR REFLECTED IMPINGEMENT OF LASER BEAM ON THE EYES.	
	7.5	Verify that retroreflectors A, B and C have been installed	de:
. 17		in the Test Article Panel, and that the thermal assembly has been shimmed to place the retroreflector front faces on the manipulator rotating axis. (See Figures 1 and 9.)	
76 M	7.6	Verify that thermocouples been installed on the ALSEP retroreflectors X and Y and on the Fest Article Panel and Thermocouple Fixture per Figure 6.	
	7.7	Verify that retroreflectors D, E and F are installed in the Test Article Panel. (See Figure 9).	
	7.8	Mount the first surface mirror, using double-sided Scotch tape, on the Test Article panel so that it is centered over retroreflector A.	
	7.8.1	Mount the position target, using Scotch tape, on the Test Article block so that it is centered over retroreflector B.	
٠,	7.9	Set the manipulator rotationally so that it is indexed to a solar angle of 0 degrees. Set the vernier drive to 0.400 on the micrometer.	



### THERMAL-OPTICAL TEST

60	HO.	REV. HO.
(8)	TP2374455	<u></u>
	PAGE 7	or <u>48</u>
		1074

	7.10	Attach the Test Article/Thermal Fixture/Support Fixture assembly to the actuator tube so that the Test Article front face is vertical and facing the chamber door. Use a spirit level to obtain the front face verticality.	7/30/24
	7.10.1	Place the spacer block, 2374469-1, on the outside end of the support tube. Verify that the boresight laser spot is horizontally centered on the position target for the B retroreflector.	<u> </u>
	7.10.2	If horizontal positioning in 7.10.1 is not correct, move the collar assembly axially on the actuator tube to obtain correct horizontal positioning. Verify Test Article front face verticality as in 7.10.	
	7.10.3	Remove the spacer block.	
	7.11	Secure the Test Article thermocouple leads to the manipulator fixed part allowing a flex loop for a minimum of 3000 of rotary freedom.	
1 <sup>1</sup>		NOTE: All operations hereafter for rotating the manipulator from solar to field view, or vice versa, will be "over the top".	* 
	7.12	Rotate the manipulator from 60° below horizontal solar angle to 60° below horizontal field view angle to verify the freedom of thermocouple lead wires.	
	7.13	Set the rotary index to the 0 degree field view point.	-
	7.14	Turn on the boresight laser.	<u>+</u>
	CAUTION:	PROTECT PERSONNEL FROM DIRECT OR REFLECTED IMPINGEMENT OF LASER BEAM ON THE EYES.	



@	HO.		186	V. <b>MO.</b>
<b>W</b>	TP23	7445	5	
	PAGE _	8,	_ OF .	48

Brospace	THERMAL-OPTICAL TEST	PAGE 8 OF 48
Systems Division	lon	DATE 9 July 1974
7.15	Adjust the rotary vernier to vertically center the re- flected laser spot on the Zygo window alignment targ Record the vernier setting.	•
	Rotary Zero Vernier Reading	
7.16	Verify that the reflected laser spot is horizontally will/4 inch (0.3°) of the alignment target center.	thin
7.17	If horizontal centering is not within 1/4 inch, proceed follows:	las
7.17.1	Adjust the rotary vernier to 0.400.	MA
7.17.2	Change shims(item 19, Figure 3) between the thermal fixture assy (item 23) and the support fixture assy (it 28) to obtain horizontal centering of the reflected lase spot within 1/4 inch (0.3°) on the Zygo window alignmentarget.	em er
	NOTE: Shims to be added and removed equally to rot the Test Article about its center line.	<b>at</b> e
7.17.3 Than 2	Loosen the support fixture saddle clamp and turn the support fixture/thermal fixture/Test Article assemble on the manipulator tube so as to vertically center the reflected laser spot within 1/4 inch on the alignment to get. Re-tighten the saddle clamp.  Repeat 7.6.1 and 2.10.2	•
7.17.4	Remove the boresight laser from its position in the teset up; its usage is completed.	
11	ser appears to contibuered.	<del>-</del> .

THE

Install the Far Field Diffraction Instrument (FFDI) on the leveling plate, 2374454, and position it on a wooden top work bench as shown in Figure 1.

7.19 Set manipulator axes for viewing the first surface mirror



**Systems Division** 

#### LAGEOS THERMAL-OPTICAL TEST



TP2374455

Date 9 July 1974

#### Item 18

7.18	Adjust the boresight laser positioning so that its beam is centered on the center aperture of both alignment targets.	8/5
	NOTE: After positioning is complete, avoid disturbing the setting of the boresight laser.	
CAUTION:	PROTECT PERSONNEL FROM DIRECT OR REFLECTED IMPINGEMENT OF LASER BEAM ON THE EYES.	
7.18.1	Verify that Addendum I, assembly of the test article/fixture and installation of thermocouples has been completed.	<u> </u>
7.18.2	Mount the first surface mirror, using double-sided Scotch tape, on the Test Article panel so that is is centered over retroreflector A.	
7.18.3	Mount the position target, using Scotch tape, on the Test Article block so that it is centered over retroreflector B.	
7.18.4	Attach the test article/thermal fixture assembly to the support fixture using shims as shown in Figure 10.	_
7.18.5	Connect the cooling lines from the thermal fixture to the actuator tube.	4
7.18.6	Secure the Test Article thermocouple leads to the manipulater fixed part, allowing a flex loop for a minimum of 300° of rotary freedom.	
	NOTE: All operations hereafter for rotating the manipulator from solar to field view, or vice versa, will be "over the top".	2/0 
7.18.7	Rotate the manipulator from 60° below horizontal solar angle to 60° below horizontal field view angle to verify the freedom of thermocouple lead wires.	L8
7.18.8	Verify that the optical node of retro-reflector A is located on the actuator rotary axis as follows.	



### Aerospace Systems Division

#### LAGEOS THERMAL-OPTICAL TEST



TP2374455

Page 8B of 48

Date 9 July 1974

Itan 18

7.18.9	Sat up a transit annumentally fire fact as a sure of sure	al das
7.10, 7	Set up a transit approximately five feet away in front of the 4' x 8' chamber so that it is located on the chamber center line.	2/3/14
7.18.10	While viewing retro-reflector A thru the transit, rotate the actuator ± 20 degrees about the 0° solar angle position, observing for apparent motion of the retro apex.	
7.18.11	Add or remove shims, at all four support spacers A-D (see Figure 10) equally, to minimize or eliminate the apparent retro apex movement. Enter shim changes in Figure 10.	
7.18.12	Place the spacer block, 2374469-1, on the outside end of the support tube. Verify that the boresight laser spot is horizontally centered on the position target for the B retro-reflector.	1/2"
7.18.13	If horizontal positioning is not correct, move the collar assembly axially on the actuator tube to obtain correct horizontal positioning.	NA
7.18.14	Remove the spacer block.	
7.18.15	Set the rotary index to the 0 degree field view point.	<i>L</i>
7.18.16	Turn on the boresight laser.	
CAUTION:	PROTECT PERSONNEL FROM DIRECT OR REFLECTED IMPINGEMENT OF LASER BEAM ON THE EYES.	
7.18.17	Adjust the rotary vernier to vertically center the reflected laser spot on the Zygo window alignment target.	
	Rotary Zero Vernier Reading 0.252	_
7.18.18	Verify that the reflected laser spot is horizontally within 1/4 inch (0.30) of the alignment target center.	•75 ## \$##



#### Aerospace Systems Division

## LAGEOS THERMAL-OPTICAL TEST

No.	nėv. No.
TP2374455	
Page 8C	of <u>48</u>
Date 9 July	1974

Itan 18

7.18.19 If horizontal centering is not within 1/4 inch, proceed 8/5/74 as follows: 7.18.20 Adjust the rotary vernier to 0.400. 7.18.21 Change shims (item 19, Figure 3) between the thermal fixture assy (item 23) and the support fixture assy (item 28) to obtain horizontal centering of the reflected laser spot within 1/4 inch (0.3°) on the Zygo window alignment target. Enter shim changes in table of Figure 10. NOTE: Shims to be added and removed equally to rotate the Test Article about its center line. 7.18.22 Loosen the support fixture saddle clamp and turn the support fixture/thermal fixture/Test Article assembly on the manipulator tube so as to vertically center the reflected laser spot within 1/4 inch on the alignment target. Re-tighten the saddle clamp. Repeat 7.18-12, 7.18.13 and 7.18.14. 7.18.23 Repeat Step 7.18.17 and record the new rotary zero reading. 0.252 7.18.23 Remove the boresight laser from its position in the test set up; its usage is completed. 7, 18, 25 Install the Zygo window on the window feedthru. 7.19 Install the Far Field Diffraction Instrument (FFDI) on the leveling plate, 2374454, and position it on a wooden top work bench as shown in Figure 1.

Set manipulator axes for viewing the first surface mirror.

7.19.1



#### ospace Systems Division

# LAGEOS THERMAL-OPTICAL TEST

	NO. REV. HO.
(3)	TP2374455
ST	PAGE 9 OF 48
	DATE 9 July 1974

		* *
7.20	Adjust the leveling plate position, height, and leveling screws so that both the incident and reflected FFDI spots are centered on the Zygo window alignment pattern.	8/6/79 0100h
	NOTE: It may be necessary to rotate (index) the Test Article away from, then back to, the zero view angle in order to differentiate between incident and reflected spots.	A.
7.21	Verify that the FFDI incident spot is centered on the alignment target within ± 1/16 inch.	<u>~ + ;</u>
7.22	Verify that the FFDI reflected spot is centered on the alignment target within ± 1/4 inch.	<u>- + (</u>
7. 23	Remove the mirror and position target from the Test Article.	• •
STEM 17 7.24	Connect the cooling lines from the thermal assy to the actuator tube. Perform a bellion in the check of the cooling circuit.	
17.25 Item 5	Install the superinsulation blanket on the thermal fixture assembly.	
	NOTE: Use care to avoid damaging the thermocouple leads from the Test Article.	* 1
	DO NOT GET FINGERPRINTS OR OTHER CON- TAMINATION ON THE RETROREFLECTORS.	
7.26	Verify that the radiometers do not interfere with the rotational freedom of the manipulator assy and the Test Article thermocouple leads.	~
7.27	Connect window hood heaters, manipulator heaters, and Earth IR heaters to their respective Variacs outside the chamber and to the DAS. See Data Sheet 10.1	





PAGE 10 OF 48 DATE 9 July 1974

7.28	Connect all thermocouples to the thermocouple reference oven/DAS, per Data Sheet 10.1.	
7. 29	Connect the radiometer signal outputs to the DAS and to the chart recorder, per Data Sheet 10.1.	
7.30	Perform verification/continuity check of all power circuits and data channels.	· // // // // // // // // // // // // //
7. 31	Remove alignment targets from chamber window.	
7.32	Close chamber door and locate and connect the Arc Lamp Solar Simulator.	
7.33	Verify that the test setup is complete.	2/74



#### LAGEOS

#### THERMAL-OPTICAL TEST

HO. 9	REV. NO.
TP23	74455
PAGE .	11 or 48
DATE	9 July 1974

Item 28

#### THERMAL-OPTICAL PROCEDURE

A series of Thermal-Optical tests are to be performed as summarized in Figure 8. Section 10.2, Test Condition and Data Log, specifies the planned test conditions and optical data for each test. Actual test conditions and optical data will be entered in Section 10.2. The test article is shown in Figure 9.

Each test is a discrete element in the series; however, environmental conditions common to preceding tests may be maintained without re-cycling the environmental control systems. The sequence of tests 3 thru 9, Figure 8, may be altered by the Test Conductor.

The following temperature stabilization criteria shall be used as guidelines in conducting the series of thermal-optical tests. All criteria apply to ALSEP retroreflector, X and Y, temperatures.

- a. Setting up initial test conditions; 2°C/Hour
- Item 6
- b. Taking optical data; stop and restabilize if radial and axial temperature gradients change more than 10%; e.g., a 2.0°C gradient goes beyond 1.8 or 2.7°C.
- c. Restabilization after gradient change as in (b); return to original radial and axial gradients within  $\pm 0.1$ °C and to original temperature within  $\pm 5$ °C.

For verification of the scale of FFDI images during the tests, place the reference retroreflector in the laser beam, between the FFDI and the chamber window, and obtain optical data. Number the photograph and record on appropriate data sheet in Section 10.2. Perform this test at the following times:

Prior to start of test No. 1
After test No. 4
After test No. 9
Prior to test No. 10
After test No. 12
Prior to test No. 13
After test No. 14





#### LAGEOS

### THERMAL-OPTICAL TEST

PAGE 12 OF 48

DATE 9 July 1974

8.1	Turn on electrical power to all test instruments and recorde Allow adequate warm-up time before starting tests. Do not apply power to Variacs I thru 4.	rs. 8/6/1
8. 2	Set DAS operating controls per STM 1017. Initiate one data printout.	
8.3	Adjust the Sanborn recorder on the radiometer channel for a sensitivity of 1.0 mv/centimeter with 10.0 mv at center scale.	~
8.4	Test No. 1 Isothermal/Ambient	
8. 4. 1	Test conditions are to be at ambient. Initiate one DAS data printout.	_
8.4.2 Fee 8.4.2.1 8.4.3	Log actual test conditions in Section 10. 2, Test No. 1 Data Sheet.  Sheet.  Character for the first state of the parties of the section of t	+
8. 4. 4	Obtain, from the DAS printout, a single set of retroreflector temperature readings and enter in the Test No. 1 Data Sheet.	
8. 4. 5	Remove and rotate retroreflector C in the Test Article Panel, about its axis and reinstall in the 80 degree orientation angle (as shown in Dwg. No. 2374458).	8/6/29
	CAUTION: No not touch, mar or contaminate the retro-	
8.4.6	Install door coldwall and connect its thermocouple.	-
8.5	Test No. 2 Isothermal/Vacuum	<del></del>
8. 5. 1	Start the fixture roughing pump and the chamber vacuum pumps, per STM 1036. Do not start the coldwall, fixture & window heaters, and IR Simulators.	0714 has



### aystems Division

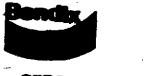
#### LAGEOS



#### THERMAL-OPTICAL TEST

PAGE 13 OF 48

DATE 9 July 1974 When the chamber is evacuated to a pressure less than 1 x 10-6 torr, enter the actual test conditions in Section 10.2, Test No. 2 Data Sheet. 8.5.3 Initiate one DAS data printout. 8. 5. 4 Obtain optical data as indicated by the Test No. 2 Data Sheet. Number the photographs sequentially (continuing from the last photo number in 8. 4. 3) and enter the numbers in the Data Sheet. 8.5.5 Obtain, from the DAS printout, a single set of retroreflector temperature readings and enter in the Data Sheet. 8.6 Test No. 3 Thermal/Vacuum 8.6.1 Initiate DAS data printout at 10 minute intervals. 8.6.2 Start the Tenney Heat Exchanger per STM 1005 and adjust for a Test Article Panel temperature of +30 ± 2°C. Start the Nesiah temperature bath per STM 1008 and adjust 8. 6. 3 as needed to maintain the radiameter temperature at 38 ± 2°C Turn on Variac #1 and set to 9.58 VAC. Refer to paragraph 8. 6. 4 6. 2. 7, Window heater voltage. Turn on Variac #2 and set to 14.99 VAC. Refer to paragraph 8. 6. 5 6. 2. 7, manipulator heater voltage. Readjust as needed to maintain the manipulator temperature at  $24 \pm 5$ °C. 8.6.6 Initiate coldwall operation. 8.6.7 When all environmental parameters have stabilized, set DAS to print channels 11 thru 68 at 10 second intervals.



ercepace Systems Division

## LAGEOS THERMAL-OPTICAL TEST

но.		REV. NO.
TP23	74455	
PAGE .	14	of <u>48</u>
DATE	0 11	y 1974

8.6.8	Obtain optical data as indicated by Test No. 3 Data Sheet.	
	When retro temperature stabilization degrades beyond the	.'
	specified limits, (see paragraph 8.0) stop data-taking and	
	restabilize temperatures.	
8. 6. 9 N	Reset the DAS to print all channels at 10 minute intervals during restabilizing.	
8, 6, 10	Perform 8. 6. 7 thru 8. 6. 9 repetitiously until all optical data have been obtained.	
8.6.11	outs and enter in Test No. 3 Data Sheet. Number all FFDI	
	photographs and enter photo numbers in the Data Sheet.	
8.7	Test No. 4 Thermal/Vacuum	
8.7.1	Set/verify the following:	
•	a. DAS printout at 10 minute intervals.	
	a. DAS printout at 10 minute intervals. b. Tenney/Test Article Panel temperature per Data	
	Sheet	
•	c. Neslab /Radiometers at 38 ± 2°C	
	d. Variat #1/Window Hood Heater at proper voltage 565 \$.64	
	e. Variac #Z/Manipulator Heater at proper voltage 554 \$1.15 / 14.9; f. Coldwall operating 551 \$1.14	Z VA
8.7.2	When all environmental parameters have stabilized, per	
0	Test No. 4 Data Sheet, obtain a radiometer No. 1 back-	
	ground reading and enter in the Data Sheet.	
8.7.3	Deleted.	
•		
8.7.4	Deleted.	
•		
		_



#### rospace Systems Division

### LAGEOS THERMAL-OPTICAL TEST

7	HO.	REV. HO.
÷	TP2374455	
	14A	or 48

			DATE	9 July 1974
	8. 1	Turn on electrical power to all test instruments and re Allow adequate warm-up time before starting tests. Description of the power to Variacs 1 thru 4.	corde	278.
	8. 2	Set DAS operating controls per STM 1017. Initiate one printout.	data	-
	8.3	Adjust the Sanborn recorder on the radiometer channel sensitivity of 1.0 mv/centimeter with 10.0 mv at center scale.	for a	
	8. 4	Test No. # Isothermal/Ambient	<del></del>	8/7/74
	8.4.1	Test conditions are to be at ambient. Initiate one DAS printout.	data	1132
	8. 4. 2	Log actual test conditions in Section 10.2, Test No. 1	)ata	1607he
8	8.4.2.1 8.4.3	Sheet. Offer on FFDI VEErficeton photo using the Este Retended in the Number photo & esting members in Testing accordance with the FFDI Operating Manual, obtain optical data for the retroreflectors at the field angles	Revel	Steet
		indicated. Number the photographs sequentially and entered the numbers in the Test No. 1 Data Sheet.	er	2/8/79 -1430 h
_	8. 4. 4	Obtain, from the DAS printout, a single set of retroress temperature readings and enter in the Test No. 2 Data s	ector Sheet	× 1833 he
•	8.4.5	Remove and rotate retroreflector C in the Test Article about its axis and reinstall in the 80 degree orientation (as shown in Dwg. No. 2374458).	Panel angle	
		CAUTION: No not touch, mar or contaminate the retro- reflector surfaces.		
	8.4.6	Install door coldwall and connect its thermocouple.		8/7/74
	8.5	Test No. 21sothermal/Vacuum	-	
	8.5.1	Start the fixture roughing pump and the chamber vacuum per STM 1036. Do not start the coldwall, fixture & wind	pum;	8/1/74

heaters, and IR Simulators.



### rospace Systems Division

### LAGEOS THERMAL-OPTICAL TEST

NO.	REY, NO.
TP2374455	
14.8 PAGE 35	or <u>48</u>
DATE 9 July	1974

VEW & SH

8.5.2 When the chamber is evacuated to a pressure less than  $\frac{2 \times 10^{-5}}{922 ha}$  torr, enter the actual test conditions in Section 10.2, Test No. 17

8.5.3 Initiate one DAS data printout.

1922 hes

8.5.4 Obtain optical data as indicated by the Test No. 2 Data Sheet.

Number the photographs sequentially (continuing from the last photo number in 8.4.3) and enter the numbers in the Data Sheet.

8/8/74

8.5.5 Obtain, from the DAS printout, a single set of retroreflector temperature readings and enter in the Data Sheet.

2011

8.6 Test No. 3 Thermal/Vacuum

8. 6. I Initiate DAS data printout at 10 minute intervals.

8.6.2 Start the Tenney Heat Exchanger per STM 1005 and adjust for a Test Article Panel temperature of +30 ± 2°C.

8.6.3 Start the Neslab temperature bath per STM 1008 and adjust as needed to maintain the radiometer temperature at 38 ± 2°C

8.6.4 Turn on Variac #1 and set to <u>9.6</u> VAC. Refer to paragraph 6.2.7, Window heater voltage.

8.6.5 Turn on Variac #2 and set to 15 VAC. Refer to paragraph 6.2.7, manipulator heater voltage.

Readjust as needed to maintain the manipulator temperature at  $24 \pm 5$ °C.

8.6.6 Initiate coldwall operation.

8.6.7 When all environmental parameters have stabilized, set DAS to print channels 14 thru 25 at 10 second intervals.



<b>—</b>	NO.	<b>[</b> ,!	REÝ. M	0.
<b>リ</b>	TP237	1455		
				,
	PAGE	40 0	<u> </u>	8
				ſ
	DATE	9 July	197	4

•		
8. 6. 8	Obtain optical data as indicated by Test No. 3 Data Sheet. When retro temperature stabilization degrades beyond the specified limits, (see paragraph 8.0) stop data-taking and restabilize temperatures.	
8. 6. 9	Reset the DAS to print all channels at 10 minute intervals during restabilizing.	NA
8.6.10	Perform 8.6.7 thru 8.6.9 repetitiously until all optical data have been obtained.	<u>N/A</u>
8, 6, 11	Obtain retroreflector temperature data from the DAS print- outs and enter in Test No. 3 Data Sheet. Number all FFDI photographs and enter photo numbers in the Data Sheet.	
8.7	Test No. 4 Thermal/Vacuum	
8.7.1	Set/verify the following:	9-9-74
	a. DAS printout at 10 minute intervals.	
	b. Tenney/Test Article Panel temperature per Data Sheet	
	c. Neslab /Radiometers at 38 ± 2°C	
	d. Variac #1/Window Hood Heater at proper voltage	· v
	e. Variac #2/Manipulator Heater at proper voltage	V
	f. Coldwall operating	
8.7.2	When all environmental parameters have stabilized, per	
- ,	Test No. 4 Data Sheet, obtain a radiometer No. 1 back-	

ground reading and enter in the Data Sheet.

8.7.4 Deleted.

Deleted.

8.7.3



<b>5</b>	NO.		REY	. HO.	
	TP23	74455	Ĺ. <u>.</u> .		-
	PAGE .	1/5	0F	48	; ==
ļ	DATE	9 Jul	v 10	74	

8. 7. 5	Turn on the Sanborn/radiometer recorder.	2/9/74
8.7.6	Set the manipulator for the required sun angle.	V
8.7.7	Start the Arc Lampsper STM 1019, and adjust for 1.0 solar constant (S.C.) as indicated by radiometer No. 1. Adjust as needed to maintain 1.0 S.C. during stabilization.	
8.7.8	When all environmental parameters have stabilized, set the DAS to print channels 14 thru 25 at 10 second intervals.	~
8.7.9	Obtain optical data as indicated by Test No. 4 Data Sheet. When retro temperature stabilization degrades beyond the limits, (see paragraph 8.0) stop data-taking and restabilize temperatures.	<u></u>
8.7.10	Reset the DAS to print all channels at 10 minute intervals during restabilizing.	<b>L</b>
8.7.11	Perform 8.7.6 thru 8.7.10 repetitiously until all optical data have been obtained.	1/2
8.7.12	Obtain retroreflector temperature data from the DAS print- outs and enter in Test No. 4 Data Sheet. Number all FFDI	
<b>8.7./3</b> 8.8	photographs and enter photo numbers in the Data Sheet.  Afficiate. Number to plant the Reference of the Test No. 5 Thermal/Vacuum	8/9/2
8.8.1	Using the Test Conditions specified in Test No. 5 Data Sheet, repeat steps 8.7.1 thru 8.7.12.99 5.2.1 5.2.4 5.2.4 5.2.4	8/12/74
8. 9	Test No. 6 Thermal/Vacuum	
8. 9. 1	Using the Test Conditions specified in Test No. 6 Data Sheet, repeat steps 8.7.1 thru 8.7.4. 8.2 2017 hes	8/9/24
8. 9. 2	Set the manipulator for viewing the No. 1 Earth IR Simulator.	



но.		1884	254. HO.	
TP23	74455			
PAGE.	16	OF _	48	
DATE	9 Jul	l <b>y 1</b> 9	74	

	8.9.3	Turn on Variac No. 3/Earth IR Simulator No. 1 and adjust for 1/20 S. C. as indicated by Radiometer No. 1.
	8. 9. 4	Repeat steps 8. 7. 8 thru 8. 7. 12. \$2.28 \$2.7.11 \$2.7.12 \$2.7.12 \$2.7.12
	8. 10	Test No. 7 Thermal/Vacuum
	8. 10. 1	Using the Test Conditions specified in Test No. 7 Data Sheet, repeat steps 8. 6. I thru 8. 6. 11.
	8.11	Test No. 8 Thermal/Vacuum
	8.11.1	Using the Test Conditions specified in Test No. 8 Data Sheet, repeat steps 8.7.1 thru 8.7.12. 8.7.7 8.7.9 8.7.9 8.7.1
٠	8. 12	Test No. 9 Thermal/Vacuum 8.7.18 8.7.18 8.7.12
	8.12.1	Using the Test Conditions specified in Test No. 9 Data Sheet, 8,7.3
Itan	8.12.2	repeat steps 8.9.1 thru 8.9.4.
	8.13	Return all environmental control systems to ambient con-
It	CAI 4	ditions, per STM 1036.
	8.14	Remove the Test Article Panel from the fixture, turn it end-for-end so that retroreflectors D, E & F are on the viewing axis, and re-install it in the fixture.
	8.15	Test No. 10 Isothermal/Ambient
	8. 15. 1	Using the Test Conditions specified in Test No. 10 Data Sheet,
Ka g	8.15. 2 8.16	repeat steps 8. 4. 1 thru 8. 4. 4.  Observe F DI Valle Station Physon using the Refraction edge 22/5  Reflector. Number the slots of state numbers in Text Data Shorts  Test No. 11 Isothermal/Vacuum
	8.16.1	Using the Test Conditions specified in Test No. 11 Data Sheet, 0053 repeat steps 8.5.1 thru 8.5.5.
<sub>KA</sub> 32	8,16.2. 8.16.2.	TEST No. 19 Theremal/Vacuum  1 Using the Test Conditions specified in Test No. 19 /8/4/20  Data Sheet represt stress 2.6.1 How 8.6.11.
(	(-30±2°C	8.6.1 <u>×</u> 8.6.5 <u>×</u> 8.6.9 <del>×</del> 8.6.2 <u>×</u> 8.6.6 <u>×</u> 8.6.10 <del>×</del> 8.6.3 <u>×</u> 8.6.7 <u>×</u> 8.6.11 <del>×</del> /4 8.6.4 <u>×</u> 8.6.8 <u>×</u>



24	HO.	REV.	NO.
	TP2374455	<u> </u>	
	PAGE 17	or _	48

Dyste	me Divis	ion				DATE 9 July	v.1974
	8. 17	Test No. 12	Thermal/Vacuum	1.6.1 <u>/</u> 8.6.2 <del>/</del> 8.6.3 <u>/</u>	8.6.5 X 8.6.6 X 8.6.7 TA	8.6.10 2	
	8. 17. 1	Using the Te	st Conditions spe	cified in Tes	st No. 12 Dat	a Sheet,	2/12/24
Sec. 8	8.17. Z 8.18	repeat steps	8. 6. 1 thru 8. 6. 1	is wave the	Acheerus .	esta-	
I	ten4	ditionar PE	R 5TM 1036,	•	:		230
_ ,	8.19	Remove the	Test Article Pane	el from the fi	ixture.	<u>~</u>	9/14/74
·		figur	in the existing the ration for addition completed.				
Stean Its	<sub>M</sub> 34	testing. I testing. I hopen the to the spe- ony functions	the Test Betse of deservations of march of march of march of a second mode. I see ans, but the march of march o	the six a SERENS TO ANNE TO	parrous strongfl med es-t barrens tongun si rk scrau	begue boll	
than 3: Than 3:	8.22 A	ridance of Emove the	de anodation de stantes. nonum sanam	du to pa	enous to	etine Loca Rove	9/1/27 1000

TOR OND 8.22 RE-BLUE TC 14 to RETROX FRONT force - 4/1



(23)
------

TP	237	44	55		

REV. NO.

9 July 1974

POST-VIBRATION THERMAL-OPTICAL PROCEDURE Stee 12 9.1 8/14/74 retroreflector E in the Test Article Panel ab and reinstall in the 100 degree orientation for shown in Dug. No. 2374458). See Figure 7. Install the Test Article Panel in the fixture so that retroreflectors D, E & F are on the viewing axis. Repeat steps 8.0 thru 8.3.

Milan Fils Vantication abote varie the Reference setto.

Reflector. Nombre the plate of setter ourbes in Test 13 Date Sheet. X

Test No. 13 Isothermal/Vacuum 1.3.1 9.4.1 Using the Test Conditions specified in Test No. 13 Data Sheet, repeat steps 8.5.1 thru 8.5.5. Part 16.21 Therend - Vac. Repeat 8.7.9 Item 38 9.4.2 Usive Trest Data shorts) 8.7.9 8.7.10 8.7.12 Test No. 14 Thermai/Vacuum 9.5 8/15/79 9.5.1 Using the Test Conditions specified in Test No. 14 Data Sheet, repeat steps 8.6.1 thru 8.6.11.

Output Frit when the plant photograms the reference return.

Reflected Number the plant states when a Test Data Shot.

Return all environmental control systems to ambient con-1408 . 9.5 Z ditions, PER STM 1036, 0800 Object Sections (Into data pag Pata Sharts 23 d 24 for Remove the Test Article Panel from the fixture. w 8/16/24 Inspect the Tast Asticle Assembly for Ctacm 4 9.8 VISUAL ENDERNCE of decendation due to previous testing. Verify the retrinestance se positive scare tichtamie tarque has 8/16/74 not Locassed from the specufied value.

LAGEOS

THERMAL-OPTICAL TEST

9.2.1 Repart Stars 8.0 Her 8.1

**9.5.3** 

9.2.2 Tast No. 20 Isothacool-Anbient. 9.2.2.1 Usive the Test Conditions space fixed in Test Nazo Data Sheet, expect stups

8.4.1, 8.4.2, 8.4.2.1, 8.4.3 \$8.4.4 1245

TUSERT-B

TEST NO. 22 THERMAL-VACUUM USING TEST DATA SHEET-22 REPEAT 8.6.1 THRU 8.6.11.

TOROSOIO

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR



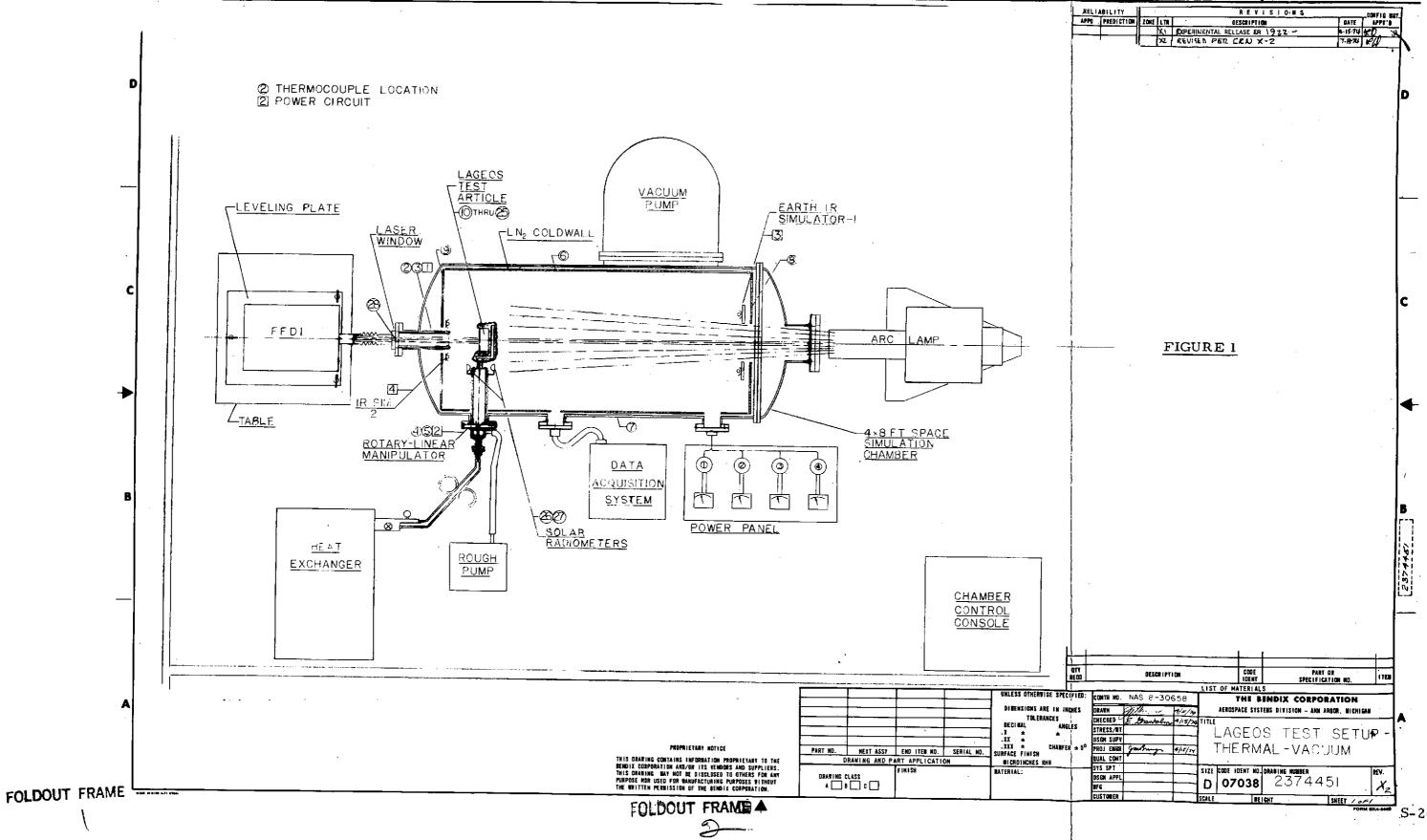
LAGEOS

THERMAL-OPTICAL TEST

TP2374455

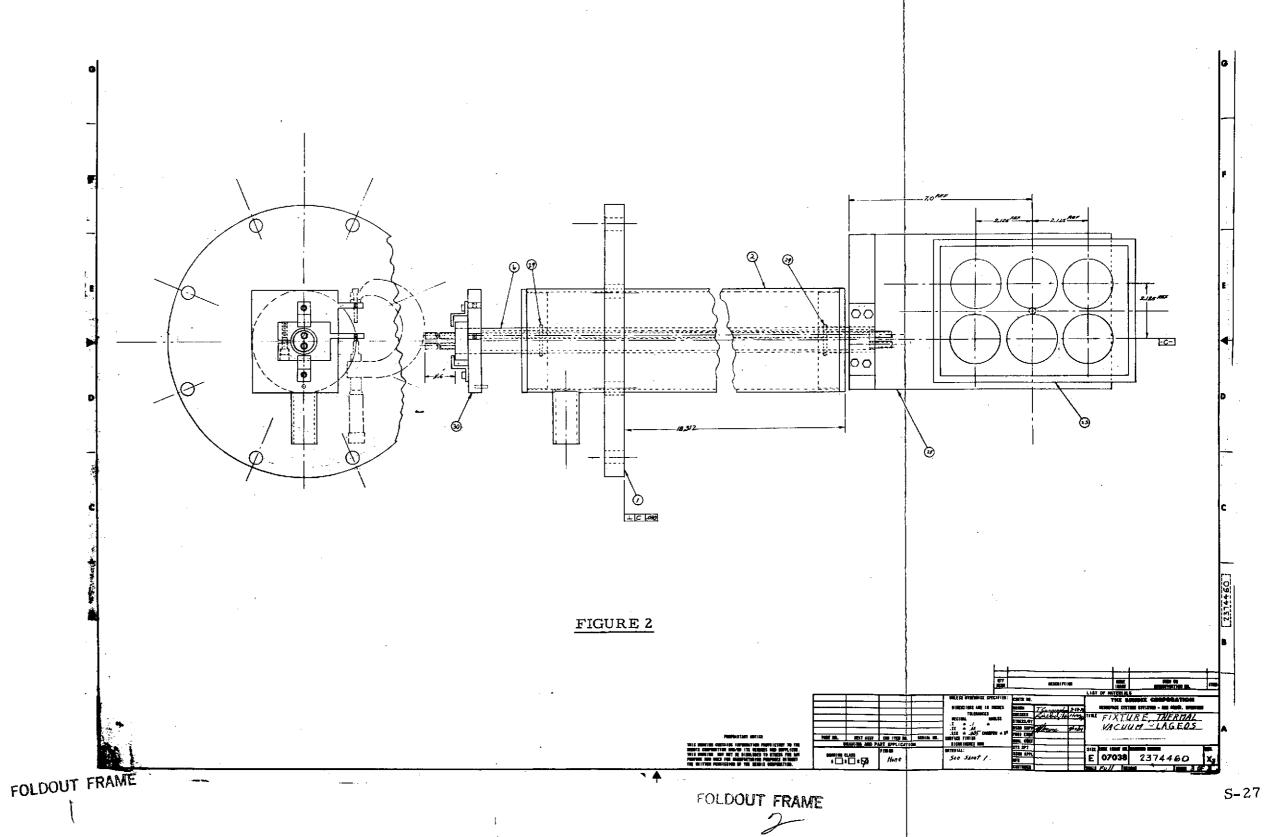
PAGE 19 OF 48

DATE 9 July 1974





REV. NO. TP2374455 DATE 9 July 1974

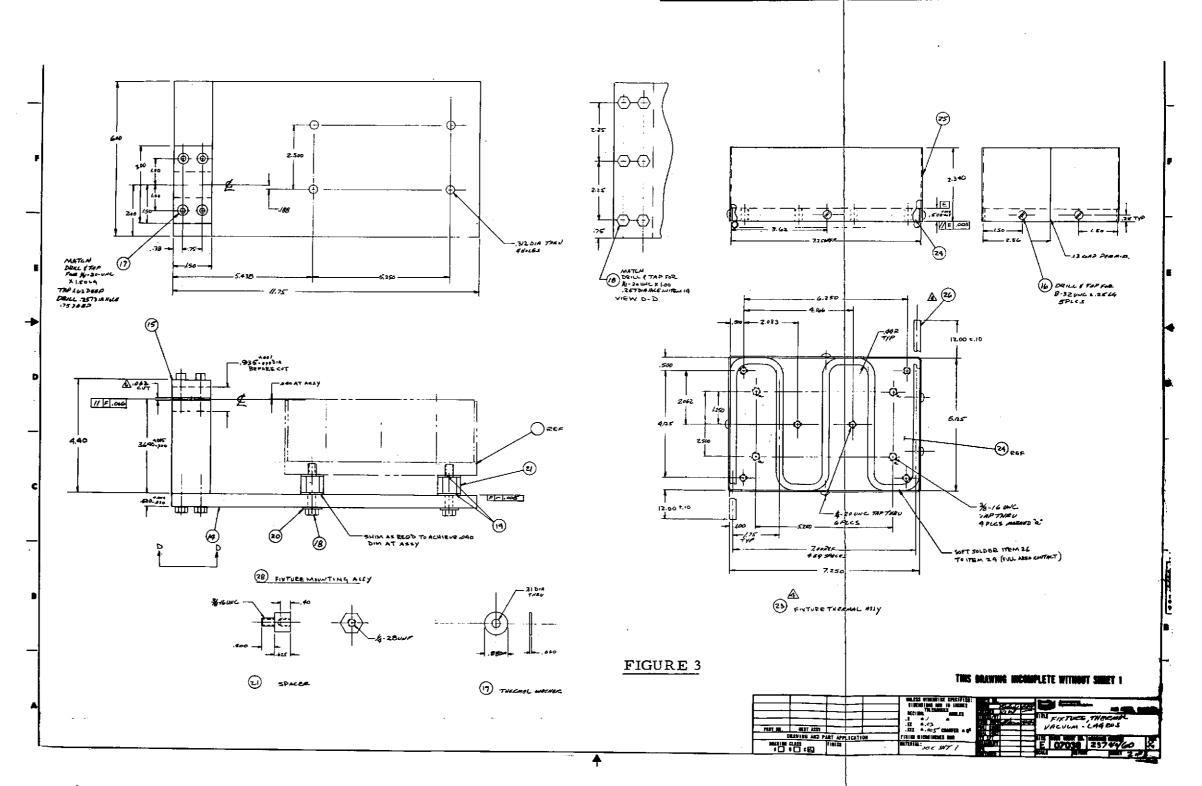




TP2374455

PAGE 21 OF 48

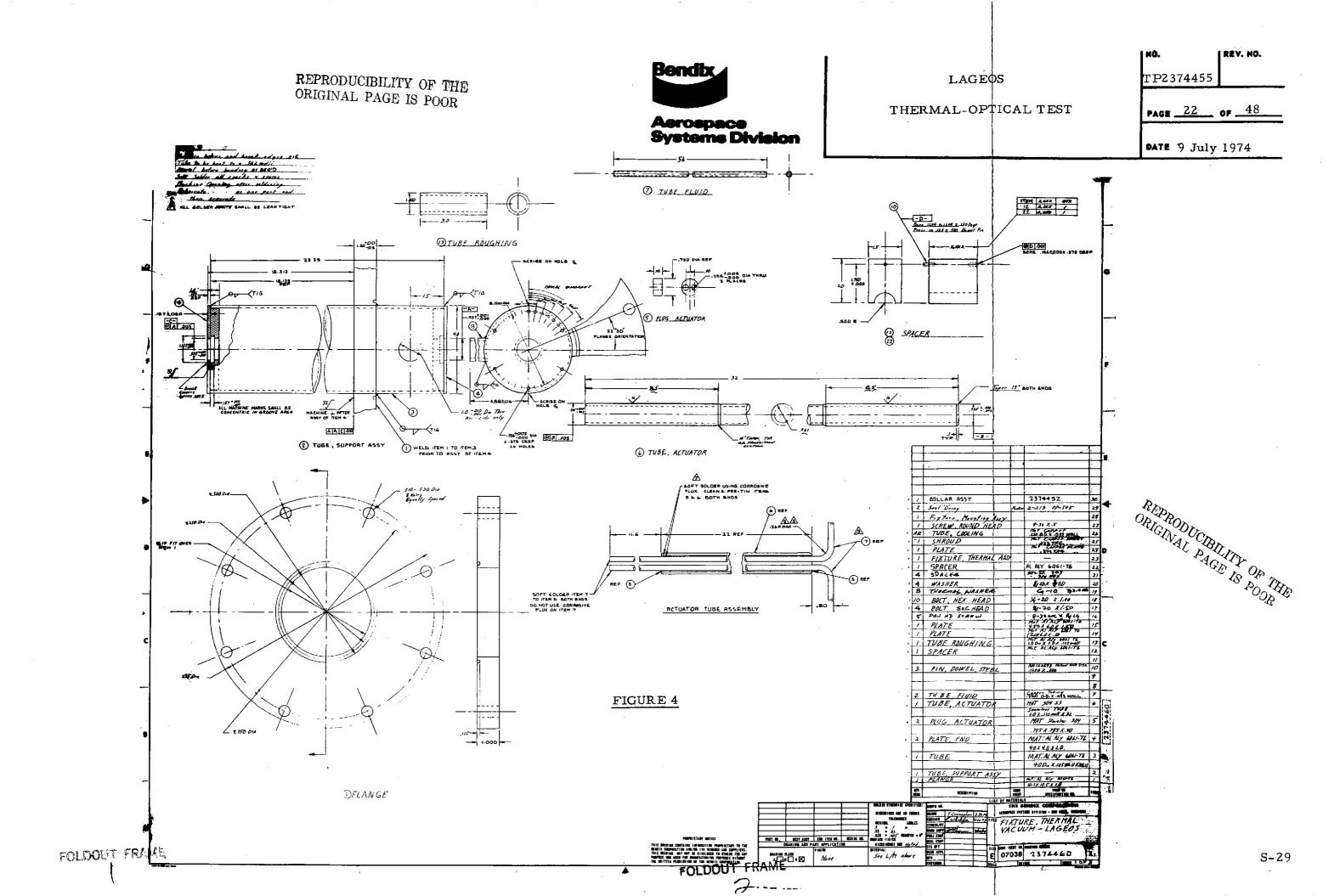
DATE 9 July 1974

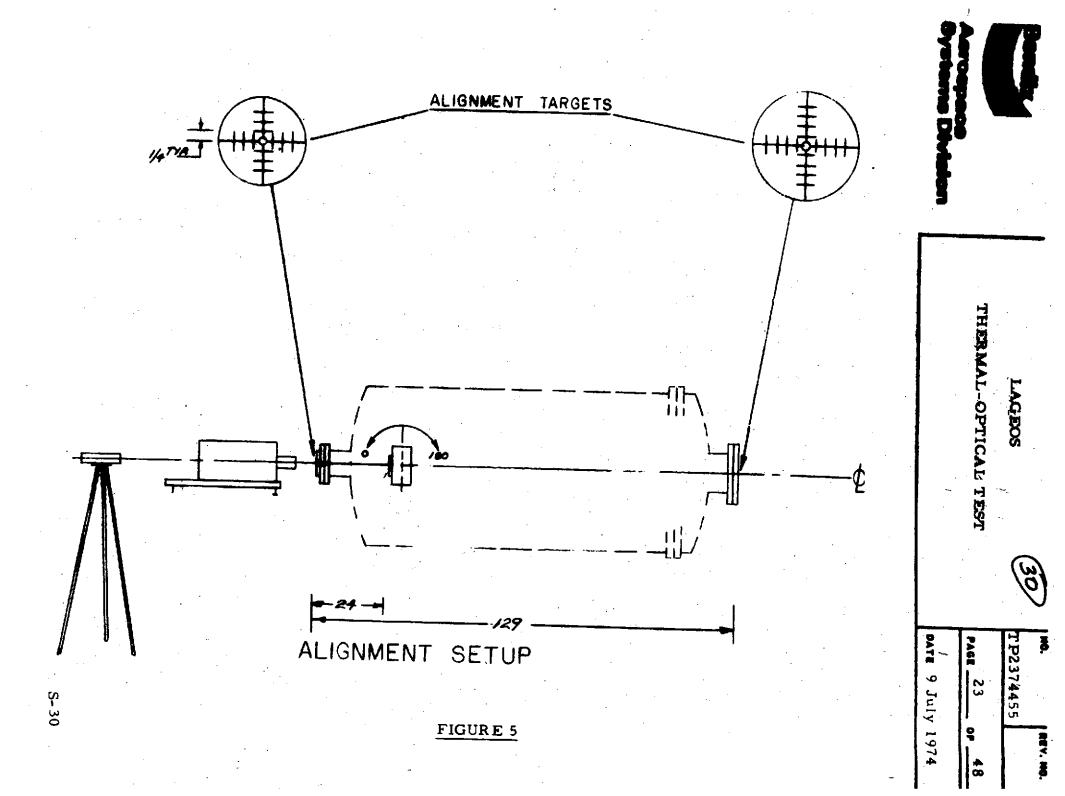


FOLDOUT FRAME

FOLDOUT FRAME

2----

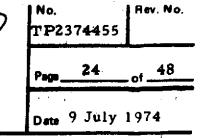


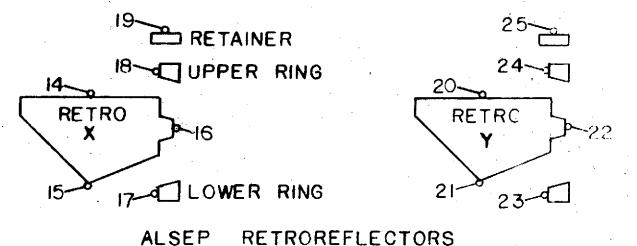




#### LAGEOS

#### THERMAL-OPTICAL TEST





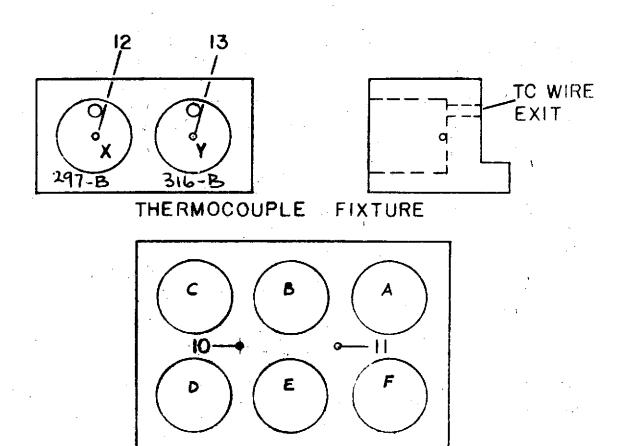
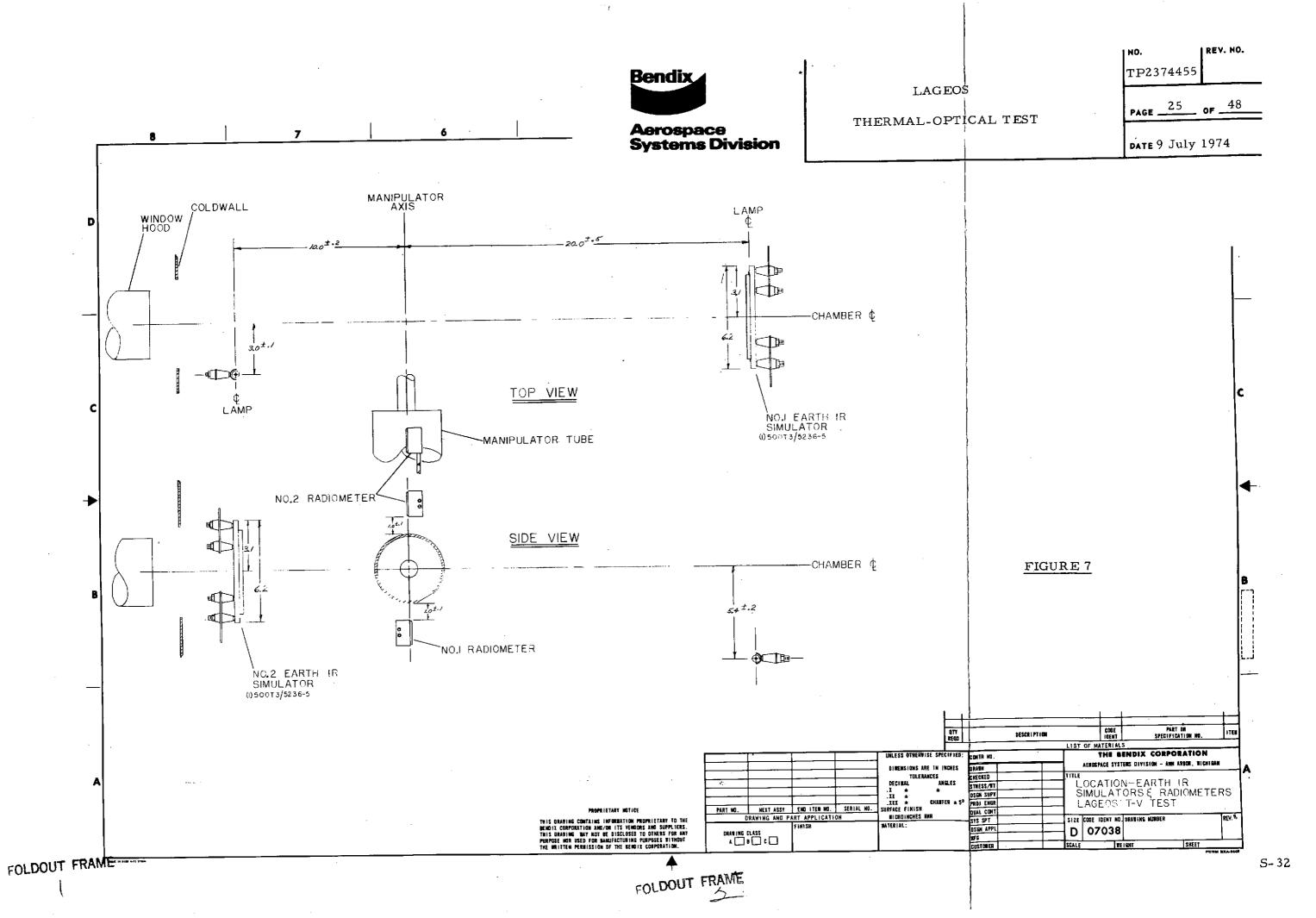


FIGURE 6 THERMOCOUPLE LOCATIONS

TEST ARTICLE PANEL





LAGEOS

THERMAL-OPTICAL TEST

I REV. NO. TP2374455

DATE 9 July 1974

FIGURE 8A

#### THERMAL/OPTICAL TEST CONDITIONS

		PARA.	Test	Description	A	Re B	etro O	rienta D	tion θ E	F	Vac Chamber Press (Torr)	Test Article Temperature	Chamber Cold Temperature	Solar Condition	Total Laser Field Angles Per Test	
		8.4	1	Iso/Amb	0	90	0				Amb.	Amb.	Amb.	N/A	8**	
		8.5	2	Iso/Vacuum	0	90	80			•	1 x 10 <sup>-6</sup>	Amb.	Amb.	N/A	15***	
<b>-</b> 8	16 Iso-Amb.7	8.6	3	Thermal/Vacuum	0	90	80				1 x 10 <sup>-6</sup>	+30°C	-185°C	No Sun	15***	
TVO	12 To 1		_15	Iso-Amb.	0	90	80							(No IR)	13	
#4007	18 Iso-Vac.	8. 7	4	Thermal/Vacuum	0	90	80				1 x 10 -6	+30°C	-185°C	l Sun Normal	8**	
		8. 8	5	Thermal/Vacuun.	0	90	80				1 x 10 <sup>-6</sup>	+60°C	-185°C	(No IR)  1 Sun +50°  (No IR)	1544 Ite	m 31
		8.9	6	Thermal/Vacuum	0	90	80				1 x 10 <sup>-6</sup>	+30°C	-185°C	No Sun l Earth IR	8** <b>R</b> Fn.	
		8.10	7	Thermal/Vacuum	0	90 ·	80				1 x 10 <sup>-6</sup>	-30°C	-185°C	No Sun (No IR)	15*** ORIGIN	ODUCBU
		8.11	8	Thermal/Vacuum	0	90	80				1 x 10 <sup>-6</sup>	~30°C	-185°C	l Sun Normal (No IR)	8**	ODUCIBILITY AL PAGE IS POOR
		8. 12	9	Thermal/Vacuum	0	90	80				1 x 10 <sup>-6</sup>	-30°C	-185°C	No Sun 1 Earth IR	8**	
		8. 15	10	Iso/Amb				60	40	20	Amb	Amb	Amb	N/A	8**	1
		8.16	11 19	Iso/Vacuum				60	40	20	1 x 10 <sup>-6</sup>	Amb -3¢ C	Amb -/85 c.	N/A No Sur/No I		Item 33
		8.17	12	The Emply X				60	40	20	1 x 10 <sup>-6</sup>	+30°C	-185°C	No Sun (No IR)	15*** I.	ten 32
				ION TEST				-								
	Item. 4	9.4 9.5	20 13 <b>21</b> 14 <b>22.</b>	Iso/Vacuum THEZMAL/VAC Thermal/Vacuum THERMAL/VAC		41-41		60 <b>60</b> .	100 100 100 100	20 20 20 20 20 20	1 x 10 <sup>-6</sup> 1 x 10 <sup>-6</sup> 1 x 10 <sup>-6</sup> 1 x 10 <sup>-6</sup>	Amb -30°C +30°C	And Amb - 185°C -185°C	N/A N/A NO \$un No Sun (No IR)	15 H**** ITE	M 37 1 38
	THE	n425	23 24	Iso/And	_	<b>.</b> .		60	100	20	mob	#90°C	Amb	NOSUN	>15	
	<b>y</b>	2	**	Iso/AnB		70					Anb	Anb	Anb	No IR	LITEM 39	
			Laser	Polarization: Linear in	Laser F	ield A	Angle	Plane	(Vert	ical Pla	ane)				TIEN 27	

= 0, +30, +15, -15, -30

\*\*\*\*D, E: = 0, +30, +15, -15, -30F: = 0

FOLDOUT FRAME 2

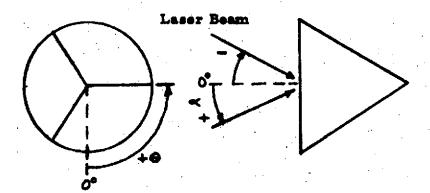
FOLDOUT FRAME

A, D:  $\alpha = 0$ , +30, +15, -15, -30 B, E:  $\alpha = 0$ , +15 C, F:  $\alpha = 0$ 

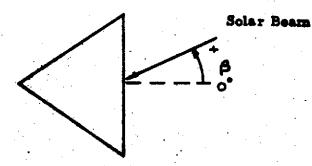
<sup>\*\*\*</sup>A, B, C, D, E, F:

9 July 1974

- © (a) - (c) - (c



Viewed from Laser Optical Window



Viewed from Solar Simulator

FIGURE 8B

SOLAR AND LASER FIELD ANGLES AND RETROREFLECTOR ORIENTATION

Bendix Aerospace Systems Div	vision ER192:		CHANGE R	EQUEST/NO			DL/C DCR/NNO.	
PROJECT LAGEOS	PART S	N EFFECTIVITY	CEI S/N EFFECT	IVITY /A	NEXT ASSY	N/A	Z 7 / 1 5 S D DWG NO. D SP 237445	EC NO. REV.
	OS TEST E ASSY	DRAW	CHANGEABILITY INGS ICATIONS		YES NO GHT DG+ H ORDERS D D NUALS D D	TEST PROC. QUAL TEST ACCEPT.TES TOOLS	YES NO HARDW DIS	POSITION
		NOTE		UMBERS IMPA				
WAS:	ATORQU	NOTE AL E ITEM 6	TO 1.0	± . 4 -: 0 2 ± 0.3	N= L85. /N-485,	arder Origi		
					Andrew Aug	ODUCIBIL!		
						TY OF THE		Then ?
								10 N
JUSTIFICATION:		WING ER					NGR	
INSTRUCTIONS: ENGR. COMPL. PROC. COMPL MFG COMPL.	INCORP. COMPL	#PL   00	CUSTOMER APPVL REDUTSTANDING ECN	O'D   MFC	3 INCORPINTO HOW ORP. INTO T.P.		PPROVED PPROVED AS NOTED	(13)
INCORPORATE:  DIN PRODUCTION  BETROFIT		DOCUMENT REC TCTO D TCTR D	DMTS. CHANGE ( D ECP D REC		CLASS	I CHAIR	ISAPPROVED	
PREPARED BY	STRESS/WT.	QUALITY	SYS. SUPP.	CONTRACT			7- 1/	1
OHECKED Denominal Readsocks	RELIABILITY	MFG	TEST	CMG:				

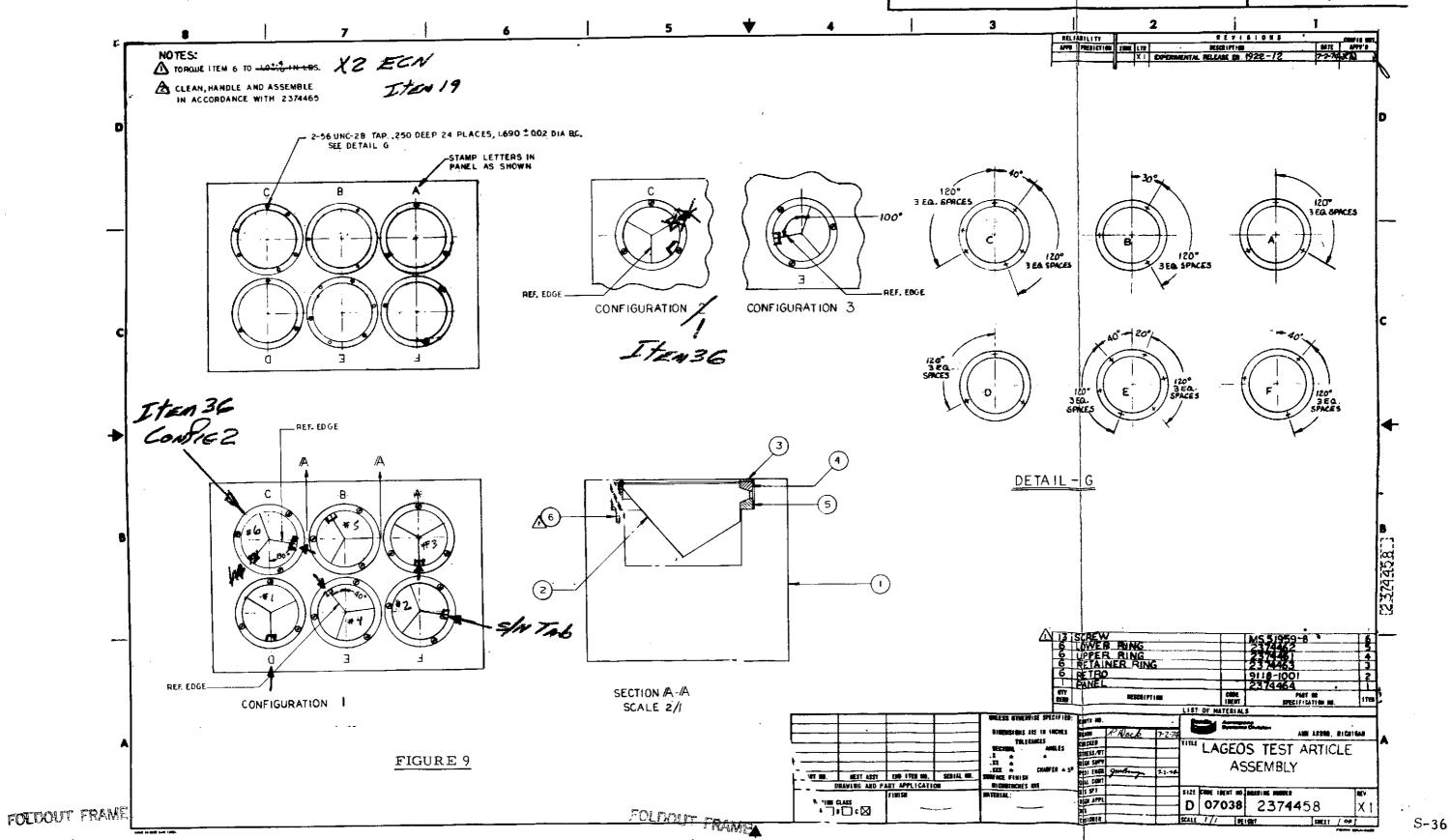


TP2374455

PAGE 28 OF 48

REV. NO.

DATE '9 July 1974





LAGEOS

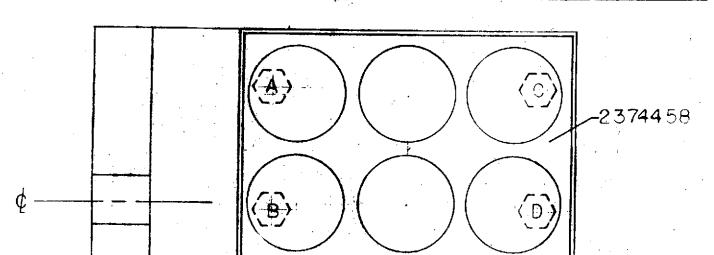
THERMAL-OPTICAL TEST

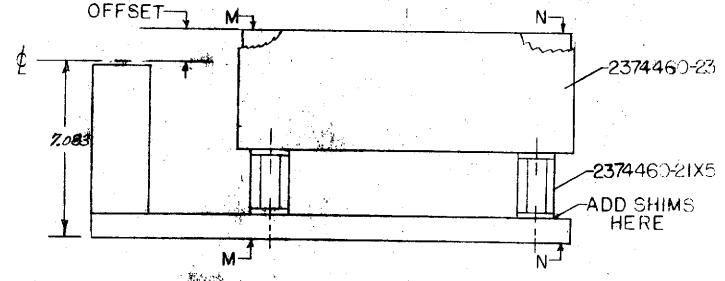
Itan 18

Page 28 A of \_\_\_\_\_

Date 7-29-74

2374455





WITH 2374460 SPACER: M-M= 7827; N-N=7.828 OFFSET=0.744

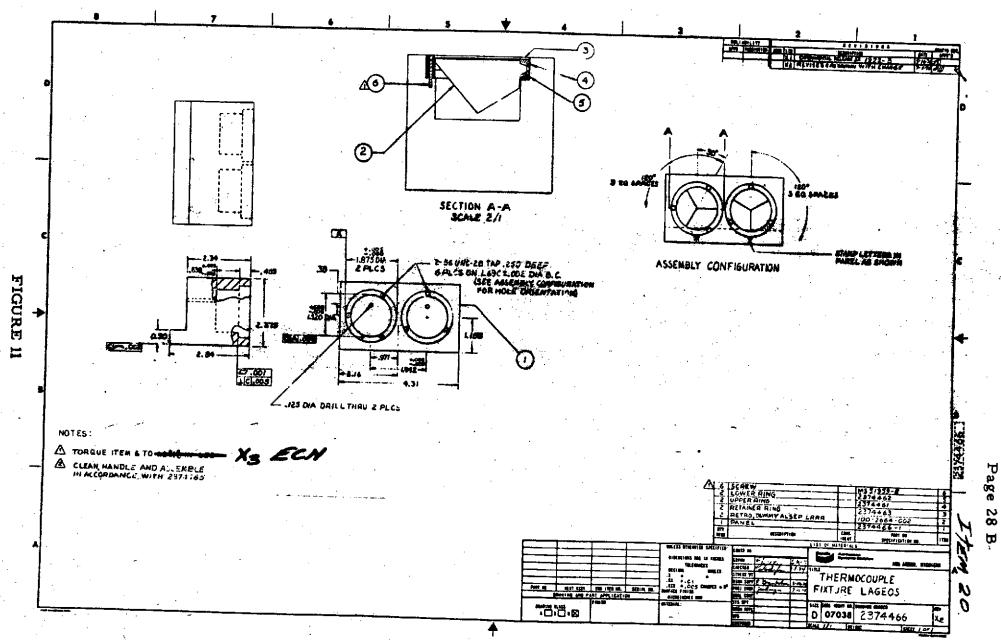
OPTICAL NODE NOMINAL 773 BELOW 2374458 SURFACE

SHIM TABULATION

OH HIM		<u> </u>			
SEQ	Α	В	С	D	7
	-015	-0/5	+015	-0/5	
2		معص	-05-	-0=	8/5/14 FINA
3	-080	.030	060	-060	Final
4	·				- Marie
5	· Ç	1			-
6					<del>-</del>
7					-
		<del> </del>			

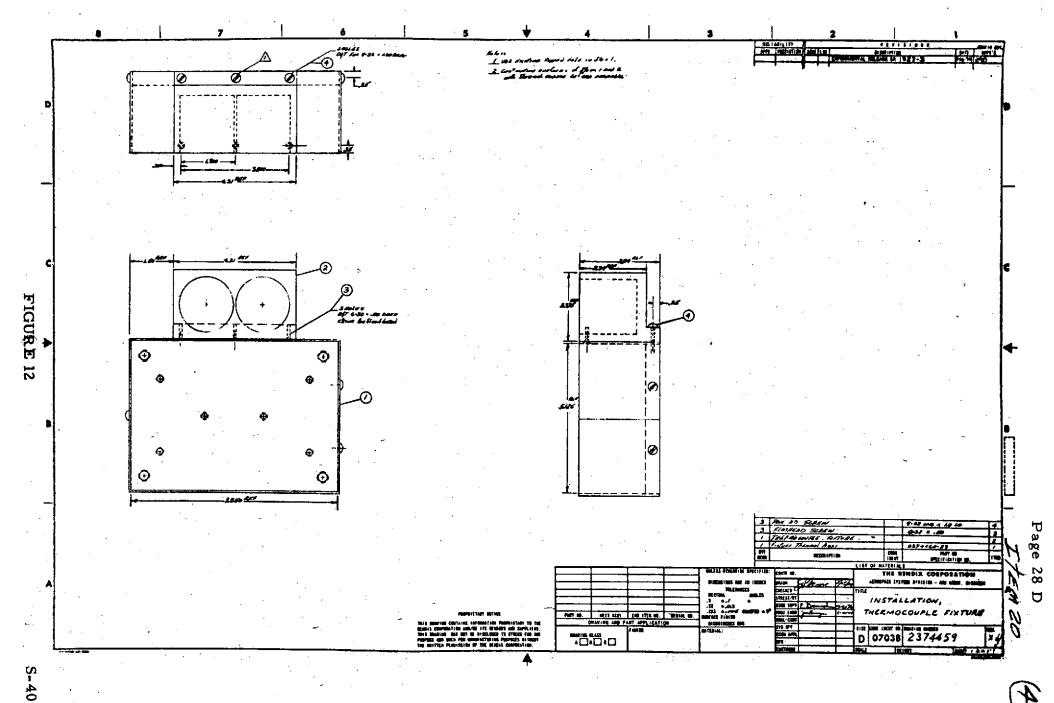
FIGURE 10 SHIM LOG

S-37



(30

Served Spaces	Bivision 7-51	74-19	CHANGE	REQUEST/NOT	ICE		DL/C DCR/NNO.	
PROJECT	PART	S/N EFFECTIVITY	CEI S/N EFFE	CTIVITY	SHEET	1 OF	BECN DSCN 2374466	y RE
TITLE	DO THE	NIA		NIA	NEXT ASSY	7	DWG NO. D SPE	
FIXTUR	25.3		IMPACTS: INTEROHANGEABILITY DRAWINGS SPECIFICATIONS SPARES	YES NO WEIGHT	RDERS D EX	TEST PROC. QUAL TEST ACCEPT.TEST TOOLS	YES NO HARDW. DISPO D	OSITION Alo ye
		dus it	ON AND OTHER DRAWING	NUMBERS IMPACTE FOLLOWS O + + + O - O		ORIGINAL PAGE IS POOR		Then 2
JUSTIFICATION:		ZAWING	ERROR			<b>REQUEST</b>		<i>n</i>
A 124 W.		SEQUEOTOS			• •	PROJ. EN	MASZATICS	
INSTRUCTIONS:		REGUESTOR DO NO	T WRITE BELOW THIS LIN	E			minings	
ENGR. COMPL. PROC. COMPL MEG COMPL. INCORPORATE: O IN PRODUCTION RETROFIT	TEST COMPL		CLISTOMER APPVL RI COUTSTANDING ECN INCORP, ON DWG. TREOMIS CHANGE CCP REC	CLASSIFICATION	CLASS I	□ АРР	ROVED ROVED AS NOTED APPROVED	(39)
PREPARED BY	STRESS/WT.	QUALITY	SYS. SUPP.	CONTRACTS	CUSTOMER	CHAIRMA	in Mulling	344
CHECKED	RELIABILITY	MFG	TEST	CNG / 1/2	1/2	DATE	7-81-7	Y



THERMAL-OPTICAL TEST

4

TP2374455

THERMOCOUPLES (CONT.)

216

9 July 1974

TP2374455

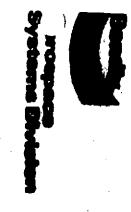
PAGE 30 OF

18

LAGE06

TC.	TC.			
Forethe	<u> </u>	LOCATION	DAS	NOTES
19		Retro Y Apex	21	Fig. 6, AT Axial, TC21 - TC20
20		Retro Y Edge	22	Fig. 6, AT Radial, TC22 - TC20
2/	23 2	Retro y Lower Mtg Ring	23	Fig. 6
22	24 ~	Retro Y Upper Mtg Ring	24	Fig. 6
23	25 2	Retro y Retainer Ring	25	Fig. 6
24	26 -	Radiometer #1	26	Sink Temperature
23	27 -	Radiometer #2	27	Sink Temperature
12	28	Verification Window	3	during Pre-Test Verif. Only
Item/	29	Ice Point Reference	0	
ENIS 8	30	Thread Future	10	Kerf testooly

<u>Item</u>	Identification	Data	Recorder Channel	Sensitivity
Variac	1	Window Hood Heater	DAS 28	VAC
Variac	2	Manipulator Heater	29	VAC
Variac	3	Earth IR Sim. #1	30	VAC
Variac	4	Earth IR Sim. #2	31	VAC
Radiomete	r 44045#1	Solar/IR Intensity	DAS 24/Chart 1	10 mv/s. C.
Radiomete	± <i>44/95</i> #2	IR Intens #2 Sim.	DAS 25	10 mv/s. C.
Blank	on R.	IsoLation Channel	DAS 32	حسم مید حسی



THERMAL-OPTICAL TEST

(4)

TP2374455

9 July 1974

S-43



PAGE 32 OF 48

DATE 9 July 1974

10.2 TEST CONDITION AND DATA LOG

Itam 28

		•
Item 22	TOUT COMMENTAL.	AS-RUN SUMMARY
7.TEM 4.6	TEGIOLUULNUE:	AS-KUN SUMMARY

172426	IEST SEQUENCE: AS-RU	N SUMMARY		
	Description		Start Time	End Time
1 1/9	I sotherwal - probudent	2/6/20	0500	0525
2 10/24	Isotharad-Vacuum	8/6/74	0714	1/33
4	Therapt - Vacuum	8/6/24	1139	TOR 04006
15 25	Toothorwood Brokent	8/4/24	2215	700 400G 2229
16 24/36	Isotherand- Ambico	1	8-7-74 701	1700
17 27/51	Isothe much Vaccoun	8-8-74	17/3	2011
	Therast-Vacuum	8-8-04	2020	8-9-74
9 67/76	T-V/IR	8-9-24	0330	0711
8 76/83	T-V/Solar	8-9-24	0730	M56
4 84/12	T-V/Solse	8-9-74	1500	2000
6 93/101	T-V/IR	8-9-74	2014	2330
	T-V (+30C)	8-10-74	0000	0226
18 118/133	Inthornal- Vocan	8-12-74	0845	
<u> 134/48</u>	Theand-Vocum	8-12-74		0910
10 Helisz	To Home work And	•		162/
	Isothernal-Bab	8-12-74	2/3/ 8-1	22/5 3-74
	Isothernol-Vocum	8-12-24	2220 84	
	T-V (-80°C)	8-13-74	0100	0723
	T-V (+30°C)	8-13-74	0740	1320
20 204/210	Isothernal-Amb.	8-14-74	1416	1728
				V - 2 - 0



TP2374455

PAGE 324 or 48

DATE 9 July 1974

10.2 TEST CONDITION AND DATA LOG THEN 28

Item 22 TEST SEQUENCE: AS-RUN SUMMARY

, , ,				
Test No. Proto	Description	<u>Date</u>	Start Time	End Time
20A 21/26	Isothernal-Bub	8-14-74	1730	1753
13 227/242	Isothernat -Vac	8-14-74	1816	2016
2/ 243/258	T-V (-30C)	8-14-74	2016	0152
14 259/224	T-V (+30C)	8-15-74	0200	0656
22 275/200	T-V ( 1900 ) +cox	8-15-74	0700	1430
23 291/306	Inthrend-Anb (DE	F) 8-16-74	0820	0854
24 307/321	Intherent-And (A, B)	C>8-16-74	1030	1052
<u> </u>				
NA	ANNULAR ARC SURVEY	8-13-74	1920	2045
· ***			•	
·				
		·		
		·		
·				
				,
·		<u> </u>	¥.	



LAGEOS (40)		2374455	
THERMAL- OPTICAL	. •	Page of	
TEST		Date 8-8-74	

237	744	55	1	
Page		· .	_ of _	
				,

10.2 DATA LOG

CALIBRATION CUBE PHOTOMETRIC

LASER = 0.94

FFDP ANNULAR = 0.17

RATIO ANNULAR: 0.18

RATIO FULL FIELD=1.22

\* CUBE ORIENTED WITH WRITING ON REAR SIDE HORIZONTAL AND UPWARDS

8-8-74 1815 HRS

Aerospace

LAGEOS
THERMAL-OPTICAL TEST

P2374455

om 9 July 1974

TEST CONDITIONS

MENT	PLANNED	ACTUAL AMB, AMB.	
SSURE	AMB		
TEMP- C	AM8		
MP - °C (avg)	AMB	AMB.	
ANGLE	N/A	N/A	
BACKGND	N/A	N/A	
INTENSITY	N/A	N/A	
BACKGND	N/A	N/A	
INTENSITY	N/A	N/A	
	BACKGND INTENSITY BACKGND	MENT PLANNED SSURE AMB TEMP-C AMB MP-C (avg) AMB ANGLE N/A BACKGND N/A INTENSITY N/A BACKGND N/A	

TEST DATE: 8-6-74 TEST TIME: FROM 0500 TO 0525
NOTES: (1) Photo #7 was se-taken (and label #7a) per

(2) optical data taken by E. Snowholm & J. May

(3) OPTICAL MERSUREMENTS INCLUDE BIAS OF . OOF (ON 10 X SCALE)

OPTICAL DATA F25 ARC SEC FUELD

OF HUAL	. DATA	- 23 //W 200 / / LICO					
		FIELD ANGLES					
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO	2	-3	4	5	6	
Α	LASER	1.27	1.29	1.28	1.28	1.29	
A.	FFDP-ANNULAR	0.20	0.08	3.005	,090	.047	
	RATIO-ANNULAR	0.16	0.068	· <i>০</i> ০3	.068	.035	
#	RATIO-FULL FIELD	0.79	0.42	.016	,44	.17	
	PHOTO NO.	7	8,	ŃΑ	NA	NA	
В	LASER	1.29	1.29	NA	NA	ŇΑ	
	FFDP-ANNULAR	,09	051	NA	NA	NA	
	RATIO-ANNULAR	.01	MAKE	NA	NA	NA.	
<i>_</i>	RATIO-FULL FIELD	.48	.20	N A	NA	NA	
	PHOTO NO.	9	NA	NA	NA	NA	
	LASER	1.29	ŃΑ	N A	NA	N'A	
C	FFDP - ANNULAR	,20	ΝA	NA	NA	NÄ	
	RATIO-ANNULAR	.15	NА	NA	NA	NA.	
Í	RATIO - FULL FIELD	.76	NA	NA	NΑ	NA	

RATIO = FFDP/LASER OUTPUT

FFDI METER READINGS

RETROREFLECTOR TEMPERATURES - ℃ (#0536)							
	R	TRO X		RETRO Y			
STABIL	FACE		ΔT RAD			AT RAD	
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22	
STRT	14	0	0	24	0	0	
I STOP							
2 STRT							
2 STOP							
3 STRT				,			
3 STOP							
4 STRT			- T			-	
4 STOP		:					
5 STRT							
5 STOP		,					
6 STRT			7				
6 STOP							
7 STRT							
7 STOP		1				₹ ·	
8 STRT			-				
BSTOP				,			

S-47

LAGE 03 THERMAL-OPTICAL TEST

	Na. TP2:	37445	Rav.	Na,
	Page.	34	_ of	18
•	Date	9 Jul	u 19	74

TEST NO.2

TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE		<1x10-6	1.3 4 10
TEST ARTICLE		AMB	AAG
COLDWALL TE	MP - C (avg)	AMB	And
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR SIMULATION	BACKGND		
	INTENSITY		

FFDI METER READINGS

OF TICK	- DAIA		+ 25	700 34	-/24		
; . }			FIE	LD ANG	SLES	•	<u> </u>
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO.	10	111	12	13	14-	1
<b>1</b> ^	LASER	1.39	1.38	1.38	1.38	1.38	1
A	FFDP-ANNULAR	.19	1004	,008	.090	.047	¥-
	RATIO-ANNULAR	.14	.064	.006	.062	.034	**
<u></u>	RATIO-FULL FIELD	.71	.38	.018	.39	15	
	PHOTO NO.	15	16	17	18	19	
	LASER	1,37	1.36	1.36	1.35	1.34	ĺ
В	FFDP-ANNULAR	.090	1048	101	.05	.009	l,
	RATIO-ANNULAR	1062	.036	.007	036	.007	**
*	RATIO-FULL FIELD	.44	.22	.023	.26	.02	**
С	PHOTO NO.	20	21	22	23	24	
	LASER	1.34	1.33	1.33	1.31		
	FFDP - ANNULAR	.17	.089	015	.087	1.30	*
	RATIO-ANNULAR	.13	.066	-01F	1065		**
<b>→</b> [	PARO FULL FIELD					_001	•

TEST DATE: 8/6/74 TEST THE	
NOTESI	- D. FROLESK

10.2 TEST CONDITIONS AND DATA LOG

RETROREFLECTOR TEMPERATURES - C RETRO X RETRO Y STABIL FACE AT AX AT RAD FACE AT AX DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 SEQ. DAS 14 ISTRT 21 21 ٥ 0 I STOP 2 STRT 2 STOP 13 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT 8 STOP O 21

Aerospace Systems Division

**LAGEOS** THERMAL-OPTICAL TEST

TP2374455

Date 9 July 1974

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 15

TEST DATE: 8/6/74 TEST TIME: FROM ZZOO TO ZZ30 NOTES: THIS ADDITIONAL TEST WAS PUN TO DETERMINE THE EXTENT OF LETTED OPTICAL PERFORMANCE DEGRADORION DUE TO CONTAMINATION OF THE GLASS.

44.006.81A5

ACTUAL

AMBIENT

AMBIBUT

76ºF

OPTICAL		#	25 AR	CSRC,	FIELD		
†		FIELD ANGLES					
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO.	25	-			_	
	LASER	1.04	1.04	1.06	1.10	1.10	
A	FFDP-ANNULAR	.10	· of	.007	059	7.031	
	RATIO-ANNULAR	10	.053	0.007	+054		
#	RATIO-FULL FIELD	252	.28	*.015	.3/	.//	
	PHOTO NO.	مسر		300 3			
<b>D</b>	LASER	1.70	1.10	1.10			
B	FFDP-ANNULAR	.46	-	*.077			
	RATIO-ANNULAR		×.036				
#	RATIO-FULL FIELD	-	.20	.43			
	PHOTO NO.						
0	LASER	1.10					
	FFDP - ANNULAR	./3					
	RATIO-ANNULAR	./2	·				
, <b>‡</b>	RATIO - FULL FIELD	.57					
	= FFDP/LASER OU	TPUT	FF	DI MET	ER RE	ADINGS	

PLANNED

RETROREFLECTOR TEMPERATURES - TO

		RETRO X			RETRO Y			
	STABIL. SEQ.	FACE DAS 14	AT AX DAS 15	AT RAD		DAS 21	ΔT RAD	
.	ISTRT				•			
	ISTOP		*.			<u>,</u>		
-	2 STRT							
	2 STOP							
:	3 STRT		7					
	3 STOP						<del></del>	
•	4 STRT							
	4 STOP							
	5 STRT			X				
	5 STOP					· · · · · · · · · · · · · · · · · · ·		
	6 STRT							
	6 STOP	19, 14		7				
Ĩ [	7 STRT					/		
	7 STOP							
I	8 STRT							
Ì	BSTOP	1					1	

TEST CONDITIONS

SOLAR

SIMULATION

EARTH IR

SIMULATION

CHAMBER PRESSURE

ENVIRONMENT

TEST ARTICLE TEMP- C

COLDWALL TEMP - C (avg)

ANGLE

BACKGND INTENSITY

BACKGND

INTENSITY

Bendix

.005 BMS

0

29

./3

Aerospace Systems Division LAGEOS
THERMAL-OPTICAL TEST

)	No. 1P2374455
	Page at
	Data Q Judia 1574

TEST CONDITIONS

ENVIRONMENT		PLANNED	ACTUAL
CHAMBER PRE	SSURE	Amb	
TEST ARTICLE	-	Buch	
COLDWALL TE	MP- ℃ (avg)	Prab	
SOLAR SIMULATION	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

10.2 TEST TEST DATE: 8-7-74 NOTES:	CONDITIONS AND DATA LOG TEST TIME: FROM 1/32 TO	TEST NO. /6
# 25 ARCSEC E.II	541	

FFDI VERIFICATION photo No. 26 28 Water 1607 bes

TOR 04008 OPTICAL DATA FIELD ANGLES RETRO DATA +15 +30 -30 PHOTO NO. 30 3/ 32 33 LASER .95 .95 .95 FFDP-ANNULAR .062 .007 .062 .032 RATIO-ANNULAR .064 .007 .063 034 #RATIO-FULL FIELD .37 .019 PHOTO NO. 34 35 LASER . 95 .95 FFDP-ANNULAR .065 .038 RATIO-ANNULAR 069 .039 #RATIO-FULL FIELD .46 PHOTO NO. 36 LASER 95 FFDP - ANNULAR ./3 RATIO-ANNULAR 14 FRATIO - FULL FIELD .7Z RATIO = FFDP/LASER OUTPUT FFDI METER READINGS

RETROREFLECTOR TEMPERATURES - TO								
		i	RI	ETRO X			RETRO	<del></del>
		STADIL			AT RAD		ΔΤ ΑΧ	AT RAD
	٦	SEQ.	DAS 14	DAS 15	DAS 16	DAS 20		DAS 22
<u> </u>	1	ISTRT	V					-
9 5 13 14	l	I STOP						
5		2 STRT		,				
/3		2 STOP				<i>\f</i> -		
4		3 STRT						
4	. (	3 STOP	O°	+15				
2	<b>mo</b> /	<del>4 STR</del> T. 4 STOP	1.17	.74	100	-15	- 30	ONE
×		4 STOP	1.16		.036	.74	. 33	AS
Fi	a44 ()	5 STRT	1.16	.68			_>_	В
Ra		5 STOP	3110					C
	1	6 STRT						
	ĺ	6 STOP				` .		
	1	7 STRT						
		7 STOP			$\rightarrow$	$\subseteq$		
	ţ	8 STRT	<del></del>					
	ł	8 STOP						
	. լ	3 3 1 01			<u> </u>	Į.		

Item 24

TEST CONDITIONS

TEST CONDITIO	NO		
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRES		212104	48×10-5
TEST ARTICLE		Anb	Anb.
COLDWALL TE	MP - °C (avg)	Anb.	Amb.
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

#.605 BIAS

OPTICAL DATA

		FIELD ANGLES					
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO.	37	38	39	40	41	
, , , , , , , , , , , , , , , , , , ,	LASER	.95	.94	.94	.94	.94	
H	FFDP-ANNULAR	.14	.066	.008	·25	200	
	RATIO-ANNULAR	.15		.008	.067	.035	
	RATIO-FULL FIELD	1.17	.73	.036	.74	.33	
	PHOTO NO.	42	43	44	45	46	
D	LASER	.95	.94	.94	.95	-94	
B	FFDP-ANNULAR	.074	:041	*.007	,038	*.009	
Ì	RATIO-ANNULAR	.083	.042	1.008	*.040	.010	
	RATIO-FULL FIELD	1.17	.69	×.049	.78	*.070	
	PHOTO NO.	47	48	49	50	51	
	LASER	.94	.94	.94	.94	.94	
C	FFDP - ANNULAR	.14	.070	+.013	*.082		
	RATIO-ANNULAR	15	.073	* .014	580.	-	
,	RATIO - FULL FIELD	1.15	.68	× .098	.82	.046	

RATIO = FFDP/LASER OUTPUT

FDI METER READINGS

Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

TP2374455	<b>7.6€. 140.</b>
Page	. 01
Data Q Lists	1074

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 617

	DATE: 8-8-					
NOTES	3 Chamber	PRESSUR	9-1.4×10-5	At End	of data	taking
	<u> </u>				, ,	

RETROREFLECTOR TEMPERATURES - C

	RETRO X			RETRO Y			
STABIL			AT RAD				
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22	
STRT						,	
I STOP					,,-		
2 STRT							
2 STOP							
3 STRT	l '						
3 STOP			7				
4 STRT							
4 STOP		X			X		
5 STRT							
5 STOP		7	· ·				
6 STRT		/			7	1	
6 STOP						1	
7 STRT				1			
7 STOP	/	20		[ ]			
8 STRT				7		1	
8 STOP	<i>Y</i>		9	<b>V</b>		1	

Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

P23744	155 Aw. No.
Pap 39	<u>48</u>
D== 9 J	uly 1 <b>974</b>

TEST CONDITIONS

I CO I OUNDING			
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE		< 1 X 10.6	1.6×10-7
TEST ARTICLE	TEMP- C	-30±2 <b>°</b> C	
COLDWALL TE	MP - °C (avg)	—185 <b>°</b> 0	-193°c
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

· · · · · · · · · · · · · · · · · · ·	10-2	TEST	CONDIT	TIONS	AND	DATA	LOG	•	TEST	NO. 7
TEST DATE:	8-9	-74	TEST	TIME	: FR	ж <u>2</u>	<i>20</i> т	0	23	7
					,					
<del></del>			·							
<u>.</u>		·····	<del> </del>					,		

Bias ous OPTICAL DATA FIELD ANGLES RETRO +30 415 DATA 0 +15 -15 -30 PHOTO NO. 54 55 LASER 94 .94 Α. FFDP-ANNULAR 100. 055 RATIO-ANNULAR 001 .051 RATIO-FULL FIELD 033 32 PHOTO NO. 41 60 LASER 94 94 94 94 .94 В FFDP-ANNULAR .069 ملان 006 029 .008 RATIO-ANNULAR .071 .638 031 .001 800 RATIO-FULL FIELD 1.16 .67 .068 PHOTO NO. 62 LASER 94 .94 94 FFDP - ANNULAR .12 058 .012 .069 800, RATIO-ANNULAR 061 .012 .012 .009 RATIO - FULL FIELD .095

FFDI METER READINGS

RATIO = FFDP/LASER OUTPUT

RETROR	EFLECT	OR TEM	PERATU	RES - 10		<u> </u>
	RI	TRO X			Υ	
STABIL	FACE	AT AX	AT RAD	FACE	ΔΤ ΑΧ	AT RAD
SEQ	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
ISTRT				-58.8	4.190 mV	+.043mV
ISTOP				-58.8	4.187mV	4.044 my
2 STRT					7	
2 STOP	-					
3 STRT						
3 STOP						
4 STRT	· =	-				
4 STOP						
5 STRT						† <del></del>
5 STOP						
6 STRT			7			
6 STOP		-/				
7 STRT				<u> </u>		1
7 STOP		<b>Y</b>				1
8 STRT				I		
8 STOP					1	

S-52

P2374455	May. 1996.
Page 41	a 48
Data 9 Juli	1974

0711

10.2 TEST CONDITIONS AND DATA LOG

TEST DATE		1691	IIME . F	NUM V 3 3	210 <u>2//</u>	
NOTES!	<u> </u>				·	
		• .				,
	•					

RETROREFLECTOR TEMPERATURES - C

	RE	TRO X		RETRO Y			
STABIL. SEQ.	FACE DAS 14		AT RAD Das 16		ΔT AX		
STRT	-48.z	-39.6	-43.4	-46.5	A 1.7	+0.7	
ISTOP	-51.2	- 40.6	- 44.4	- 47.5	+3.7	+0.9	
2 STRT		•					
2 STOP					·		
3 STRT							
3 STOP							
4 STRT							
4 STOP						<b></b>	
5 STRT			7				
5 STOP							
6 STRT							
6 STOP	•					·.	
7 STRT				*.		<del> </del>	
7 STOP	. /					<del>\</del>	
8 STRT			<del> </del>			1	
8 STOP			·		<del>                                     </del>	1	

#### TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	i	<1X10 <sup>-6</sup>	1.6x167
TEST ARTICLE	TEMP- C	-30±2 ℃	-30°C
COLDWALL TE	MP - °C (avg)	—185 ℃	-193°C
SOLAR	ANGLE		,,
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND	N/A	-3.72
SIMULATION	INTENSITY	1/20 S.C.	- 3.22_

FFDI Vacification photo was bee 67

OPTICAL DATA

OFTICAL		FIELD ANGLES					
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO.	68	69	10	11	72	
A	LASER	.94	.94	.94	.94	.94	
	FFDP-ANNULAR	.13	.063	.007	.061	.031	
	RATIO-ANNULAR	.14	.065	007	.064	,032	
	RATIO-FULL FIELD	1.16	.13	.033	p.13	32	
-	PHOTO NO.	13	14				
ا م ا	LASER	94	.94				
B	FFDP-ANNULAR	.08	.042				
	RATIO-ANNULAR	.083	.043				
	RATIO-FULL FIELD	1.15	.67				
	PHOTO NO.	75					
С	LASER	.94					
	FFDP - ANNULAR	.14					
	RATIO - ANNULAR	15					
	RATIO - FULL FIELD	1.14					

RATIO = FFDP/LASER OUTPUT

FFDI METER READINGS

Aerospace Aerospace

LAGEOS
THERMAL-OPTICAL TEST

Page 40 of 48

Date 9 July 1974

TEST CONDITIONS

OPTICAL DATA

1501 00110111			
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	<1XIO6	1.2 × 10-7
TEST ARTICLE	TEMP- C	-30±2 °C	- 36.6°C
COLDWALL TE	MP — ℃ (avg)	−185 <b>°</b> C	- 195 °C
SOLAR	ANGLE	0°	0°
SIMULATION	BACKGND	N/A	- 3.70
	INTENSITY	I.O S.C.	1.0
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

TEST DATE: 8-9-71 TEST TIME: FROM 0730 TO 405 1456

NOTESS SETTIF 1.6 SC AT 6907 8/9/74 : Photo 18 @ 128:57 Photo 76 @ 12:08:00

Radal Good (5) 10 very low of eggs out of tolangues considering

PROTO 74, 80, 81, 82,83 (Street 1930) STOP 14185 +21)

BACKEDO

RATIO = FFDP/LASER OUTPUT

BIAS . OOK

FFDI METER READINGS

			FIE	D ANG	LES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	77	78	79	80	81
	LASER	.9/	.9/	.9/	.91	.90
Α	FFDP-ANNULAR	.15	.07/	- 667	.074	339
	RATIO-ANNULAR	.16	.076	868	.082	.042
<u> </u>	RATIO-FULL FIELD	1.23	.77	.039	.80	.35,35
	PHOTO NO.	82	83			
	LASER	.91	.9/			
В	FFDP-ANNULAR	, 103	.055			
	RATIO-ANNULAR	.108*	.06/			
	RATIO-FULL FIELD	1.25	.73			
	PHOTO NO.	76				
	LASER	.91				
C	FFDP - ANNULAR	ide.				
	RATIO-ANNULAR	.16				
	RATIO - FULL FIELD	1.19				

RETROREFLECTOR TEMPERATURES - C

	METNOR	C CC	OR IEM	PERMIU	れたシー し		
		R	TRO X			RETRO	7
	STABIL	FACE	<del>OT AX</del>	AT RÁD	FACE	ΔΤ ΑΧ	AT RAD
Kotos	SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
96,77, 78	ISTRT	+/	-31	-37.5	-13.5	+2.00	+0.15
78	ISTOP	+9	-30.6	-38	-+5	+2.77	-0.49
79,86	2 STRT	0	-29.5	-36.5	-12.5	+ 2.96	+0.81
485	2 STOP	-47	-35.0	-37.5	-13.5	+2.53	+0.83
1 U -	3 STRT						7
* *	3 STOP			7	1		
	4 STRT				1		
	4 STOP						/
	5 STRT					7	/
	5 STOP		LX.				
	6 STRT				3 M. A.	X	
	6 STOP		7			<b>7</b> \	
	7 STRT					/	1
	7 STOP						
	8 STRT						
	8 STOP	7		,	1	1	1
						1	

Λ 1. 1. 4.

Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

7P2374455

Page 36 of 49

Date 9 July 1974

TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	<1 X 10 °6	1.6 ×10-1
TEST ARTICLE	TEMP - C	+30±2 °C	+29.5°C
COLDWALL TE	MP - ℃ (avg)	—185 °C	-1912
SOLAR	ANGLE	0°	0.
SIMULATION	BACKGND	N/A	-3.71 41
	INTENSITY	1.0 S.C.	-3,24
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 4

TEST DATE: 3-9-74 TEST TIME: FROM 1600 TO 2000

NOTES: #8+ plots at 19:29:51 442; #91 plots at 19:38:31

The 9 FFDI Vacification photo No. 92

OPTICAL	DATA		1			
[			FIEL	D ANG	LES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	94	85	86	87	88
ΙA	LASER	9t	.91	9	.91	_91
	FFDP-ANNULAR	.004	.øን	.012	.089	.045
	RATIO-ANNULAR	.19	_8 <del>84</del>	.013	.098	049
	RATIO-FULL FIELD	1.35	, de	.043	.88	.41
	PHOTO NO.	89	90			
	LASER	.91	9(			
B	FFDP-ANNULAR	.09	.054			
	RATIO-ANNULAR	.09	.058			
	RATIO-FULL FIELD	1,35	.80			
	PHOTO NO.	91				
C	LASER	91				
	FFDP - ANNULAR	.15				
l	RATIO-ANNULAR	11				
· ′	RATIO - FULL FIELD	1.35				

RETROREFLECTOR TEMPERATURES - C

		RE	TRO X		ſ	RETRO	
かん	STABIL	FACE	<del>∆T AX</del>	AT RAD	FACE	ΔΤ ΑΧ	AT RAD
164.	SEQ	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
26	ISTRT	-24	-2.0	-12.0	-20.0	6.05	1.95
	ISTOP	-25.5	-2.0	-/3.0	-20.5	6.07	1.77
	2 STRT					1	
	2 STOP						
	3 STRT				·		
	3 STOP	·					
	4 STRT				ファ	1	
•	4 STOP						
	5 STRT				<u> </u>	1	
	5 STOP						
	6 STRT	De mark for en		Land in		1 2019	
	6STOP	emples mil som	in more for	a de la companya de l			
Λ,	7 STRT				and the second		Xre'
	7 STOP			सर्वेद सिंद सम्ब	14.		
	8 STRT					1	
	8 STOP						
					-		

in S

- RATIO = FFDP/LASER OUTPUT

FFDI METER READINGS

33

priginal 18/1.22 0.148 (8-8-79 1855 day) After +30 - 4 Solar .22/1.35 = 0.161 the initiation of the text about the resulte labelled original. The measurements were made again after the test + 50°C with solar. The ratio at this time has changed along with a slight decrease in lacer power . The lacer pour decrease can't account for the fact. Since there for been a change is the temperature the animaling could be comed by the a change in practice of the beam who it atribes the love power maile mice . The informity of the beam incident on the CCR in still very good . \* Could also be counted by the temperature of the calibration cube, Aerospace Systems Division

NOTES:\_\_\_\_

LAGEOS C

P2:	<b>3744</b> 5	5 Hav. No.
		<sub>01</sub> 48
) ata	9 Ju	lu 1974

TEST NO.6

TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	<1 X10_6	1.2×10-7
TEST ARTICLE	TEMP- C	+30±2 °C	+30°C
COLDWALL TE	MP - C (avg)	−185 °C	-196°C
SOLAR	ANGLE	-	
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND	N/A	-37/AV
SIMULATION	INTENSITY	1/20 S.C.	

FFBI Verification Photo No. 93

OPTICAL	DATA	Bias = .067					
0. 7.07.		FIELD ANGLES					
RETRO	DATA	0	+15	+30	-15	-30	
	PHOTO NO.	94	95	96	97	98	
Λ	LASER	.90	90	.90	90	.90	
A.	FFDP-ANNULAR	16	.684	اله	.083	434	].0
	RATIO-ANNULAR	18	.093	.012	.091	.046	
	RATIO-FULL FIELD	1.30	.84	و39	.83	.34	
	PHOTO NO.	99	100				
1	LASER	.90	.10				
B	FFDP-ANNULAR	35.08	664				1
	RATIO-ANNULAR	1-001	.095				1
	RATIO-FULL FIELD	1.28	.15				1
	PHOTO NO.	1 01					1
	LASER	.90					1
C	FFDP - ANNULAR	-15					1
. –	RATIO-ANNULAR	.16					1
•	DATIO CULL SICLO	1.01					1

RATIO = FFDP/LASER OUTPUT

I METER READINGS

				<del></del>
,		,		<del></del>
RETE	ROREFLECTOR TEN	MPERATUR	si– °C	
	RETRO X	(	RETRO Y	
`	<del></del>		<del></del>	

10.2 TEST CONDITIONS AND DATA LOS

TEST DATE: 8-9-74 TEST TIME: FROM 2014 TO 2330

SEQ. DAS 14 DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 I STRT -20.5 +0.5 -10 -13.5 +5/2 +1/74	RETROREFLECTOR TEMPERATU						
SEQ. DAS 14 DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 I STRT -20.5 +0.5 -10 -13.5 +5.20 +1.79 I STOP -23.5 -1.0 -11 -14.5 +5.30 +1.03 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 7 STOP 8 STRT 7 STOP 8 STRT		R	ETRO X		ſ	RETRO Y	<u> </u>
I STRT -20.5 +0.5 -10 -13.5 +5/2 +1/74 I STOP -23.5 -1.0 -11 -14.5 +530 +1.03 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 7 STOP 8 STRT	STABIL	FACE	AT AX	AT-RAD	FACE	ΔΤ ΑΧ	ΔT RAD
I STOP -23.5 -/.0 -// -/45 +530 +/.63 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 7 STOP 8 STRT	SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 7 STOP 8 STRT	ISTRT	-20.5	+0.5	-10	- 13.5	+5/2	1174
2 STRT. 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 7 STOP 8 STRT	ISTOP	-23.5	-1.0	-11	-14.5	+530	+1.43
3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	2 STRT.						
3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	2 STOP					,	
4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	3 STRT						
4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	3 STOP						
5 STRT   5 STOP   6 STRT   6 STOP   7 STRT   7 STOP   8 STRT   8 S	4 STRT						
5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	4 STOP						
6 STRT 6 STOP 7 STRT 7 STOP 8 STRT	5 STRT					1	
6 STOP	5 STOP					1. "	
7 STRT 7 STOP 8 STRT	6 STRT			7		· -	
7 STOP	6 STOP						
8 STRT	7 STRT						
	7 STOP					·	X
8 STOP	8 STRT						
	8 STOP	· /					

No. 172.	574 J	Rev. No.
Pap.	35	<u>48</u>
Date	9 Jul	u 1974

RETRO Y

FACE AT AX AT RAD

+6.46

+6.41 + 1.70

+1.86

DAS 15 DAS 16 DAS 20 DAS 21 DAS 22

- 23.5

-23.0

TEST CONDITIONS

OPTICAL DATA

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	X   <b 66	1.8 × 10-7
TEST ARTICLE	TEMP - C	+30±2 °C	
COLDWALL TE	MP - C (avg)	—185 °C	- 1962
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

FFDI	Verif.	Photo	No. 102
		ı	Bias = , out

			FIEL	D ANG	LES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	103	104	105	106	107
	LASER	.90	.90	.90	.9/	.91
A	FFDP-ANNULAR	.15	.070	.009	ં	.036
ļ	RATIO-ANNULAR	.16	.016	010	.013	.039
	RATIO-FULL FIELD	1.25	.18	. 036	.80	36
	PHOTO NO.	108	109	110	111	112
	LASER	.9(	.90	.90	.90	90
В	FFDP-ANNULAR	.059	.035	.008	,030	,008
	RATIO-ANNULAR	.063	.038	1009	.033	.009
	RATIO-FULL FIELD	1.24	.13	.05	.84	.075
	PHOTO NO.	113	114	115	116	117
$\sim$	LASER	90	.90	.90	.90	90
C	FFDP - ANNULAR	-11	.062'	.013	.013	
	RATIO-ANNULAR	112	.068	. 015	.080	.011
	RATIO - FULL FIELD	1.24	.13	.104	.88	.049

RATIO = FFDP/LASER OUTPUT FFDI METER READINGS 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT **7 S.TOP** 8 STRT 8 STOP

	10.2	TEST	CONDIT	TIONS AND DATA LOG	TEST NO.3
TEST DATE	<u>. a</u>	944	TEST	TIME: FROM 8000 TO 0	126
NOTES:			_		
				,	
<del></del>			ره،		
		-	· · · · · · · · · · · · · · · · · · ·		

RETROREFLECTOR TEMPERATURES - C RETRO X

-6.0

AT AX AT RAD

-18.5

-18.5

FACE

DAS 14

-34.5

-34.0 -5.5

STABIL

SEQ

STRT

STOP

2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP REMANDICALITY OF

Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

No. TP23	74455	Aou. No.
Page_		ol
Dete	9 July	1974

Inotherand - Vocum

Item 40.30

10.2 TEST CONDITIONS AND DATA LOS TEST NO. 18

TEST DATE: 8/2/74 TEST TIME: F	
	· ·

PLANNED ENVIRONMENT ACTUAL 2410-6 CHAMBER PRESSURE 6 × 10-6 TEST ARTICLE TEMP - C Anh AND COLDWALL TEMP - C (avg) Anh. AMB SOLAR ANGLE SIMULATION BACKGND INTENSITY EARTH IR BACKGND SIM ULATION INTENSITY

FFDI Vacilization Photo 118

TEST CONDITIONS

OPTICAL DATA

HH .004 BIOS \* 005 BIOS

			FIE	LD ANG	BLES	
RETRO	DATA	. 0	+15	+30	-15	-30
	PHOTO NO.	119	120	121	122	123
2	LASER	.91	.91	.9/	.91	.91
17	FFDP-ANNULAR	-14	.064	1.007	.064	033
	RATIO-ANNULAR	.16	.020	.007	06	.037
	RATIO-FULL FIELD	1.22	.77	.034	.78	.34
	PHOTO NO.	124	125	126	127	128
12	LASER	.9/	.91	.91	.9/	.9/
B	FFDP-ANNULAR	000	.039	<del></del>	838	008
, -	RATIO-ANNULAR	.078	<del></del>		t	.009
	RATIO-FULL FIELD	1.20	-71	.047	.82	.072
	PHOTO NO.	129	130	131	132	/33
	LASER (13)	.91	.91	.91	.9/	.90
	FFDP - ANNUL AR	<b>E</b> 3	.067	1.0/2	1.078	
	RATIO-ANNULAR	.14		0/3	- 84	
	RATIO - FULL FIELD	1.Z	.71	.097	.85	.009
	- FEDRAL ACED ON		•//			.046

RATIO = FFDP/LASER OUTPUT FFDI METER READINGS

RETROREFLECTOR TEMPERATURES - TO RETRO X RETRO Y STABIL FACE AT AX AT RAD FACE AT AX AT RAD SEQ. DAS 14 DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 STRT STOP 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT **7.STOP** 8 STRT 8 STOP

Aerospace

8 STOP

LAGEOS
THERMAL-OPTICAL TEST

Ne. TP2.	374455
Page	to
Date	9 July 1974

Jhr431

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 5

EST DATE: 8-/2-74	TEST	TIME: FROM 0720 TO 1621
INTER.		

NOTES:		 	*			
				 · · · · · · · · · · · · · · · · · · ·		
			-			
	<del>, , , , , , , , , , , , , , , , , , , </del>	 ············		 <del></del>	<del></del>	<del></del>

RETROREFLECTOR TEMPERATURES - ℃

6145 .006

ACTUAL

1.6×10-1

-193°C

+61°C

OPTICAL	DATA					
			FIE	D ANG	BLES	
RETRO	DATA	0	+15	+30	-15.	-30
	PHOTO NO.	134	135	136	137	138
<b>7</b> 1	LASER	.89	.89	99	.89	.89
M	FFDP-ANNULAR	.15	.072	.009	.061	.036
	RATIO-ANNUL AR	يا.	.079	.010	.077	.040
	RATIO-FULL FIELD	1.24	.78	.036	.80	.36
	PHOTO NO.	139	140	14-1	142	143
	LASER	.89	. 89	.98	.89	.88
B	FFDP-ANNULAR	.078	.040	100A	.041	.010
	RATIO-ANNULAR	24.80	,045	.010	.046	-011
	RATIO-FULL FIELD	123	.12	.051	.85	.016
	PHOTO NO.	144	145	146	147	148
	LASER	.89	.89	-89		
C	FFDP - ANNULAR	14-	014	.014	.88	.88
	RATIO-ANNULAR	.17	580	.016	.098	-01-
	RATIO-FULL FIELD	1.24	13	048	.87	.050
RATIO	= FFDP/LASER OU	TPUT	FF		ER RE	

PLANNED

KIXID-F

760 12°C

-185°C

RETRO X RETRO Y FACE AT AX AT RAD STABIL FACE AT AX AT RAD SEQ. **DAS 14** DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 TIME STRT -18.5 +17 125 +8.34 +2.74 16:08:01 STOP -18.5 +19 73 +8.09 +2.79 16:19:31 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT

S-60;

TEST CONDITIONS

SOLAR

SIMULATION

EARTH IR

SIM ULATION

CHAMBER PRESSURE

ENVIRONMENT

TEST ARTICLE TEMP - C

COLDWALL TEMP - C (avg)

ANGLE

BACKGND

BACKGND

INTENSITY

Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

Page 42 of 48

Date 9 July 1974

JE	•	7	CO		N	TI	^	kt	c
	.0		UU	м	vi	,,	v	п	э

MENT	PLANNED	ACTUAL
SSURE	AMB	Male
TEMP - C	AMB	Anb.
MP - C (avg)	AMB	Mak
ANGLE		
BACKGND		
INTENSITY		
BACKGND		
INTENSITY		
	ANGLE BACKGND INTENSITY BACKGND	SSURE AMB TEMP-C AMB MP-C (avg) AMB ANGLE BACKGND INTENSITY BACKGND

10.2	TEST	CONDITIONS	AND	DATA	L06	TEST	NO.10
40.00							

	DATE: 8-72	24	TEST	TIME:	ROM Z	TO	22/5	• •
								<u></u>
· <del></del>				· <b>-</b>		· · ·	· · · · · · · · · · · · · · · · · · ·	<del></del>

### 48 FFDI Vachicator Noto 16, 149

<b>OPTICAL</b>	DATA	#.007 Bros							
		FIELD ANGLES							
RETRO	DATA	0	+15	+30	-15	-30			
1	PHOTO NO.	150	151	152	158	154			
	LASER	.89	.89	.87	.89	.88			
D	FFDP~ANNULAR	-/2	.05.	. 02	.04	20			
	RATIO-ANNULAR	.14	.05	.02	.05	.007			
	RATIO-FULL FIELD	1.24	.76	. 35	.82	035			
	PHOTO NO.	155	156						
	LASER	.88	.88						
E	FFDP-ANNULAR	.12	.06						
_	RATIO-ANNULAR	14	.07						
	RATIO-FULL FIELD	1.26	.78						
	PHOTO NO.	157							
	LASER	.88							
F	FFDP - ANNULAR	.10							
	RATIO-ANNULAR	.12							
	RATIO - FULL FIELD	1.24							
RATIO	RATIO = FFDP/LASER OUTPUT FFDI METER READINGS								

#### RETROREFLECTOR TEMPERATURES - 90

NETRON		ETRO X	PERATU			
STABIL	FACE		AT RAD		RETRO	
·	DAS 14	1			ΔΤ ΑΧ	AT RAC
	UAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
STRT	21	20	2/	2/	0	3
ISTOP	20	20	20	20	0	/
2 STRT						
2 STOP				··········		/
3 STRT						<del> </del>
3 STOP	···					<del>                                     </del>
4 STRT						
4 STOP	·				· · · · · ·	<del> </del>
5 STRT					<del>                                     </del>	
5 STOP					<u> </u>	<del> </del>
6 STRT						<del> </del>
6 STOP						-
7 STRT			, , , ,			
7.STOP			_		<del>                                     </del>	
8 STRT					<b> </b>	<del></del>
8 STOP					<del> </del> -	<del>                                     </del>

STABIL

7 STOP

8 STRT 8 STOP FACE

SEQ. DAS 14

LAGEOS THERMAL-OPTICAL TEST

TP2	374	455		
			of	
O ete	9,	Joly	1974	

RETRO Y

AT RAD

TIME

00:20

00:53

FACE AT AX

DAS 15 DAS 16 DAS 20 DAS 21 DAS 22

TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	2 × / 6-8	12 ×10-5
TEST ARTICLE		T-1-1-1	1 Mak-5
COLDWALL TE	MP - °C (avg)	Anh	Amb
SOLAR	ANGLE		400
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND .		
SIMULATION	INTENSITY		

FFDZ Verification Photo No. 158

10.2 TEST CONDITIONS AND DATA LOS TEST NO. !

TEST DATE: ------TEST TIME: FROM 7220 TO 0053 NOTES:\_

> RETROREFLECTOR TEMPERATURES - C RETRO X

> > AT AX AT RAD

HEN 33 OPTICAL DATA Bias = .006

		FIELD, ANGLES					
RETRO	DATA	0	+15	+30	15	-30	
	PHOTO NO.	159	160	161	162	163	
	LASER	.89	.89	.89	.88	.89	
	FFDP+ANNULAR	.163	.050	.031	.648	.008	
	RATIO-ANNULAR	.116	.055	.034	.053	.008	
	RATIO-FULL FIELD	1.25	.77	.33	.82	.038	
	PHOTO NO.	164	165	166	167	168	
س م	LASER	. 89	.89	.89	.89	9.9	
<u> </u>	FFDP-ANNULAR	, <i>11</i>	.066	510.	.661	.009	
•	RATIO-ANNULAR	.12	.074	.014	.065	.010	
	RATIO-FULL FIELD	1.28	.79	.084	.81	.052	
	PHOTO NO.	169	170	171	172	173	
-	LASER	.89	. 29	89	.89	.89	
	FFDP - ANNULAR	.102	.046	.007	.056	.013	
	RATIO-ANNULAR	116	.051	800.	190	.014	
	RATIO - FULL FIELD	1.25	.19	.039	480	.10	
RATIO	= FFDP/LASER OU	TPUT	FF	DI MET			

STRT 19.0 20.5 204 19.5 +0.4 STOP 19.5 2/.0 20.5 20.0 to.4 2 STRT 2 STOP 3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT

S-62

Bendix

TEST

Systems Division

LAGEOS
THERMAL-OPTICAL TEST

)	Na. TP2374455
	Page of
	Date 9 July 1974

0723

Item 32

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 19

DATE: 8-13-74	TEST	TIME: FROM 0100 TO 0723
:•		•

OTES#		•	 		
-	 	 			
	 		 <del></del>		
•	 ,	 		 	·

JAM

RETROREFLECTOR TEMPERATURES - %

	11011			PERAIU	462- C		
			ETRO X			ſ	
	STABIL			AT RAD		ΔΤ ΑΧ	AT RAD
	SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
	STRT	-93	-47	-54	-62.5	+6,3	+1.1
	ISTOP	-10	-47	-53	-62	+6.2	11.1
	2 STRT		•	,			
٠	2 STOP						
	3 STRT						
•	3 STOP						<del>                                     </del>
,	4 STRT						
	4 STOP	-					
	5 STRT					<del> </del>	<b></b> -
	5 STOP						
	6 STRT						-
	6 STOP						
	7 STRT						
-	7 STOP				•		<del> </del>
	BSTRT						<u> </u>
-	BSTOP			<del></del>			

#### TEST CONDITIONS

TEST CONDITIO	113		
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE		1×10-6</td <td>1.5+10-7</td>	1.5+10-7
TEST ARTICLE	TEMP - °C	-30±2°C	-30
COLDWALL TE	MP—°C (avg)	-185°C	-194°C
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

## FFDI Varification photo No. 174

OPTICAL	_ DATA			Bio	'Z = '00F	)
			FIE	D ANG	BLES	
RETRO	DATA	0	·+15	+30	-15	-30
1	PHOTO NO.	175	176	177	178	179
D	LASER	.89	.89	.88	.89	.88
	FFDP-ANNULAR	.10	.043	.028	.043	.008
	RATIO-ANNULAR	.10	.047	.031	.051	.001
	RATIO-FULL FIELD	1.26	.76	.33	.82	.038
	PHOTO NO.	180	[8]	182	183	184
E	LASER	.84	.88	.88	.88	.88
	FFDP-ANNULAR	.103	.056	.011	.053	,007
	RATIO-ANNULAR	-	. 061	.013	.060	.010
	RATIO-FULL FIELD	1.27	.78	.082	8	.052
	PHOTO NO.	185	186	87	188	189
<i>j</i> = 1	LASER	.88	.88	.88	.88	.88
	FFDP - ANNULAR	.093	.043	007	-048	.012
	RATIO-ANNULAR	.102	.047	800,	.054	.013
	RATIO - FULL FIELD	125	70	A20	TAX I	

RATIO = FFDP/LASER OUTPUT

FFDI METER READINGS

Systems Division

LAGE 05 THERMAL-OPTICAL TEST

No. TP2374455	Rer. Ne.
Pm_ 44	<u>., 48</u>
Date 9 Juli	ų 1974

TEST NO. 12

TEST CONDITIONS

TEST COMPLIE	7113		-
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE		<1X10 <sup>-6</sup>	R8x10-8
TEST ARTICLE	TEMP - C	+30±2 °C	
COLDWALL TE	MP - ℃ (avg)	—185 °C	-195°C
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

TEST DATE: 8-/3-79	TEST	TIME: FROM 0730 TO 1320
	,,,,	

10-2 TEST CONDITIONS AND DATA LOG

has 9 FFDI Vactication photo No. 190 OPTICAL DATA

			FIE	LD AND	BLES		1
RETRO	DATA	0	+15	+30	-15	-30	Ì
	PHOTO NO.	191	192	193	194	195	5 
_	LASER	.87	.87	.87	.27	.27	
D	FFDP-ANNULAR	*.096	1047	207.	.046	W 00.9	
	RATIO-ANNULAR	10	.052	. 267	.063	1.010	]-
	RATIO-FULL FIELD	1.27	.78	.34	. 23	040	. *
-	PHOTO NO.	196	197	198	199	200	
	LASER	.87	.87	.87	.27	.87	
E	FFDP-ANNULAR	N	.067	.0/3	4M .063	.01/.	
-	RATIO-ANNULAR	.12	.075	.015	.070	.0/2	
	RATIO-FULL FIELD	1.29	.50	.086	.83	.053	+30
	PHOTO NO.	201	202	203/	204		203
_	LASER	.87	.88	302	.87	.87	.87
F	FFDP - ANNULAR	don	.046	200	.054	10/9	.009
	RATIO-ANNULAR	.11	.052	- 1	.062	.0/6	.010
	RATIO - FULL FIELD		.80	7	. 82	.10	.041
RATIO	= FFDP/LASER OU	TPUT	FF	DI MET		ADINGS	

REINOR			PERATU	RES - C	-		
		TRO X			RETRO	Y	,-
STABIL	FACE	1 .	AT RAD	FACE	ΔΤ ΑΧ	ΔT RAD	
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22	TIME
STRT	-68	-9	-23	-27	+293	+2,27	13:02:01
STOP	-63	-9	-22	-26	+5.26	+2./3	18:19:41
2 STRT					<del></del>		
2 STOP							-
3 STRT						<del>                                     </del>	
3 STOP						<b> </b>	1 2 7
4 STRT							
4 STOP						<del> </del>	
5 STRT						<del>                                     </del>	. *
5 STOP			<b>*</b>		<del> </del>	<del> </del>	
6 STRT					<u> </u>	† - · · ·	
6 STOP					<del>                                     </del>	<del> </del>	
7 STRT				20			
7 STOP					1	<del>                                     </del>	
8 STRT				<del></del>	<del>                                     </del>	$\overline{}$	
8 STOP		<b></b>			<del> </del>		

<b>)</b>	No. TP2374455	Rev. No.
٠	Page	. of
	Date 9 Juli	1974

Item 37 TEST NO. 20 1728

TEST CONDITIONS

OPTICAL DATA

LASER

FFDP - ANNULAR RATIO-ANNULAR RATIO - FULL FIELD

RETRO

ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	<del></del>	Amb.	Anb.
TEST ARTICLE		Anb.	AMb.
COLDWALL TE	MP - °C (avg)	Anb.	Dub
SOLAR SIMULATION	ANGLE		
	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

Item 9 FFDI Venification Photo No. 266

Bias = .006

FIELD ANGLES

	J.					
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	207	208	209	2/6	
_	LASER	.87	81	87	. 97	<del> </del>
D	FFDP-ANNULAR	.11	, 656			
	RATIO-ANNUL AR	12	.059	.629	05+	<u> </u>
	RATIO-FULL FIELD	1.24		433	-064	
	PHOTO NO.	<u> </u>	.74	3/_	.86	
- سو	LASER		<del> </del>			·
E	FFDP-ANNULAR		<del>                                     </del>			
{	RATIO-ANNULAR					
	RATIO-FULL FIELD	<del></del>	<del> </del>	<del></del>		
	PHOTO NO.					

IMMINO TOLL FIELD	
RATIO = FFDP/LASER OUTPUT	FFDI METER READINGS

RETROPERIECTOR	TEMPERATURES - 9
NETROREFLECTOR	TEMPERATURES - 90

10.2 TEST CONDITIONS AND DATA LOG TEST DATE: 9-14-74 TEST TIME: FROM 4517 TO 0528-

Repeat optical data - Test zon

		TRO X				RETRO	Υ
STABIL.	1	ΔT AX	ΔΤ	RAD	FACE	ΔT AX	AT RAD
	DAS 14	DAS 15	DAS	3 16	DAS 2	DAS 2	I DAS 22
STRT							and the same of
ISTOP							
2 STRT						<b></b>	/
2 STOP	-				•	1/	<del></del>
3 STRT						/-	<del></del>
3 STOP		1					
4 STRT		7-	1				<del></del>
4 STOP	,			V		<del></del>	-
5 STRT						<del>                                     </del>	<del>-  </del>
5 STOP						<del></del>	<del></del>
6 STRT				-	1	<del> </del>	<del></del>
6 STOP						<b>/</b>	<del> </del>
7 STRT		1				1	<del></del>
7 STOP					•	1	
8 STRT					<del></del>	<b>`</b>	4
8 STOP			_		<del></del>	+	+

Bendix
Aerospace Systems Division

7	<sup>Np.</sup> TP2374455	nov. Ne.
	Paga	of
	Date 9 July	1974

ITEN 37

10.2 TEST CONDITIONS AND DATA LOG

TEST NO. 20 1

TEST DATE: _ &	TEST	TIME: FR	OM 0530 TO 3	552	
NOTES#	_			/730	

- FFDI Verification Photo No. 206

PLANNED

mb

OPTICAL DATA

SOLAR SIMULATION

EARTH IR

SIM ULATION

TEST CONDITIONS

CHAMBER PRESSURE

ENVIRONMENT

TEST ARTICLE TEMP - C COLDWALL TEMP - C (avg)

> ANGLE BACKGND INTENSITY

BACKEND

INTENSITY

ACTUAL

			FIE	D ANG	SLES	<del></del> -
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	212	213	214	215	216
	LASER	.87	.97	.67	.87	.87
	FFDP-ANNULAR	.11	.054*	03!	.050	.008
	RATIO-ANNULAR	12	۵59*	.035	.056	.009
	RATIO-FULL FIELD	1.27	.18	34	.43	,039
4.	PHOTO NO.	217	218	219	220	22/
	LASER	.87	.87	.87	.87	.87
. <u>E</u>	FFDP-ANNULAR	.12	,073	609	064	.015
• •	RATIO-ANNULAR	.13	.075	.011	.675	.017
	RATIO-FULL FIELD	1.29	.76	046	- 86	-10
, *	PHOTO NO.	222	223	224	225	226
. سم	LASER	.87	.87	.87`	.87	07
F	FFDP - ANNULAR	.10	049	800	058	.015.
•	RATIO-ANNULAR	.11	.057	009	.067	015
	RATIO - FULL FIELD	1.27	.81	640	. 81	.11
RATIO	= FFDP/LASER OU	TPUT	FF			ADINGS

RETRORES FOTOR TEMPERATURES

METROREFLECTOR TEMPERATURES - C							
· <b>1</b>	R	RETRO X			RETRO Y		
STABIL	1	ΔΤ ΑΧ	ΔT RAD	FACE	ΔΤ ΑΧ	ΔT RAD	
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22	
ISTRT							
ISTOP			-				
2 STRT							
2 STOP							
3 STRT							
3 STOP							
4 STRT					<del>                                     </del>		
4 STOP			X				
5 STRT						<del></del>	
5 STOP		-				1	
6 STRT							
6 STOP	1		240		100		
7 STRT							
7 STOP				•			
8 STRT							
8 STOP	/				1		
•						<b>4</b>	

Systems Divisio

LAGE 05 THERMAL-OPTICAL TEST

No.	i Rev.	No.
TP2:	374455	
Page.		
		_
Date	9 July 19	74

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 13 TEST TIME: FROM 18/19 TO 2016 NOTES:\_

### Strag FFOI Vacification photo 227

TEST CONDITIONS

SOLAR

SIMULATION

EARTH IR

SIMULATION

OPTIONI DATA

CHAMBER PRESSURE

**ENVIRONMENT** 

TEST ARTICLE TEMP - C

COLDWALL TEMP - C (avg)

ANGLE

BACKGND INTENSITY

BACKGND

INTENSITY

ACTUAL

1.6 × 10-5

Amb

Amb

OPTICAL	DATA					
			FIE	LD ANG	LES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	228	229	230	231	212
	LASER	0 88	0.88	0.37	0.25	0.38
D	FFDP-ANNULAR	0.10	0.059*	0.032	0.049	0.001
	RATIO-ANNULAR	0.12	0.0634	0.036	0.053	0.009
	RATIO-FULL FIELD	1.28	0.78	0.35	0.72	0.039
	PHOTO NO.	233	234	235	236	237
E	LASER	0.88	6.27	0.18	0.88	0.82
	FFDP-ANNULAR	0.12	0.064	0.009 4	0.063	0.015
	RATIO-ANNULAR	0.15	40724	0.010	0.671 4	0.016
	RATIO-FULL FIELD	1.28	0.77	0.017*	0.15	0.10
	PHOTO NO.	238	239	240	241	242
ميو	LASER	088	0.72	0 21	0.28	0.1%
<i>F</i>	FFDP - ANNULAR	010	0.049 4	0.008 N	0.457 #	0.01
	RATIO-ANNULAR	0.11	0.05/ 4	0.009 4	0.063	0.015
	RATIO - FULL FIELD	1.27	0.81	0.040 4	0.8/	0.10
RATIC	# FFDP/LASER OU	TPUT	FF		ER RE	

ITEM 24

**PLANNED** 

ZX10-4

Anb

Anb

RETRO			PERATU	RES— °C	<u> </u>	
		ETRO X			RETRO	Υ .
STABIL		AT AX	AT RAD	FACE	ΔΤ ΑΧ	AT RAD
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
STRT	21.5	22.0	21.5	21.4	+.3	0
ISTOP	21.5	22.0	21.5	21.5	4.2-	0
2 STRT		]			<b>1</b>	
2 STOP						
3 STRT					-	/
3 STOP			10.1			
4 STRT						
4 STOP					-	<del>                                     </del>
5 STRT				1/-		<del>                                     </del>
5 STOP					1	-
6 STRT					<u> </u>	
6 STOF	)					<del>                                     </del>
7 STRT						<del> </del>
7 STOP					<u> </u>	$\leftarrow$
8 STRT					<b></b>	1
8 STOF	, 7	1		<u> </u>	<del> </del>	<del></del>
			4	<b>_</b>	1	

Bendix

#### Aerospace Systems Division

LAGEOS
THERMAL-OPTICAL TEST

D	No. TP2374455
	Pagenf
	Date 9 July 1974

TEST CONDITIONS

TEST CONDITIO	7113		
ENVIRON	MENT	PLANNED	ACTUAL
CHAMBER PRE	SSURE	4/x10-6	1.4 × 10-7
TEST ARTICLE	TEMP - C	-3012°C	-312
COLDWALL TE	MP - °C (avg)	-185°C	-1852
SOLAR	ANGLE		
SIMULATION	BACKGND		
	INTENSITY		
EARTH IR	BACKGND		
SIMULATION	INTENSITY		

Itan 9 FFDI Varification photo 143

RATIO = FEDP/I ASER OUTPUT

Bias = .606 OPTICAL DATA FIELD ANGLES RETRO DATA +30 -30 PHOTO NO. 246 248 LASER FFDP-ANNULAR 010 .643 830 RATIO-ANNULAR RATIO-FULL FIELD 1.27 .82 PHOTO NO. 252 LASER FFDP-ANNULAR 654 200 RATIO-ANNULAR .055 RATIO-FULL FIELD 1.27 ,046 PHOTO NO. 255 LASER 88 FFDP - ANNULAR 100. 210 RATIO - ANNULAR RATIO - FULL FIELD

	CONDITIONS AND DATA LOS TEST NO. 21
TEST DATE: 8-14-74 NOTES: 10 8-15-74	TEST TIME: FROM 2016 TO 0152

RETROREFLECTOR TEMPERATURES - %

		ETRO X	PERATU	<del>,</del>	RETRO	Y
STABIL. SEQ.	FACE DAS 14	í	DAS 16		ΔΤ ΑΧ	ΔT RAD DAS 22
STRT	-57.5	-48	-57.5	-62.5	+8.5	+1.0
STOP	- 57.5	-48	-53.5	-62.5	+8.4	11.0
2 STRT	<u> </u>					
2 STOP					<u> </u>	
3 STRT					<b>_</b>	<del>/                                    </del>
3 STOP						
4 STRT						<del> </del>
4 STOP					f	
STRT					<del></del>	<del></del>
5 STOP			X		<del>                                     </del>	
6 STRT					l	
6 STOP				/		<del> </del>
7 STRT				<u> </u>		<del> </del>
7 STOP					<del>\</del>	<del> </del> -
8 STRT					<del>                                     </del>	$\overline{}$
BSTOP	7			<del></del>	<del></del>	<del></del>

. S-68

TP2374455									
Page_		of							
Date	9 ժակ	1974							

TEST CONDITIONS

ENVIRON	MENT	PLANNED	ACTUAL		
CHAMBER PRE	SSURE	41 × 10.6	1.4×10-7		
TEST ARTICLE	TEMP - C	+30 12°C +30°C			
COLDWALL TE	MP - ℃ (avg)	-185°C	-/96°C		
SOLAR	ANGLE				
SIMULATION	BACKGND				
	INTENSITY				
EARTH IR	BACKGND		<del> </del>		
SIMULATION	INTENSITY	,	· · · · · · · · · · · · · · · · · · ·		

Item 9- FFDI Verification Photo No. 259

OPTICAL	DATA		BIAS	= .00	7	
			FIE	LD ANG	BLES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	260	261	262	263	264
7	LASER -	.88	. 88	.87	. 28	. 88
D	FFDP-ANNULAR	.08/	.042	.028	.039	. 008
İ	RATIO-ANNULAR	.091	.047	. 032	.048	.009
	RATIO-FULL FIELD	1.27	.78	. 35	.92	.038
	PHOTO NO	265	266	267	268	269
_	LASER 4	.88	.37	.87	48.87	
E	FFDP-ANNULAR	.098	.057	. 007	.052	.014
_	RATIO-ANNULAR -	.10	.064	.011	.059	.016
	RATIO-FULL FIELD	1.28	-76	.047	.75	.10
	PHOTO NO.	270	271	272	273	274
_	LASER	.78	.88	.87	.87	.87
-	FFDP - ANNULAR	.084	.040	.007	.016	.013
	RATIO-ANNULAR	.096	.015	.008	.052	.014
	RATIO - FULL FIELD	1.27	.81	. 040	.81	.10
RATIO	FFDP/LASER OU	TPUT	FF	DI MET	ER RE	

-	-	10-2	TEST	CONDIT	rions	AND	DATA	LOG	TEST	NO. 14
	DATE:			TEST	TIME	: FR(	OM <u>02</u>	<i>00</i> то	0656	
****						_				
		·							***************************************	
	·									<del></del>
	<del></del>							•	SW	1

RETROREFLECTOR TEMPERATURES - C RETRO X RETRO Y AT AX AT RAD FACE AT AX AT RAD STABIL FACE SEQ. DAS 14 I STRT -28 -8,5 -22 -27 +16.8 + 2.4 ISTOP -17 -26 2 STRT 2 STOP 3 STRT

DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 7im @ 0635 0656 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT 8 STOP

8 STOP

LAGEOS THERMAL-OPTICAL TEST

No. TP2374455	Roy, No.
Page	. ol
Date 9 Juli	1974

14:17:41

14:30:01

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 22

TEST DATE: 8-15-74 TEST TIME	·
NUTESI	

RETROREFLECTOR TEMPERATURES - C

Item 9 FFDI VERIFICATION Phato No. 275

ANGLE

BACKGND INTENSITY

BACKGND

INTENSITY

TEST CONDITIONS

SOLAR

SIMULATION

EARTH IR

SIMULATION

CHAMBER PRESSURE

ENVIRONMENT

TEST ARTICLE TEMP- C

COLDWALL TEMP - C (avg)

OPTICAL DATA A.0/0 B/AS

OI LIGHT	- <u> </u>			1,0/0 B	7-	
			FIE	LD ANG	BLES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	276	227	278	279	280
D	LASER	.87	27	.87	87	.87
	FFDP-ANNULAR	.12	.068	.038	1065	0/2
	RATIO-ANNULAR	./3	.077	.043	.073	.0/3
·	RATIO-FULL FIELD	1.38	.96	.39	.91	.045
	PHOTO NO.	281	282	283	284	285
	LASER	.87	87	.87	.87	.87
I	FFDP-ANNULAR	./3	.054	.0/3	.023	.019
	RATIO-ANNULAR	.15	.095	.016	.094	.022
	RATIO-FULL FIELD	1.39	.84	.054	.95	.12
	PHOTO NO.	286	287	288	289	290
اسرا	LASER	.87	.17	.97	.87	.87
	FFDP - ANNULAR	./3	.064	*011	.070	*0/8
	RATIO-ANNULAR	.14	.070	.0/2	.080	020
	RATIO - FULL FIELD	1.38	.90	.047	89	.12
	= FFDP/LASER OU					ADINGS

PLANNED

<1×100

+60 12 C

-185°C

ACTUAL

1.ZX10-7

59°C

-193 C

RETRO X RETRO Y STABIL FACE AT AX AT RAD FACE AT AX AT RAD DAS 15 DAS 16 DAS 20 DAS 21 DAS 22 SEQ. DAS 14 STRT -6.6 16.5 -25 +12.9 STOP -60 16.0 4.5 +17.05 2 STRT 2 STOP I3 STRT 3 STOP 4 STRT 4 STOP 5 STRT 5 STOP 6 STRT 6 STOP 7 STRT 7 STOP 8 STRT

70

No. TP2.	374455	Rev. Na.
Page _		of
Dane	9 Julu	1974

Item 42

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 23

TEST DATE: 270-77			TEST	TIME:	54		
NOTE	Sr						
						·	,
					-		
	·.						<del></del>

Item 9 FFDI VERIFICATION Photo 291 44.007 B/45 4.006 Bras OPTICAL DATA

ANGLE

BACKGND INTENSITY

BACKGND

INTENSITY

TEST CONDITIONS

SOLAR

SIMULATION

EARTH IR

SIMULATION

CHAMBER PRESSURE

ENVIRONMENT

TEST ARTICLE TEMP - °C

COLDWALL TEMP - C (avg)

OPTICAL	. UATA			. 006 2	4.465	
			FIE	LD ANG	SLES	
RETRO	DATA	0	+15	+30	-15	-30
	PHOTO NO.	292	293	294	295	296
	LASER	,87	.88	. 88	,88	.87
D	FFDP-ANNULAR	.10	.045	*** 033	.048	.008
- 1	RATIO-ANNULAR	.12	.058	** 036	.059	.009
•	RATIO-FULL FIELD	1.28	.78	.35	.82	.039
	PHOTO NO.	297	298	299	300	30/
_	LASER	.88	.88	.87	.87	.87
E	FFDP-ANNULAR	.11	.060	.00744	.06/	.014
	RATIO-ANNULAR	./3	A-078	-0// 44	.065	.016
	RATIO-FULL FIELD	1.28	.75	.096	. 8:5	.10
	PHOTO NO.	302	303	304	305	306
2	LASER	. 88	.88	.87	. 87	. 37
<b>/</b>	FFDP - ANNULAR	.093	.030	## .008	1054	.013
·	RATIO-ANNULAR	.10	.015	008	.06/	H# .015
•	RATIO - FULL FIELD	1.26	.80	040	.8/	.10
RATIO	= FFDP/LASER OU		FF	DI MET	TER RE	

PLANNED

Anb.

Asb.

ACTUAL

Amb 375

RETROBES SOTOR TEMPERATURES

ᄺ	EIROR			PERATU	RES - °C			
			TRO X			RETRO Y		,
S	TABIL			Δ <del>T-RAD</del>		ΔΤ ΑΧ	ΔT RAD	
L	SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22	
	STRT	36	37.5	36	35,5	+41	±73	08155'S
1	STOP							
2	STRT				~			
2	STOP							
3	STRT						. ·	
[3	STOP							
4	STRT					`		
4	STOP							
5	STRT					<u> </u>		
5	STOP						1	1
E	STRT					]		1
$\epsilon$	STOP							١
7	STRT						=	
7	STOP							1 1 1
e	STRT	/						1
Ε	STOP	7				<u> </u>		1
-				<u> </u>	<u> </u>	<u></u>		'I

No. 1P2374455
Pageof
0 == 9 July 1974

Item 42

10.2 TEST CONDITIONS AND DATA LOG TEST NO. 24

TEST DATE: 8-16-74	TEST	TIME: FROM 1030 TO 1052
NOTES:		

## RETROREFLECTOR TEMPERATURES - C

	RETRO X		RETRO Y			
STABIL.			AT RAD		ΔΤ ΑΧ	ΔT RAD
SEQ.	DAS 14	DAS 15	DAS 16	DAS 20	DAS 21	DAS 22
ISTRT				,		7
1 STOP						//
2 STRT	(					/
2 STOP						
3 STRT						
3 STOP		• • •				-
4 STRT						
4 STOP						<del> </del>
5 STRT.						
5 STOP						
6 STRT						
6 STOP	<u>-</u> 1 144.	. /			1	
7 STRT			1 1 1 1 1			15.
7.STOP						
8 STRT						
8 STOP					1	<del>                                     </del>

TEST CONDITIONS

ENVIRONMENT		PLANNED	ACTUAL	
CHAMBER PRESSURE		Amb	Anb	
TEST ARTICLE TEMP - C (avg)		Bab	Amb Amb	
		Anb		
SOLAR	ANGLE	_		
SIMULATION	BACKGND			
	INTENSITY	Y		
EARTH IR	BACKGND			
SIMULATION	INTENSITY			

OPTICAL DATA 4.007 BIAS FIELD ANGLES RETRO DATA +30 -15-30+15PHOTO NO. 308 309 310 LASER 86 86 .87 86 .87 FFDP-ANNULAR 065 .035 RATIO-ANNULAR 16 078 075 RATIO-FULL FIELD 1.27 80 058 PHOTO NO. 312 314 316 LASER 0.86 FFDP-ANNULAR RATIO-ANNULAR RATIO-FULL FIELD PHOTO NO. LASER FFDP - ANNULAR RATIO-ANNULAR RATIO - FULL FIELD

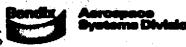
RATIO = FFDP/LASER OUTPUT

.17 ıιΨ

1.25

FULL FEB

ORIGINAL PAGE IS POOR



						. /	1100	/Adme	475	MAG	SAL	TH.	Seco	240	رايم عمل	well	·s .	٠.						FFTP	
19	); 74	<u> </u>	1007	.047	.005		.005	.001	.001	<b>2347</b>	.001	A PACE PA	7A RAC ,000	,00€ ,∞6		, eo 5 ,	,	, 205	1005	.005	.005	1		RATIO	
ate	10	ime -24Hr	FALL	1/2	0-60	60-120	120-150	190-240	RV0-300	300-360	Fuce		Fuu	1/2	ه-ده	60-120	•	•		. •	. •				
	Т	FFDF	-11	.072	.671	.020	.027	1019	.072	.032		~	. 14	077	026	.020	.029	.02/	,024	.046		+	+	1	┝
Z	2	Onu	1.28			ļ	L				1.26	-	1.78	7						-	1,28	1	1	<del>                                     </del>	┢
			. 662	1035	-012	017	.016	009	.013	·01 I		` .	680	.042	,617	.012	.020	.018	.018	.016	1	†	1	<del>                                     </del>	
		15	.78	٠.	<del> </del>						.77		.80								. 80	1	1	<del>                                     </del>	一
		30	037	.021	610	.01.1	·010'	,007	.008	.006			.0/1	008	.006	. 603	005	.067	,007	.006			•		┢
	<del> `</del>	-	.34		<del>                                     </del>	<del> </del>	<b> </b>	<del>                                     </del>		<u>.</u>	.34		.082								453				Γ
	-	15	,059	.03Z	, 81 Z	-014	.019	.010	. 00 7	.016	ļ		1072	.038	,013	0/5	.0/8	,019	.013	.019			Ī,		
	<del></del>		84		<del> </del> -	ļ	<del>  .</del>	<del> </del>			.83		.82			<u> </u>					.82				
	-3	30	.40	.008	006	1007	.006	.002	.003	.003			008	007	006	003	.005	. 006	.006	.006					
			•404	MAY.	na weo	4 560	1194 801	<u></u>			.035		.050								.050				
4	WAY NA	20.364			. o. 4"									***	.005							1_	1		
- 25	~ 1~		.28	<u> </u>	076		GREA	KTHRE	44					.045	, 505 °	.005	.005	. 004	1006	,006	315	<u> </u>	80	NKTI	
F	1-	25		125	.075	=	-25	,08		120	-F-	0	.12	, 076	.024	. 016	.018	.024	,027	1039		40	0	127	_
			42		18		ļ	.27	<b> </b> -	.63		<u> </u>	1.26								1.26	+	4.5	,74	1.0
	-	20		+20			-20	<del></del>	120	,		+15	.857	.024	1013	.016	,014	.015	10/0	015		+	4 15.	78	<u> </u>
			.79	كالد	.82			,62		.80-			.007	006						-	.00	+-	+10	162	<u> </u>
	٦	. 15	•	-13			-15	10	+15	-		A 30	.038	006	.004	006	,605	.006	1006	۵٥٥.	.040	╀	+ 30	_	1-
	1-		. 97	A /0	,98	14-17		.99		.47			.048	.035	.017					د در ماکیر چا		+-	+ 40	111	-:
		10					-10		410			,15	.8/		UT	-,014	013	. 518	2014	, out	.81	+	1 1 1	1	
مدر		-5	1.15	+5	1,13		ىم	1.16		1./3			1014	.0/6	.007	.001	.006	.008	.007	.co7		+	+6:	9.0	-
		7		7.			-5		75			- 70	.10				- 5		,ω/	.007	.10	+	+	+	-
		<u> </u>																				+	+	206	1 .0
	1	0	1.27			. 7	1.28												<del></del>			╁	+	<del> </del>	<b></b> -

for each test parameter to be monitored.



INERIA-OPTICAL TEST

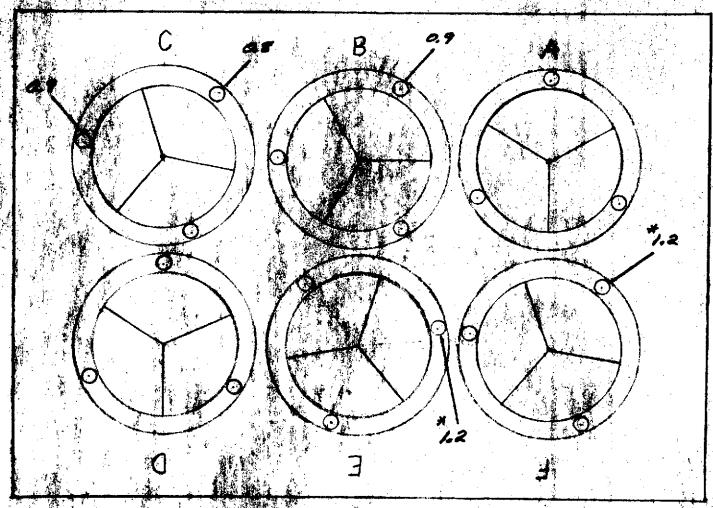
		1.
	of	
The state of		
Date	9 dely 19	*

1013 Replect To again View fication

2013 Present 9.8

Chances show below; oll others account at 19 mill.

Millio ocional telzanice.



REPROPOSE TELITY OF THE ORIGINAL PAGE IS POOR



Aerospace Systems Division

	,	Δ			_	
-	_	~	G	Æ	1	•

THERMAL- OPTICAL TEST

(73)	772374455	1, 1, 1, 1, 0.
7	Page	. of

Date 9 Joly 1974

10.4 FFDI POLAROID FILM EXPOSURE TABLE

,		FIEL	D ANG	LE	126 s
RETRO		+15	+30	-15	<u>-3o</u> _
A				1250	
- <b>B</b>	1/250	1/125	115	1/250	//30
C	1/250	1250	/30	1/250	/30
D	1/250	1/250	160	1/125	1/8
E	1/250	1250	1/15	/125	1/15
F	1/250	1250	1/8	1/250	1/15



Aerospace Systems Division

1	A	4	F	/	<
_	~	•	•	~	_

THERMAL-OPTICAL TEST

V 7 43	/77102			
			<del></del>	
			_	
1_				
I Page		nf _		

Date 9 July 1974

10.5 TEMPERATURE DATA LOG

ORIGINAL. PAGE IS OF THE



LAGEOS THERMOLOPTICOL TEST 772574455 REV.MD. (2)

	F	•	G.		Macib	Haziè	3	3	٠	TEST I	PARAJE	TER DA	ta reci	ORD CF CAS	ioale	ΛTa	Δτ.	Uno stera.	D	Y=~=	AT.	ĀŤ.	LOMTA	J. 1175	Q <sub>ET</sub>	
	ate	Time [0-24Hr	1	ک	4	5	6	7	8	٩	1.0	11	12	13	14	15	16	18	19	20	21	22	23	24	25	
	اد/مر		-2.74	-1.59	-2.29	-2.29	-10.61	-1.62	-1249	-9.91	-५:६।	-5,58	-2.41	- ዛ. ዓን	-331	10.38	+0.28	- 2.45	-243	-308	10.15	10.05	.234	-2.46	- 2.54	76
	16/70	1530	+71	<b>ት</b> ገ	185	+85	-208	-87	-310	-1]}	- 5	-17	-12	+ 3	124	+ .3-	_	+80	+80	161		_	+81	+80	+77	1
																							- 2.57			:
ò		1300																+73					176			ı
		1330														$\overline{}$					+.194		266			
Ś					+86								-246		+9			+69					+74			
10		14 00										13 30	-8.40 -13.8	-15.77	-1								-212			
		1500			180							10.		31 (4				167					+72 -1.20			i
			-4.47	72.03	- 2.11		12.10	12.6	-12.60	-12.57	- (11)	-10.2	- 1.35	-16.60	-4	7.721	+.40	-1.3	-1.23	+4	T. 510	7.140	- 1.20	-1.2 /	-1.4 <del>4</del>	
			<del></del>	<del>                                     </del>	<del> </del>				<del>                                     </del>						<del> </del>		<del>                                     </del>	<del>                                     </del>		<del>                                     </del>	<del> </del>		<del>                                     </del>			ł
			,							l	ļ — —		<del> </del>		·				·	-	<b></b>					ĺ
												<del> </del> -	<u> </u>			<u> </u>	-		-	· · · · · ·			<b></b>			ĺ
																										ĺ
										,							٠.									ľ
		``																								
			<u> </u>				ļ. <u></u>	ļ	<u> </u>	<u> </u>		<u> </u>									<u> </u>			,		
	an.										<u> </u>		<u> </u>	<u> </u>	<u> </u>			ļ				<u> </u>	<b></b>			
		,	<u> </u>		ļ	<u> </u>			<b> </b>	<u> </u>	ļ		<u> </u>									<u> </u>	<u> </u>	<u> </u>	<u> </u>	1
	· · ·		<u> </u>	<del>                                     </del>		ļ		<u> </u>	<u> </u>		ļ	<b>├</b>			ļ		<u> </u>		ļ			<b></b>	<del> </del>	<del> </del>		1
			<b></b>	· ·	6.		ļ ,	1	-	<b> </b>	ļ	ļ			J 1			<del>                                     </del>				<del>                                     </del>	<del>  </del>	<u> </u>	<u> </u>	
	<del></del>		<del> </del>	<b> </b>		<b> </b>		-		<del> </del>	<del>                                     </del>	1			<del> </del>	ļ	<del> </del>		<u> </u>	ļ		<del> </del>	<del>                                     </del>	₩-	<b></b>	1
			<del>                                     </del>	<del>                                     </del>	<del> </del>	-	-	1	-		<del> </del>	<del> </del> -	-	-	<del>                                     </del>	├	<del>-</del>	<del> </del>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	<del> </del> -	<del> </del>	<del> </del>	<del>├</del> -	1
		<u> </u>	<u>L</u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1	<u> </u>	1	1	<u> </u>	1	1	<u> </u>	<u></u>	<u> </u>		<u> </u>	<u></u>		1	1	1	]

Enter appropriate data system termination symbol for each test parameter to be monitored.

THE BOOK-COTTICOL TEST

110. 772374465

		/\.e.o.	AR	o ja	geor .	See Co	* 5 4	₹.	Tel.	PAPAMET Q* •	TR DAT	A RECO	<u>PLD</u>	
	Time [0-24Hr	26	27	20	29	30	31	32	33	34	•	•	•	
าบ	1230	-1.81	-1.80	9.74	15.12	,40	46	-	-3,36	-3 2 y				

				L	<u> </u>	L.	1	i	1					1	I	1						1 '	1 1	1 )
8/6/70	1230	- 1.81	-1.80	9.74	15.12	.40	46	-	-3,36	-324							<b> </b>	<del></del>						<u> </u>
10170								ı	1															
	1300	-183 148	-1.82	9.12	1504	-41	.45		-368	-167														
<u> </u>	1300	198	198	~	-			-																
	1330	- 187 +98	-1.82	9.11	15.02	.41	.44	-	-3.67	-3.68														
-	,,,,,	198	19 E									<u> </u>												
	1400	-1.¥3 +98	· I. B 3 .	4.70	14.44	ų I	45	· <u>-</u>	-3,70					<u> </u>				<u> </u>						
<b></b>		+78	115					<del></del>		-			-	<b> </b>	<u> </u>	<u> </u>								
			-										<del></del> -		ļ	<del></del>			<b> </b>		<b></b>			
			161											<del> </del>	<del> </del>	<u> </u>	ļ				ļ!	-		
] ,						· .					<del></del>			<u>.</u>		<u> </u>	-	·			<b> </b>	-		ļ
_								- , -	· · ·					-	<b></b>						<b> </b> -			
										-										<b></b>	<b> </b>	ļļ	<b></b>	<b></b>
						1 .											-		-					<u> </u>
											· · · · ·								-			<b> </b>		
																						· -		<b> </b>
			l																-					
															4									
		1								-	ar :													
.	ŀ					<del></del>		- '						·										
7											`													
	ŀ			<del></del>	<del></del>		1						·				ļ							
<u> </u>		1					i							. 1	]			·	Ī	` `		1		

<sup>\*</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

Bench: Aerospace Systems Division

LAGEOS THERANL-OPTICAL TEST

10. 172374435 | RIV.NO. (29

P

## TEST PARAMETER DATA RECORD

ate	Time (0-24Rr	14	15	16	19	20	2/	22							• i	•	•							
06	1705	-3.20	<del> </del>	-2.60		-2.18	-2.72	-2.87						1			-	<del>                                     </del>		-	┼	ļ	<del>                                     </del>	╁
·	-	58	67	75		64	72	67	<u> </u>	<u> </u>										<b> </b>	1	<u> </u>	<del> </del>	╁
•	1211	-3.21	-2.18	-2.62	·		-2.74	2.89	<u> </u>									-	<del>                                     </del>		<del> </del>	<del>                                     </del>	<del>                                     </del>	+
		57	67	75	<u> </u>	64	71	67									1		<del>                                     </del>	<del>                                     </del>	<del> </del>	<del> </del>	<del>                                     </del>	<del> </del>
	1800	-3.01	-	-254			-2,45	-2.76							<b> </b>					<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	┼╌
<del></del>		64	7.	77	<b> </b>	<b>PS</b>	74	71	ļ	<u> </u>						1			1		<del>                                     </del>	<del> </del>	<del> </del>	╁╌
	1920	• 2.22 87		-2.06	<u> </u>		-2.11	-2.17			<u> </u>									<del></del>	1	<del> </del>	<del> </del>	$\vdash$
			8.8	91	ļ <u>.</u>	87	90	18		ļ	<del> </del>										† — —		<b>!</b>	┼-
	2010	·1.92	97	-1.86		-1.92		-185		ļ		ļ					<u> </u>					<del>                                     </del>		<del>                                     </del>
		76	7/	97		96	97	98		<b> </b>	<del> </del>	<u> </u>	<u> </u>	<u> </u>										<del>                                     </del>
				<u> </u>	<del></del>	<del> </del> -				<u> -</u>	<del> </del>		_						·					<del>                                     </del>
		-3.08	7 77	-2.53	-2.25	2 0 2	-2.48		<del></del>	<del> </del>	<del> </del>	<u> </u>	ļ	Ĺ		<u> </u>	<u> </u>							
	1720	41	70	78	86	64		-2.8			<del> </del>			<u> </u>	-									
·			75	<del></del>	• •	99	73	. 67	<del></del>	-	<del>                                     </del>				<del> </del>	ļ								
,			٠,								<u> </u>	<del> </del>	├				ļ							
												<del></del>		<b> </b>		ļ	<b> </b>							
	·	· · -				· ·				-	<del> </del>		<del> </del> -	ļ	<del> </del>	<del></del> -	<b> </b> -			· · · ·				
									,				<del></del>	<del> </del>	<del> </del>									
													<del>                                     </del>			<del> </del>					ļ			<u> </u>
										· ·						-	-					<b> </b> -		<u> </u>
			]							,	-		-		<del> </del>	<del> </del>			· ·			<b> </b>		├
. ]				]	]											<del>                                     </del>					-			<b> </b> -
Enter												-			<del></del>	<del> </del>	<del> </del>							

 Enter appropriate data system termination symbol for each test parameter to be monitored.

Sendby Aerospace Systems Division

LAGAUS THERNAL-OFFICEL TEST 772374455 REV.NO. 60

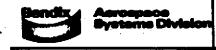
OF

## THEY PARAMETER DATA RECORD

		Time	•		12	12	,,,	•	•	•	•	•	•	•		•	-	•	•	•	•	•	•	٠	•
	<b></b>	(0-24Hz				13				18			21	22.		2,4						<u> </u>		4	
	57	1651				2.31														,		ļ			· .
-	••••		67			1.85			68.5				2.83	_		3 64			-,						ļ.—.—
		1703		67.9		67	69		60.7	69		50.7	49.5		68	63	68								
		10.22				2.20			2.78			2.78				2.19					<del></del>	<b></b>			<u> </u>
L		1732				695		70.2			17:20		76	70	70	70	_								<u> </u>
Г																									
-									ļ														-		
1											, ;											<u> </u>			
-			·									-				<u> </u>	-								
																			,			<del>                                     </del>			<u> </u>
-																-						<del>                                     </del>			
				!							·								,		<del>                                     </del>	-			
Γ																				~	<b></b>				
L							·							77											<u> </u>
	.																								
-																			-	ļ <u>.</u>	ļ ·				
1	ı		<del></del>			-				-			•								<u> </u>	ļ			<u> </u>
$\vdash$			-	<u> </u>	•				-				·				<del> </del>					<b>-</b>			
		•							~	,		, · , · · ·	· .								-	-			<del> </del>
												ļ. <del></del>					-					<u> </u>			<del> </del>
	1	Ì										<u> </u>			•		<b>-</b>	<del></del>			<del> </del>	_	<del></del>	-	<del> </del>

Enter appropriate data system termination symbol for each test parameter to be monitored.

°C



LAGEOS THERMOL-OPTICAL TEST

110. 17/23/24455 | REV.MO. (

#### TEST PARAMETER DATA RECORD

		Xfore	XAPEK	KTAB	YUP THE	Xen	6 Yface	YAU	YAA?	Yu 100	Yer mi	YPETM	(6			٠.								
		•	•	*	•	*	•		•	•	•	•	•					. •	٠	•	•	* **	٠	
	Time [0-24Hr	1	15	16	18	19	20	2/	2,2	23	24	25												
9/00/	2/:30	-5.74	-5.33	-528	-5.62	-5.68	-5.14	t. 022	+.40E	-5.62	-5.58	- 5.77									<u> </u>			<u> </u>
109714	27:30	-30.0			-28.0						-27.o	7			· · · · · ·									
			-593	-6.02	-5.85	-5.85	-5.96	r. a 83	1.0/5	-5.78	-5.82	-5.91									<u> </u>			
	12:00	روتيد. در دويد	.273	-3t,15"	-52.	$-i\delta^{2}$	- 29,3	+1.54	1.35	-23	-25	-270		· · · · · ·	•				·		1		-	<b>†</b>
		-6.88	-6.26	-6.44	-5.97	-5.94	-6.46	†.  20	+.038	-586	-596	-5.99									<del>                                     </del>			
•	22:30				-34-5									ì						<del></del>	<del>                                     </del>	-		
	2300				-6.05																<del>                                     </del>			<del>                                     </del>
	2300				-36.0															· · ·			<del></del>	$\vdash$
og/ah	200				-6.08																<del> </del>	ļ		<u> </u>
1-714	0003				-31.5														<b></b>		<del>                                     </del>			┢
					-6.10											,,,,,,					<del> </del>		<u> </u>	<del> </del>
	0033	-60.8	-47	-52.8	-37.0	-350	-57.2	3.38	.72		-31.5			т.								<u> </u>		$\vdash$
	.1.0				-6.10										<u> </u>								<del></del>	-
	oloo				-37.0	1				_										<b></b>	<b>†</b>	<del></del>	<b></b>	<del>                                     </del>
					-6.11																<del>                                     </del>	1		<del> </del>
· . ·					-37					-34													<del>                                     </del>	-
•					-612													<del>                                     </del>	<b> </b>		<b>†</b>	<b>—</b>	<del>                                     </del>	╁╌
	0152				-31						-37.5											-	<del> </del>	十
	0237				-6.11												<del>                                     </del>				+	<b></b>		<del> </del>
	0727				-37														<del></del>		<del>  -</del> -			╁╾
	0300				-6.12																-		<del> </del>	†
	U 300				-37										3.72	1				<b></b>	<del>                                     </del>		<del>                                     </del>	<del>                                     </del>
																				<del> </del> -			<del> </del>	+
																		<del>                                     </del>	-	<del>                                     </del>		<del></del>	<del></del>	+

 Enter appropriate data system termination symbol for each test parameter to be monitored.

		13, 62	400	30	Retir	Rosel	) 	Cocou		<u> </u>	75.7	ARTICLE	- Table	optowerld   Rocker	1	RAGO.	METALI 4	1	Service Services					٠.,	
pate	Time (0-24Hr	00	01	oz	04	05	#3T 06	емт 07	Disk. 08	Sm7H 09	10	"	12	13	<b>34</b>	26	27	AL 1643 28 66	29		•	•	•		
08/08/	2020	-402	-2.59	278	-2.78	-7.79	-2.81	-2.84	- 2.90	2.84	- z.84	-z.83	-2.7	-2.84		1.76	-1.75	,Š/	49						1
774		4.023		-270		70	69	68	66	68	68	69	68	67		100	101								
	2040	-402	-2.58	<del> </del>	2.65	<del> </del>	-6.35	-3.41	<del></del>	-3.11	-415	- 4.15	-3.97	- 3.98		-1.78	-1.79	9.5	15.3						1
-	,	33	76	73	74	74	-42	+51	.309	160	Z9	29	34	34	<u> </u>	100	99							,	]
	2110	-402	-2.60 75	- 265	- 2.69	<del></del>	12.27			· · · · ·	- 2.68	-5.67	-5.67	5.67	 	-1.87	-1.87	9.6	15.4						
}	<del> </del>	33	- 2.61	- 2.66	73 -2.10	73	-296	-315		-3/5	-20	-20	-20	-20	ļ	99	99								
	2130	33	75	73	69	<del>1</del>	-12.37 - 302	- 316		<del> </del>	<del></del>	<del></del>		<b></b>	ļ	-/.83	-1.82	9.6	15.3			ļ		<u> </u>	]
		-4.02		- 2.66	-2.9/	70		-12.57	1	-316	-22	-22	-22	22		98	99	0.50		<u> </u>			ļ	ļ	1
}	22:00	33	75	73	66	67	304	-315	-314	-316	-5.79 -24	-5.79	-5.79	-5.79 -24	ļ	-1.82		9.59	15.4				<b> </b>	<u> </u>	┨
	0.212	-4.02	-2.62	-2.68			-12.40	-		<del></del>	-5.62		-5.80			-1.84	99	953	15.3	-	ļ		<b> </b>	<del> </del>	┨
	22:30	32	75	73	64	64		-316			-25	-24	-24	-24		98	98	1.97	13.3		- }	<b>_</b>	<del> </del>	<u> </u>	┨
	2300	-4.03	-2.64		-3.06	-3.65		12.58		<del> </del>	-5.85	-5.84	-5.62	<del></del>	<del>-</del>	-1.84	1.84	9.47	15.2				<del> </del>	<del>  -</del>	┨
		32	74	72	62	62					-25	-25	-25	-25		98	98	1.7/				<del> </del>	<del></del>	<del>                                     </del>	┨
08/09/14	ms	-4.02	-2.66	-2.74	-313	-3.12	-12.40		-12.54		-5.7 <b>6</b>	-5.15	-5.76	-5.76		1.82	-1.82	9.53	15.30	* 17	CREASE	O MAI	VIPULAT G TO	PAL NO.	١,
/*	رکس	33	74	71	60	60	-304	-316	-314	-316	-23	-22	-23			99	99		1.00		MAIAE	387710	9 To	= 20	1
ŀ	0038	-4.02	-2.66	-2.66	- 2.99	-2.57	-12.4/	-12.57	-12.55	-12.57	- 5.80	-5.79	-5.78	-5.79		-1.85	-1.84	9.50	19.45				- ; -	<del>                                     </del>	1
	0070	33	74	74	64	<u> </u>	-305	-316		-3/6	-24	-24	- 23	-24		98	98							<del></del>	1
	0100	-4.62		-2.79	-2.73		-12.40				-5.79	<u>-5.78</u>	-5,18	-5,78		1.84	1.84	9.55	20.04		1 A 1				1
		33	73	70	71		-304		-313		-14	-23	-23	-23		98	98								1
	0130	- 4·07		-2.81		-262		1259					_	<u>-5.77</u>		1.84	1.64		19.99	¥ 85	PEAS	M	אַיוּאַנ	TOOL H	<b>)</b> •
. 4		33	13	69	75	75		-316			-23	-23	- 23	- 13		98	98								]
	0152	<b>-4∙03</b> 3Ն			-2.69		-17.44							-5.78	<u> </u>	<u> </u>	ļ								]
L	L	30	12	68	13	13	-307	$[-3]^{q}$	_317	-318	-23	-23	-23	-23	l '	1	[	t	ł	1	]			,	1

Enter appropriate data system termination symbol

for each test parameter to be monitored.

oF



LAGEOS TNERMI-OFTICAL TEST PAGE COP PAGE

			zik	75°C	King P	JAKEP.	arigh	•		148 <u>7</u>	APA I	TER DA	TA REC	) ) 	. Ciyek	ave.	. •	1 (	ا العراقة	liked.	West.	اير	000		
		-	<b>3</b> 00	<b>(</b> K	•	*	4	***	6	o. Day	5	7.	*	•	•		•		AC V.	ACV	A V.	•	•	•	-
( * 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1	ate	<b>Time</b> [0-24Hr	٥٥	01	02	04	05	06	07	08	09	10	II	12	13		26	27		29	30		33	,	
24°	08/9/14	0237	4.02	-1.64	- 2, 85	-2.80	- 2.78	-12.43	-12.66	-12.57	-12.60	-5.76	-5.75	-5.76	-5.77			1.84	+9.45	18.27					
757	عداد لهم	0071	33	14	ሬዩ	69	70	-306	-317	-316	-317	-23	-23	-23	-23		98	98					· · · · ·		
#1	:	0300				-7.79		-12.95							-5.71		-1. <b>8</b> 5	-1. <b>64</b> 98	9.5	18.30					
	· · ·		33 -402	74	-7.16		-7.75	-36.7 -12.21			-317		-23	-23	-23 - <b>ごフフ</b>	<del> </del>			10.01	וא עו	57.2	<u> </u>	-3.23		<del>                                     </del>
		0400	33	75	68	71		-296			-3/7		-22		- 23		98	98	, 0.07	70.77	7,5		- 5.65		
.4		04/30	-4.02	-2.63	- 2.76	-2.75	-274	-17.27	-12.59	-12.58	-12.60	-5.75	-5.74	-5.75	-5.7L		1.84	-1.23	9.91	18.31	57.37		-3.19		
•		0730	33	75	48	7/	7/		-317		317			- 22	-23	<b> </b>	99	97			ļl			<u> </u>	
KF.		0500	33	-2.43	-286	-2.74 71		-12.23 -296			-318	- 23	- 23	-3.76	-5.76	<u> </u>	-1.83 98	-1.83	9.57	18-35	55.36	<u> </u>	-3.16		
•				- 2.62								•—-	<del></del>				-1.84		9.95	16 17	57,31	· ·	-3.19		
		0530	33	75	68	7/	12	-2%	-3/7	-3/4	-3/7	-25	-25	-23	-25		98	98	7,7,5	787.7	777		211.1		
		06W	-4.02	-2.42			-2.73	-12.23	-12.40	-12.58	-1240	- 5.79	-578	-5.78	-571		-1.84	-1.84	994	18.05	57.18	- 7	-3.21		
	,		33	75	68	72	72	-2 <i>9</i> <u>८</u>	-317	-314	-317	-53	-23	-53	-53	-	93	91				·			
, :		*1												<u> </u>	_	-						<b> </b>			
		المسترة		· ·											<b></b>	<del>                                     </del>					: -		<u> </u>		ļI
,																									
							<u> </u>				<b> </b>	<del> </del>	<del> </del>		-				1.		<del>                                     </del>	<del></del>	-	<del> </del>	<del>                                     </del>
,		·an	-			<b>-</b>				· <u>-</u> ·			<del> </del>			<u> </u>						<del> </del>	-	<del></del>	<del>                                     </del>
ζη.											<u> </u>					1		<del>                                     </del>	-	1	1	<del> </del>		-	
8 S										_										.,					

Enter appropriate data system termination symbol for each test parameter to be monitored.

Bendix Aerospece Systems Division LAGEOS THERON-OPTICOL TEST

PAGE 7 09 --- PA

°C

# TEST PARAMETER DATA RECORD

		Xface	XAME	X TAB	Kyti	XW.	Yface	YAGAL	Ymd.	YMEN	· Yum	YH.				4.2							
ate	Time [0-24]	14	15	16	18	19	20	21	22	23	24	25	24		•				•			•	
1/9/1	0400	-7.00	-6.46	-6.74	-6.00	-5.94	-6.99	+.160	7.034	-5.92	- 6.04	-5.47	-	 1		<u> </u>					<del> </del>	<del>                                     </del>	†
1/1/1	4 0400	-54		-42.5			-54			-33.5								t			<del>                                     </del>		╁
\	ada	-6.89	-6.37	-6.62	-5.97	-5.7/	-6.85	4 .150	+.035	-5.90	-6.00	-5.95						<del> </del>		<del>                                     </del>	<u> </u>	<del>                                     </del>	†
<u>l·</u>	0430	-51.5	-42	46.5	-345	-33	-51	2.94	1.69	- 33	- 35	-34						<del>                                     </del>	<u> </u>			<del> </del>	十
	700	-6.82	-6.31	-6.54	-5.95	-5.90	-6.75	1-11-11	+034	-5.87	-5.97	-543		 1				一	<u> </u>	1	<u> </u>		十
	0500	-50	40.5	-45	-34	-33	-49	2.66	+ 64	-32.5	-34.5	-17:5						<del>                                     </del>	1		$\vdash$		t
		-6.78	-6.28	-6.50	-5,93	- 5.88	-6169	+.137	1.033	-5.87	- 5.76	-5.92								<u> </u>	†		十
<u> </u>	05%	-49.5	-40.0	-44			- 48													<b> </b>	<del>                                     </del>		十
1		-675	6.26		-593		-6.65								. ,		·	1			<u> </u>		t
	0600	49.0	-39.5	-43.5	-33.\$		- 47.0					33.5										<u> </u>	十
		-4.68		-6.55	-5.52	-5.12	- 6.81	+.118	+.aty	- 5.75	-5.57	-5:13							<b> </b>		<del> </del>		十
.	0910	-11	-37	-45	-26	]	1	+ 3.36			-27									+ -		<u> </u>	╁
د 📗	0940	-422	-5.97	-6.37	-5.39	-5.00	-6.69	+ 174	+.024	- 5.70	-5.51	-5.07										<u> </u>	†
	0710	- 8.5	-74	-42	- 2 Y	-17	-48	13.28	+.45	- 19	-26	- 12								<del>                                     </del>			+
••	1010	-4.19	-5.88	-6.27	-5.35	-4.95	-6.61	+,169	4.016	-5.69	-5.48	-50E										<u> </u>	十
		-2.0	- 3 Z	- 40	- 23	-16	-46	+3.15	1.30	- 29	- 25	-/7								<u> </u>		<u> </u>	†
·	1040	-1.44	- 5.86	-6.32	5.35	-9.97									4.						<u> </u>	<del></del>	十
`	70.10	-7.					- 45														<u> </u>		t
7		-426	-5.82	-6.19	-5.32	-4.43	-6,54	1.164	+.015	-5.66	-5.47	-5.05						1		<u> </u>	<u> </u>	<del>                                     </del>	十
<u>.                                      </u>	Hio.				-23	l		13.09							c	~			-			<del>                                     </del>	t
	1140	- 4.13	- 5.81	-4.17	-5.31	-4.91						-4.13						1		<del>                                     </del>	<del>                                     </del>	<del> </del>	+
·	1,32	- 2	-31.5	-37	-22.5	-15_	-44	+3.06	t.25	- 21.5	-24	-15.5						1	<u> </u>	<del>                                     </del>	<del> </del>	<del>                                     </del>	+
	1200	-298										-4,68					1		<del>                                     </del>	<del>                                     </del>	<del> </del>	<del> </del>	十
	.	+/	-3/	-375	-21.5	-14	-43.5	+300	+.15	-28.5	-24	-145		1	<del>                                     </del>	<del> </del>	<del> </del>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	+	<del> </del>	+-

Enter appropriate data system termination symbol for each test parameter to be monitored.

Bendix Aerospece Bystems Division

LAGEOS THEOMPI-OPTICOL TEST

HD. 776374465 REV.HD. (

•			<i>X</i>	X4	<u> </u>	X	Y	v		TRAT	PARAJE	TRA DA	TA REC	ORD		•		· .							
	_		-	/ Lagran X	~yyys	4444	1880	Aus	IAX	TRAL	Holing	Yuza	e Yad	5.6											
<b>,</b>	pate .														•					֓֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		•			
	<i>चीतृ</i>	1330	3,78/	-5758	6.125	5.328	-4.806	-6.428	+.149	-,015	-X630	-634	-4705	.963					<del> </del> -		<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	╁
/N	47774	12.30	سى بر	- 30	-37	-2/	-/3	-43	+2.81	- 28	-28	*235	-11.5							<del>                                     </del>	1	<del>                                     </del>	<del>                                     </del>	<del> </del>	╆
1,5	1		-3384	75.67/	-6254	5.168	-1.714	.6.357	+.14.5	017	5.611	3,000	- 4.415	821	<u> </u>			<del>                                     </del>		<del> </del>		<del>                                     </del>	<del> </del>	<del> </del>	╁
K		/	<i>+//</i>	- 29	- 36	-/2.	-/2	-91.5	12.70	- 92	- 28	24	100	l .			· · ·	-	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	<del> </del>		<del>                                      </del>	╀
Ņ			- T 44 F	- 5 42 2	-411	- 5.440	_ 4 609	- ( 7.0	1 144-0		-5.60	-6.234	-4 519	902	<del> </del>		<b></b>		<del> </del>	<del> </del>	<del> </del>	<del>                                     </del>	├	<del> </del> -	╀
-1	ł	/320	+15	-28	-35	-19	-11	-40.6	12.64	40	- 27.5	-2/	- 25	347			<del>                                     </del>	<del> </del> -		<del> </del>	1	<b></b>	-	<del> </del>	Ł
1		1340	-3.449	-5.650	-6.009	5/8/	4761	-63//	1.139	015	-5.60X	-5.825	4685	a.		<b></b>	ļ	-		<del> </del> -		<del> </del> -	ļ	<del> </del>	╀
		1.	1 1 1 1 1	7 / 4	~ Z Z '	l - 26	-12 -	at/	127		- 27-				-	<del> </del>	-	<del> </del>	<del>                                     </del>		<del> </del>			<del> </del>	╀
		1400	-3.840	-5.485	-6.624	-5.127	-4.125	-6.31+	+ .140	014	- 5.630	.5.31/	7/12/	1.04		-		<u> </u>	<del></del>		┼	<del> </del>		<del> </del>	Ļ
i		r (	マンツ	- 6 1	- >> -	- 24.7	-17	l – T/	127/4	~~~	1 - 2.8	1-75	1 x 17 C	***				-	├	<del> </del>	<del>                                     </del>		ļ		Ļ
		/4 Z o	-3.857	-5.689	-6.675	-5.219	4.817	-6-337	+.143	- 007	-5.647	-5.724	-4.744			<del> </del>		<del> </del> -	<del>                                     </del>			-			Ļ
		/4 Zo	+3.6	-29	- 35.5	- 26.5	-17.5	-91	. 7 20	- 12	-28	-21.5	-13			<b></b>		<u> </u>			<del>                                     </del>		ļ		Ļ
^		1430/1	4.04	-5.7n	_/ ^4	F 23	Agn	440		/3		6 47				<del></del>	ļ	ļ		<del> </del>	1		<u> </u>		L
		1430/1	0	-295	_2C <	-3.62	-15.0	420	291	4.013	-28.0	220	-2.02			<b> </b>				<del> </del>	<b> </b>		<u> </u>	ļ	L
		1455/31	<u></u>	_/ ^/	7 15	C 53	62.0	147	2110	0.01	-28.0	-23.0	- 17.0	- ,			ļ		<u> </u>	<del> </del> .	<u> </u>		<u> </u>	<u> </u>	L
		H-55/3 H	-47 n	-3- 0	22.5	-2.21	2.20	42 =	*.157	4.094	-5.73	- 5.61	-56/			A in		<u> </u>			ļ	<u>                                     </u>	<u>.                                    </u>		L
ヿ			-17.0	_32.0	3 (· 3	-110	~ <u>[ 1.0</u>	131.5	7.22	0.63	-30,0	~4.5	-24.5		1.50	410	RADIAL	<b>!</b>			ļ		<u> </u>		L
	•	. I	<del></del>				-									<u> </u>		ļ		ļ				<u> </u>	
ł						-					-					<u> </u>	<u> </u>				-				Γ
	- 1	· · · · · · · · · · · · · · · · · · ·						· · · ·		·			` _							<u> </u>	<u> </u>				
ł															-	<u> </u>				<u> </u>	<u> </u>				Γ
-		ŀ								<b></b>							<u> </u>		· .						Γ
ł			<del></del>															ļ							Γ
		ļ																							Γ
l	لبَ ــــــــــــــــــــــــــــــــــــ																					, ,			T

Enter appropriate data system termination symbol for each test parameter to be monitored.

THERMI- OFFICEL TAST

		$\int \mathcal{T}$	A.	772	Blac	X	X Acres	X	THE L	40	Xed.	Yraca	74	Yand	1/4m	Y.	Yest	3,00		. '				
ate	7ime [0-24H	1			1		15	i .		l '	1	1 -	•	1	1 -	•	'l •	•		,				•
4/1/7	y 1542	-7.14	215	1.15	2.16	- 3.30	4.46	-5.52	-7.67	- 2.53	-179	-4.01	+ 417	+ 04	221	7/9	163	77				-	ــــ	_
	A 112.4X	<b>₹21.7</b>	1131.1	131.5	31.5	+12	- ]	1-2 <i>L</i>	_	154	122 (	-35	19.2	4171	-	197	136	<del></del>			<del> </del>	<u> </u>	<del> </del>	
	1600	2112	2,/92	-2.166	2/84	-3.657	- 4.257	×225	1	-2382	1663	-5.689	1 4 2 2	1,00	7 6 6	7 600	+ 55	-	3	-	<del> </del>	<del> </del>	<b>├</b>	
	1600	+3/	+31	31.5	31	+10	-3,5	-205		+27.5	+375	-29	+ # 0	4000	1775	12.337	7,702	وود	~,	<del> </del>	ļ	-	<del>  </del>	_
	1630	-2.28	-2.29	-2.21	2.31	-3.92	-416	-4.95		-2.56	-1.99	-5.37	1.303	//.33 i AGE	215	763	7 44	- 0			<del>                                     </del>	<del> </del>	—	_
	1630	29.5	29.5	29.5	29.0	+ 2.0	-2.0	-16.0		せてり	34.0	-23.5	/ 84	1.70	2 1 5	715	20.5	2.55			<del> </del>	<u> </u>	<del> </del>	_
	1700	-2.29	-2.30	-2.30	-2.32	335	-4.20	488		-2.70	-232	-2:52	4.384	+ 042	275	220	49.3	/ 62	· ·		<del> </del>	<del> </del>	├—-	4
		79.0	24.0	29.0	29.0	+10.0	-3.0	-14.5		22.5	28.5	-21.0	6.41	1.66	7 6	71.0	290	6.15		-	├		<b>├</b>	4
	+730	-2.28	-2.29	-2,28	-2.30	-3.24	-3.47	-4.72		-245	-1.84	-5.05	+.335	4.075	-74.7	259	7.0	7 19			┼	ļ	<del> </del>	4
		29.5	29.5	29.5	29.0	13.5	1.0	-120		26.5	36.5	-17.5	5,98	1.34	23.D	744.0	72.0	6.12						4
	(B00		ļ	<u> </u>	<u> </u>	-3.82	-3.99	-A.69		-2.56	-1.05	-Sa6	4.341	4.403	-2.72	-2.75	-2.41	286				<del></del>	<del></del>	4
	-					3.5		-11.5		25.0	330	-18.0	6.09	1.84	22.0	21.5	76.5			,:			<b> </b>	┨
	1830	<u> </u>	ļ			4.02	-4.01			-240	-7,13	-5.12	1.346	+.113	-2.74	-7.39	-2.52	6.17						╁
	<u> </u>			ļ		0		-11.5		+24 o	32.0	-19.0	6.18	2.02	21.5	21.0	25.5						<del> </del>	╁
	1980	-2.27	-2.27	-2.28	2.30	4.14	-4.62			-262	-2.16	-5.15	+.553	+.117	-2.74	-2.61	-7.54	4.29			,		<del> </del> -	+
· .	<del>- </del>	\$M5	24.5	29.5	21.0	- 2.0		-11.5	4	+ 44.0	31.0	- 19.5	6.30	2.09	21.5	20.5	25.0			· -			<del> </del>	+
	1927							-4.73		-2.65	-2.32	-5.19	+.340	+.09	-2.76	-2.63	-7.67		-		<del> </del>		<del></del>	+
	19.2951						-1.0			.Z3.0	285	<u>-20.0</u>	6.07	2.13	2.5	200	22.0							+
	14.691		* * * * * * * * * * * * * * * * * * * *		-		-4.14		-\-	-2.74	-2.50	-5.19	1.339	+.110 }	2.77	-2.86	-2744			:				†
···	19:38:3/			-			-2.0			21.5	26.0	<u>-20.9</u>	ا کو. ی	1,96	21.0	20.0	215						<u> </u>	†
	11.70.71						-4.18			<u>-2.88</u>	-2.67	-5.21	+.340	4.0991	- 2 21	-2 42	-2 42							†
	-					-255	-2.0	-13.0		19.5	23.0	-20.5	4.07	111	20.5	18.5	20.5			_				†
						<del>-</del>										I						`		†
	er approp							1	!							I					,			†

for each test parameter to be monitored.

Bendix Aerospace Systems Division LAGEOS THEOMH-OFFICAL TEST

10. 7772374455

The   Te   Black   Free   Annual Text   Mark   Free   Annual Text   Mark   Free   Annual Text   Mark   Free   Annual Text   Mark   Free   Annual Text   An	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
2/00	
2/00	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	<del>_</del>
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	+-+
23°1 29 29 29 29 29 -20.5 0 -10 20.5 24 -13 5.15 1.63 22 20 215  23:11:21	
23:11:21	+
-20.5 ,5 -10 +20.5 24 -13.5 5.12 1.74 22 70.7 71.5 -27:18:41 5.37 -4:01 -4:61 -7:85 -2:66 4:97 +302 .093 -2:74 -2:96 -2:80	
6ND 27:18:41 5.37 -4:07 -4:62 -2.95 -2.66 4:97 +302 .093 -2.74 -2.96 -2.80	
23.5 10 -11 120 72 145 1-20 1/2 12 12 12 12 12 12 12 12 12 12 12 12 12	
2321 -2.31 -2.30 -2.29 -2.29 -5.26 -4.06 -4.67 -2.82 -2.63 -4.85 +.207 +.092 -2.74 -2.84 -2.76 -3.15	
29 29 29 -214 -11 +20 23.5 -14 5.21 1.61 22 20 21	
· <del> </del>	
╏┃ ┃ <del>┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃ ┃</del>	

Enter appropriate data system termination symbol for each test parameter to be monitored.

Sendby Aerospeos Systems Division

LAGROS TNARADI-OPTICOL TEST

110. [REV.110. [8

	•									1														
	•	1				-	- X	->	TREE.	<u> </u>	TER DA	ta rec	<b>030</b> ◀	- y -	•	•	· 4;		£.					
		TA		RA	Lock	FACE	AAN	TAR	upra	ReT	FALE	ARIAL	RAD.	La Birth	UPBUG	ReT				-				
pate	Time 0-24Hz	10	<i>"</i>	12	/3	14		Ţ	•	19	•	"	, ,	•	•	4	•	,	•	•		•	•	•
1/1/	_	+	-2.72 28.5	-2.31	-2.3/	-5.59	-4.23	-4.17	-2.90	-2.69	-5.0Y	+.322	+.092	- 2.78	-2.92	-2.14								
<del>                                   </del>	<u> </u>									+22.5														-
	0030	29.5		30,0	30.0	-29.5	-4.5	-10.3	+19.5	123.5	-20.5	16.11	41.64	+21.5	+19.0	+20.5	-	· .	<del> </del>					<u> </u>
	0100	-2.24	- 2.23	- 2.22	-2.22	-5.92	-4.34	-5.04	2.86	-244	-5.29	+351	+.095	-2.75	-2.89	- 2.79								
	0,00	30								123.5							ļ							
	0130	30	30.5							-244 +23.5										ļ				<b></b>
	1		-2.23	-2.22	-2.23	-5.98	- 4.34	-5.//	-2.88	-2.65	-537	+.365	+. 100	-2.76	.2.9/	-2.80			<del> </del>					·
	0200	30	30	30.5	30	-345	-4.8	- 18.5	+19.5	+23.5	-23.5	16.52	+1.79	+21.5	+19.0	+20.5		-						
Test Start	0206	30	-2,25	-2,22	-2.22	-5.97	-4.38	-5.10	-2.87	-2.64	-5.37	+,357	+,095	-2.75	- 2.91	-2.79								
#3 64		<del>                                     </del>		30.5		-34.5	-6.0	-18,5	17.5	+23.5	-23.5	+6.41	+ 1.70	121.5	+19	+21	ļ	<u> </u>	ļ	<del>                                     </del>			<u> </u>	<del> </del>
- )	0226	30	30.5	30.5	30.5	-34	-5.5	-5.07 -18.5	-19.5	-2.64 +23.5	-230	+1.41	+104	21.5	+19	-2,/8 +21	<u> </u>	<del></del>		<del> </del> -			· · ·	
								720	17.5				1100	41.5		7 -1						<del></del>		-
																		,						
									·			<u> </u>				ļ								
	+	-					<del></del>					<del>                                     </del>					<u> </u>		-	<del> </del>	·			<b></b>
			_									, , , , , , , , , , , , , , , , , , ,		-	-		<del></del>		<del>                                     </del>	-				<del> </del>
																								<u> </u>
ů.			-						<del>                                     </del>	ļ			<u>.</u>	· · · · · ·			<b> </b>							
88	1.								<del> </del>	<b> </b>					<u> </u>		<u> </u>		-	-	<del> </del>		ļ	

<sup>\*</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

REGROOM PACE IS POOR



LOGIOS THAMMA- APTICAL TEST

100. [2574465 | REV.MG. C

## THEY PARAMETER DATA RECORD

_															ويسمسمم										
	ate	Time [0-24Hr	4	7	8	9	10	lı .	lz	13		29	*	3;	Eumo Par-	•	•	•	•	*.	•	•	. •	*	•
,	8/14/74	0634	-4.31	-7.06		-6.55	- 7.0B	-207			9.86	८.१८	410	. 07											
	74		-41	-67		-49	+41		٠ ٩١		- 4.5	<b>-</b> .	-												
	ft	07		-6.46		-5.46 -29	ζ <b>00</b>	-1.99 + 13	.200 193	193	4. 4. 2.	7,03	. 4	, o <del>0</del>		<del></del> -									· · · · ·
			-15	-46							9 61	991		.08		<u> </u>									<del>'</del>
		0110	-4. 10 +11	-18			496				1.6	<del>0. ] Q</del>	· 4	.00	·		<u> </u>								
				-4.80							9.6	8. 1	.4	. 08						٠.			<del></del>		·
		080*		+8								-	-	•											
		0700		-3,74								2.1	7	.07	17-14										·
ļ			146	¥35	+ 54	+40	<b>1</b> 104	4104	+100	1104		_	_	-						-	_		7.5		
.				-3.84	1						9.8	e. 9	.4	.07			·								
					155	42		91	94	94	•	-	-	<b>-</b> .	ļ	ļ									
				nay			Los			ARIA		065			1 TOR	1									
	· · ·	०१८०			3			-207 71	91	7.07	Ø	0	0	<u> </u>	1700	<b>4</b>		ļ							
	:		+ 20	141	150	+44	-11	17	71	7/		-	<u> </u>	<del>                                     </del>	1				•						
						· · · · ·		: .								-		<u> </u>		<del>                                     </del>					
	•																								
	•																								
		· ·	,			·																			
. ]									<u>.                                    </u>					<b> </b>	<u> </u>		<u> </u>		<u> </u>						
										`			1	-	<del> </del>	<del> </del>	<del>                                     </del>	ļ	ļ		•			<u>.</u>	
.								<b> </b> -							<del>                                     </del>	┵	<del>                                     </del>						<u> </u>	<del> </del>	
ı				<u> </u>		L	[	L	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	1		<u> </u>	<u> </u>	<u> </u>

\* Enter appropriate data system termination symbol for each test parameter to be monitored.

LAGEOS THERMA-OFFICAL TEST 10. 12.374455 REV.NO.

Cw %

#### TEST PARAMETER DATA RECORD

						=		· · · · · ·										. ,							
	ate	Time [0-24Hr		7	8						ξ <b>6</b>	29	30	3 /	76	27		•			. •		•		
	063	0/1/2					٠٦.١٥				•	•	~ <b>.</b>	,	7		<del></del>								<u> </u>
		. 470	+21	121	(2)	111	.11	421	121	13.1															
	'										·	·										-		-	-
	Ola I.		-698	-3 65	-1247	- 3. 23	-2.31	-2.30	- 2.30	- 2.31	10.08	15.19		-	1.79	-1.79									
16	,, , , , , , , , , , , , , , , , , , ,	0940	-54,5	144F	-3.04	156	+54	128	128	+28	_	1.	1	1	38										
X	11																								
,-		,000					-229				9. 1	15.0		-		-1.81				-			·		
			-567	-301	-312	-246	+29	1 ዓ	१५	27		-	-	-	137	137			<u></u>						
			-13.28	12.62	.12.60	12.62	-1.19	2.16	7.76	2.77	4-9	14 60			16.7	LFZ		•	• .	-					<del> </del> -
	*	1050					124				<del></del>	*				37									
			-12.32	17.61	-12.59	-12.62	.2.24	-224	-227	-2.17	9.9	14.96				184									
-			- 299	-319	-317	-319	†3 <b>o</b>	130	130	+ 3 c	<b>-</b> .	+			34.	37		* * * * * * * * * * * * * * * * * * * *	· ,			,	,		
														-			· · · ·					,			
							·		<b></b> -		<del></del>				<del> </del>					*		<b></b>			
							-							<b> </b>	<u> </u>			· ·			<u> </u>		<del></del>		
															•						·				
			,																						
	- ·		- :		<u> </u>	<b> </b> -				<u> </u>				<b> </b>	ļ	<u> </u>		<b> </b>	ļ					-	<u> </u>
					<del>                                     </del>		<del> </del>			<b></b>	<u></u>	<del> </del>	<del>                                     </del>	<del>  -</del> -							ļ <u>.</u>	<del> </del>	<b> </b> -		<del> </del>
	' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '		-				<del> </del>			-		<del>                                     </del>	<del> </del>	-	-	<del>                                     </del>		<del> </del>					<del>                                     </del>	<del> </del> -	<del> </del>

 Enter appropriate data system termination symbol for each test parameter to be monitored.

÷					•	•	X		7767_1	ARAJE	TEAL DA	A RIC	DRD	Y		1					5	٠.		
		1/	A	The	Block	Fors	Pra	Tab	Volume	ed.	Esca	Rece	Tab	484	Voling	Ret.	•1	•	•	•	•	•	- 4	
ate	Time [0-24Hr	10	11	12	13	14	15	16	18	(9	20	21	23	23	24	دد								:
-1 /		-228	7.2.7	-2.27	.2.17	-4.99	-3.55	-375	. 7.40	- 2.56	4.10	LVE.1	+.095	-1.18	-270	271								
8/11/74	1030	<b>-30</b>	+3:0	+30	+3 0	-16	+ 8	+ 1	+ 23					425		23								
		-2.31	- 2.30	-2.29	-2.29	-5.45	-392	.4.43	.280	-1.63	-4.61	+.411	+.106	-7.67	-2.81	-278					ļ		·	
	1100		129		124	- 52				123				+53	_		11.33	7000	75 b			<b></b>		
	1130	-2.29	-7.78	- 2.2 }	.1.18	-5.69		4.11	-7.85	.266						-7.61	902	70	0 + 6	o'C.			<u> </u>	
		124		124		-24				+23				112	1	1 1					-		<u> </u>	<del> </del>
		<u>120</u>	-701	7		1	-3.76				T		1	-156	1	T		<u> </u>				<del> </del>	$\vdash \vdash$	$\vdash \vdash \vdash$
	Dat	+ 54	124	124	154	-30	+5		+35	+40				+41		138		<del> </del>	<del> </del>	-	<del>                                     </del>		ļ	
	1200					-5.69								+45		+43		ļ <u>.</u>						i
	<del> </del>	+57		157		-29			+41							-1.29	<del></del>		<del>                                     </del>	<u> </u>	<del></del>			
	1230		- 474 58		£	-5A9	ı	- 6	+43	+48				+47		+45	<b>-</b>			-				
	<del>- </del>	58	<del></del>	57	+	-5.38		<del></del>		-1.67	1		1.159	T		-1.27					<del>                                     </del>			1
	1300	<del>43/</del> 59	54	59		-23	+12		+44	149	+	<del></del>	2 74			46					1		<b> </b>	
<b> </b> -	+	196		<del></del>	<del> </del>	-5.24	<del> </del>	<del> </del>				+		- 979										
	1330	61	41	61	61	-21	+15		146	52	-5		1	+50		,48								
	1	<del></del>	- 214		269	-519		<del></del>		88	-4.27	+.516	+.16.3	- 940	-1.17	-101								
1	1400	60.5	<del>                                     </del>	7.1		T	+16	T		+52		T		1 + 50.5		148	<u> </u>		<u> </u>		1		<u> </u>	<u> </u>
				- 264	1212	-515	-307	-3.95	-1.17	- 88	1-4.16	. 506	1.16	495	-1.16	-1.09	<b></b>		<u> </u>		<del></del>	<del></del>	<del>  </del>	<del>                                     </del>
	1430	105	61	415	$u_{5}$	1-195	+16	1+1.5		152	-3	8.13	2.83	+ 50.5	1		<u> </u>		ļ	<del> </del>	—	<del>                                     </del>	—	<del> </del>
	1500	288	-,275	265	271	-5.13	-3.65	-3.13	-147	- 878	4.1		1		115		<del> </del>		<b> </b>	<del> </del>	<del> </del>	<del> </del>	+	<del>                                     </del>
	1300	4 4	101	161.2	161	1-11	1,16	<del></del>	+47				2.81		41	48	<b> </b>	1	<u> </u>	-	+	<del> </del>	<del> </del>	<del> </del>
8/1/2	1530		· -		273	5./2	-3 03	-39/					1.162	- 944	1.15	1.08		10-7	<del> </del>	<del>                                     </del>	<del> </del>	+	<del></del>	<del> </del>
" 7/4	.  ' -	61	61	11.5	1 6/.5	1-19	1-17	1 2	+ 47	152	-/_	18.53	1279	+51	+47	1.4(5)					<u> </u>	<u> </u>	1	

<sup>•</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

Bendity Aerospece Systems Division LAGEOS THEROSI-OPTICAL TEST

10. 772374455 REV.MO. (9

				ω.		t _		٠,	7257	PARAME	TER DA	TA ARC	DEN X	•	,	Ar	)				1			
						7.	A.	76 E	York	FARE	Ma	Tob	Upline	Ret.	FACE	Aprix	716	LeRong	4Pm	Ret.	<u> </u>			_
pate	Time [0-24Hr	6	7.	8	9	10	"	12	/3	14	15	16	18	17	20	2,	12	23	24	55-				
8//	1600	-/2.43	12.65	12.63	-12.66	-, 278	-, 266	-,258	-, 260	-5.10	-3.03	-3.89	-1.16	. 859	-107	4 195	+.163	936	-1.14	-1.08		-		I
רְדִייִי	4					61.5	+61.5	161.5	161.5	1	1							L	1					ļ
State	16:03:01	<u>-</u>		<b> </b> -		<u> </u>										1.784							<del>                                     </del>	+
					<u> </u>			<u> </u>			¥	1	Y .		r	+8.34						<b></b>	<del> </del>	╁
5/00	16:19:31	├─		<u> </u>	-		<b> </b>									+8.09						<del></del>	<del> </del>	+
			4	1					· · · · ·				,,,,,		۲	1 2127		, -,						t
	ł			$\overline{}$		-																		t
		-(2.4)	-17.56	12.63	12.67																			T
	1690		12.51	= .	-317"	14																		Ī
	ļ.	-12.76	11.36	****					<u> </u>					,·	ļ	ļ								I
	1700		12.37		-302		1,5	-	ļ. <u> </u>	ļ		ļ	<b> </b>	ļ	ļ	<u> </u>	<u> </u>		<u> </u>				—	$\downarrow$
,	1390	12.09							-	<u> </u>			<b> </b>	ļ.,	-	<b>.</b>				-		<del></del>	<b>├</b> —	╀
		10.71	12.2	=	-292	<u> </u>	10	<del> </del>	ļ	<del> </del>	-	-		<del> </del>	-	-		<u> </u>	<del>                                     </del>	<del> </del>		<del>                                     </del>	<del> </del>	+
	1120	10.71	11.57	17.38	-522	7	100			╁┷┷		<del>                                     </del>		<del>                                     </del>					-	-		<del> </del>	┼	╀
·	<u> </u>	-942	+		10.67		<b>,</b> ,			<del> </del>	<del>                                     </del>	1-	╀──	<del> </del>		<del> </del> -	<del> </del> -	-	<del>                                     </del>	<del>                                     </del>		<b></b>	<del> </del>	+
	1730		10.12=		- 21 3		42				<del>                                     </del>	<del> </del> -	<del> </del>	<u> </u>	<del>                                     </del>	†	11.77				<del> </del>	<del> </del>	┼	†
		1						·						·						1		-	<b>†</b>	†
	1740	<u> </u>	9.3 -		-125	5.4-7	61"			,														†
	1750	-255		-6.64										,		-								I
	1130	<u> </u>	8.29	<u> </u>		12-7	27°		ļ	<u> </u>			<u> </u>		-		_		<u> </u>					1
·	1800	-482		-2:12	812	4-			<del>                                     </del>	<del> </del>	<u> </u>	1	ļ <u>.</u>	ļ		<b>. </b>	1.		1			<del> </del>	<u></u>	$\downarrow$
	- 1	]	1.51	1	8. U	11.3	28	L	L	<u> Li</u>	1	ŀ	I	1.	1	1	1	1	1	1	1	1	1	1

<sup>•</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

LAGEOS THERON-OPTICOL TEST

10. 772324466 REV.MO. (9

وس ۱<sup>۱</sup>

## TEST PARAMETER DATA RECORD

	·	<del></del> .			<del>\</del>	•		•			٠.			1 -	-			-						
ite	Time  O-24Hr	,	fm1 *	•	364ТН. 9	10	11	1%	13	Ι¥	" وا	16	18	19	20	યા	دد	23	24	25	e Harr	*	•	
1/2/	1810	- 6.17	-8.41	-5.17	-7.37	259	-,243	-, 231	140	-4.23	-260	-175	-101	13 8	-347	+.373	+.150	829	170	915				
774			4.85		- 57"	61								+54							1.2-6	240'		
	1850	-5.59	-6.02		-6.65						ļ		<u> </u>		·	<del></del>								
			6.27		40"						ļ		<u></u>						•	·	5.5.6	190,		· ·
			-7.41						<u></u> -			ļ	ļ	<del> </del> -	<del> </del>		· · · · · · · · · · · · · · · · · · ·					9.5	<u> </u>	_
			-79		- 33						$\vdash$	<del> </del>	<del> </del>	<del> </del>	<del> </del>		-				15-6	16	<u> </u>	· ·
	,,,,,	_	-57	1				·			<b></b>	<del>                                     </del>	<del> </del>	<del> </del>							3.2-6	3.0	<del> </del>	<del> </del>
		-431	-4.20					<del></del>			<b>-</b>	-	<u> </u>	<del>                                     </del>	<del> </del>	- <del></del>					3. 4	74	<del> </del>	$\vdash$
			-31			De	FF R	mp C	55		t —		· · · · · ·	<del> </del>		_					4.5-6	<del></del>		-
	.a .	-3.98	-5.64	-4.16	-4.59				-					<u> </u>	· · ·						1×10-4			<u> </u>
			-19																					Г
	10.4	-3.70	-5.11	-4.10			ļ		<u> </u>			<u> </u>									30 JI			
	1910	+42	- 2	<i>+30</i>	+28						<u> </u>		<b></b>	ļ	<del></del>			· ·						
-	1920	-3.43	4.62	-404	-3.77					ļ	<b>!</b>	-	<del> </del>	ļ ·							3/M_		ļ	L
		+>' -≥ 10	1.20	-396	-247	771				7.70		1.0%	. 0.0	729	.2	. 25	1/2	404	7#1	-		<u> </u>	<del> </del>	├
	1930	+5.7	+27	+34	+51	47	46	61	12.	7.8	47	36	53	54	34	7.540	7.743	56	r. /01	53	344	├	<del> </del>	├
	1940	-2.99	-3.83	-3.88	-3.14	-			4		7	-	<del>-</del> -	†		<u> </u>			37	37		-	<del> </del>	+
	1940	64	39	37	59																		<del>                                     </del>	<u> </u>
	1950	-2.81	-3.51	-3.79	-2-87					-1.93					-1.62									
		<i>&amp;</i> ,		75	6/					35					40					S	ARTE	D 7	ACKF	VZ.
	2000	-2.14	-3.26				<u> </u>		<u> </u>	1.15	<u> </u>	· .		<u> </u>	-1.14	<u> </u>	ļ	ļ						
	-	//	56	42	73	ا ــــــــــــــــــــــــــــــــــــ	<u> </u>			48				<u>                                     </u>	4/8		<u> </u>	<u> </u>			<u>l</u>			

Enter appropriate data system termination symbol for each test parameter to be monitored.

			· · · · · · · · · · · · · · · · · · ·	°C	W. C.	CORP.	(1) (4) (4)		e e			•		3	Adri Bysi	bepec terne (	o Divisio	× 7		NGAT AL-O BST	os Pico	4 2 P	0. 22324	+55    	eev.
			7/4		1/c	,	Pace	Mer.	7#8	TEST up Auc		TER DAY			La Rim	White	<b>→</b>		Windows Name	o f		<b>  ←</b> (o	i pwpil	<del></del>	. · ·
) -	nto	Time [0-24Hr	10	"	12	/3	14	15	16	18	19	20	21	22	23	24	25	•	Z	71:77	-> *	west*	ens*	8R	3
2/0	28/12/2	2150	-2.86	2.25 Zu	-2.25 Zo	-2.85 20	- 2.79 Z/	- 7.43 20	-2.80 2/	-2.82	-2.83 20	2.78	.003	7.021 7.30	2.72	2.22	-2. <b>87</b> Zo		-2.79 70	-2.69	-2.76			N/A	- 7.
<u>-</u>		2214	-2.85	-2.85	-216	-2.87	-2.45	-2.85	-2.75	-2.74	-2.16	-285	7.001	00S	-2.25	2.26	-2.36		70	73	72	73	. 72		7
-			20	20	20	19.5	20	20	2-0	20	20	26	0	10	20	20	20								
0	28/./	4472	-2.66	- 2.66	- 2.67	-2.67	- 2.90	- 2.81	-2.85	-2.72	-2.69	-2.86	+,026	f.003	-2.70	2.72	-2.71		-242	- 2.78	-2.79	-2.96	-2.92	-2.95	-2
_	/'ሃላ	0020	23	2.3	73	23	19	20.5	20	22	22.5	19.5	+0.4	+0.05	22.5	22	22		69	70	70	66	66	65	٤
•		0053	-2 66 23	23	23	2.3	-2.87 19.5	-2.79	-2.12 20.5	-2.70 27.5	-2.68°	-2. <b>3</b> 3	+.024	<u>4.603</u> 4.05€	-Z.cv	-2.70 22.5	-2.70 22.5	-			<u> </u>				$\vdash$
			-						-												-			**	
1	10/20	0200	-5.12		512	-5.62	-7.65		_	-5.45	-5.52		+:0/0	1.933	-5.43	-5.42	-5.64		- 2.67	-2.33		-12.32	-12.57	११५४	-13
<b>*</b>  -	7"		-5.68	-28	-28	-28	-67	-/9	-18	-25	-26	-16	10.2	7.6	24.5	-54.7	- 28		73	69	69	-295	-315	-314	-
		0230	-29	-19	-28.5	-28.5	-16	-30:5	-32	-29.5	-29.5	-31.5	+2.0	+0.78	-28.5	-29	-5,78 -30,5		-2,69 73	65	1.6	-13.36 -301		-12.55 -314	1
			-5.79	-5.79	-5.77	-5.78	-8.50	-6.1P	-6.37	-5.93	-5.90	-6.37	1	+.043	-5.87	-5.41	-5.95		-2.66		-2.94		15 <sup>-</sup>		Ť
L			-3/		-30.5	-3/	ن مين	-38			- 37	-42	+3.0	+0.79	- 32	-37	- 34		74	65	65				
		0330	-5.81	-5.81	-5.79	-5.80	-8.68	-6.41	-6.63	-2.03	-5.98	-6.76	t,211	1.050	-5.91	-6.02	-6.01				-2.95				
-			C 20	-31.5	-31	-31	*3	-42.5	-47	-35,5	- 34	-49	14.0	+0.9	-33	-35	-35				65		<b> </b>	<u> </u>	lacksquare
		do	-3./I -3/	-3/	-3.78	-3.4	90.5	-6.5Y -48	-50	-6.08	3.0	र्	r, 248	4.053	-5.74	-6.08 2/ Y	-6.04				-239		<b></b>	<b></b>	╀
+				-5.75	-5.73	-5.7V	18.K	-4.60	-4.14	4.07	- 5.55	212	1.279	344	-(41	-26-7	-55.5	<u> </u>		2 98	-2.87	<del> </del>	<del> </del> -	<b></b>	╀
1		0430	-30	-30	-31	-30	42	-46	. < -	- 2/	2/5	(7	16.67	1.030	22	77.5	25		73		67		<del> </del>		┼

<sup>•</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

Sendty Aerospace Systems Division LAGEOS THERAN-OPTICAL TAST 772374456 REV.HO. 6

TEST PAGE 18 DP

		•		=								1		•		-				of.			··-	•	<del></del>
			1 7/	Ā	1 77	£ 1	Eng	APER	X —	7857_ ********	PARAJE G-+	ER DA	ra REC	0 <b>12-</b> )	/			1 12	اليون الدوا	<u>-</u> 	Arlette	l		1 <b>6</b>	
	ate	Time  0-24Er	•	•	•	•		15	•	•	•	20	•	•	•	•	•		2	a	5-,	6	7	8	9
<b>)</b>	°8/13/74	0500	-5.76	-5.76	-5.75	-375	1.7 >	-644	-6.54	-6.09	-6.0/	-7.27	+.29/	+ .057	-5.95	-6.11	-6.03		· · · · · · · · · · · · · · · · · · ·	-2.76	-2.75	-		0	
}	774		- 30.3	-305		-30	-92.	- 47 -6.46	- 52.5	- 37	- 35	-59	+5.1	+1.1	-34	-37	-35.5		77	7/	7/				
		o530	-30	-31	- 30	-30	-93	-47	-53	-36×	-35	-60.4	16.0	+1.2	-34	37	- 355		72	72	-2.69 73				<u> </u>
		06.00	-5.7/	-5.8	-5.73	-5.24	890	-6.67	-6.49	-6.10	-6.01	-7.38	t.310	+.059	-5.96	-6.13	-6.04		-2.70	-267	- 2.67				
ŀ			-5.75	- × 76	-5.74	-574	-491	-47 -L.L4	-100	-6.10	4.01	-742	F.Stu		-591	1.14	·InC		72.70	73 - <b>26</b> 6	73				<u></u>
ł		0630	-30	-30	-36	- 3c	-73	-47	-514	-365	-35	-624	+6.3	11.2	-34	- 37.5	-34		72	74	74				
		0704	-30	-3 <i>116</i> -3 <b>9</b>	-30	-5,/5 -30	-8.92 - 93	-6.68 -47	-7.01 -54	-345	-6.02 -35	-625	+6,3	+,057	- <u>5.27</u> -34	-6./5 -38	-6,05 -36		1	-2.65 74	-2.69 74				
1	-		-5.74	-5.75	-5.73	-5.74	-8.72	10.46	-698	-4.09	-4.00	-241	1. 209	4.054	-594	112	V 04		-2.7/	-2,45	2.64	-12,44	-12.44	-13.62	-12.6
╁	. <u>-</u> .	0723	-50	-50	- 50	-30	-70	-47	-55	-37	-35	-62	+6,2	+1.1	-34	-37.5	-35.5		72	74	74.	-367	-320	-319	-32
				074	12	A DIL	3 F 7	CARRY	7	- 30	c														
١	•	, .		* +: :	<u> </u>	ļ			-		ļ														
ľ	• .															<u> </u>									
╀																									
	<u> </u>																	`				-			
																-			-		-				-
L																<del>                                     </del>		<del></del> -	<u> </u>		<del> </del>	<del>-</del>	<del>                                     </del>	-	_

Enter appropriate data system termination symbol for each test parameter to be monitored.

Sendity Aerospace Systems Division

LAGROS THEROOL-OPTICAL TEST 

# TEST PARAMETER DATA RECORD

ate	Time (0-24Hr	2	4	5	ر ان	7 -4-	₽ ¥	¢ +3	10	1:	12	13		•		•		•		•	•	•	•	•
8-13-74			-2.55	-7.54	-(2.44	-12.63	-11.61	-12.63			4.15	-4.15												
-	<del></del>	+22				12.57	- 1	130			2 // 0										·			<u> </u>
		+22	-213	٠ <u>۲.۲۶</u> عن		ļ —				125		-24B		<u> </u>		<u> </u>								<b></b>
		_	.2.41							.244				•	<u> </u>			·	<del>-</del>					
	0900		127							111	-				<del></del>							· · · · ·		
	<b>67</b> (0		-2.43						-244	- 1.44	-242	-242			7.5									
· <del></del>			+ 17							127													·	
,	10014		-1, 44.		<b> </b>		<u> </u>	ļ	-2.34						ļ									
			15.7		<b> </b>	-		-		128					ļ <u>~</u>							<del></del>		
			1,44 +27 °							129			-	-		-			-	,	-		<del>  </del>	$\vdash$
		4.72				<b> </b>			464	164	1157	1 4 4 7	<u>-</u>							<del>                                     </del>				
~ <del>-</del>								<u> </u>		<del>,</del>	<del></del>	ļ		<u> </u>										
																-					•			
•																								
						<b></b>		<b>!</b>				ļ		<u> </u>										
		· :										<del> </del>					<del></del>	<u> </u>	<b> </b>	· .	ļ			<del> </del>
					ļ·			-11	-		<del></del>		<del> </del>	<del> </del>	-			,	<u> </u>				<del>                                     </del>	<u> </u>
<u> </u>					<u> </u>						<b></b> -	-	<del> </del> -		<del></del>	<del></del>	ļ						<del>                                     </del>	<del> </del>
								<b> </b>	<del></del>						1		<del>                                     </del>			<del>                                     </del>	<del>                                     </del>	<del> </del>	<u> </u>	-
													Ì	1		<u> </u>				1	1			
_	1 . 1																							<b> </b>

REPROPUCIBILITY OF WHILE



LAGROS THERMAL-OPTICAL TEST 10.
772374466 PEV.HO. G

#### test parameter data record

ate	Time [0-24Hr	10	11	12	13	14	15	16	10	19	20	21	22	23	24	25	-							
8-13-74	•740	-2.] L	.233	-2.29	. 230	- 7.94	4.82	-£73	.306	.7.17	6.15	+.601	+.(3)	-799	-311	-296						•		
		+29	+24	157	129	-73.	-13.5	-30	+ 11.	+ 11	-38	์แน <b>ง</b>	2.43	+17.5	+16	+18								<u> </u>
	1000	- 2.32	-2.33	-1.29	-230	-188	.4.75	-562	-304	-1.17	6.00	1.170	+.130	-297	·308	2.95								
	1000	424	+21	129	+24	-12	-12	-58	+ 1 G	121	-35	110,56	† 1.40	418	+16	+18		-	•					
	1030	-1.32	-2.33	-1.29	- 3.30	-181	-4.68	-5.51	-302	-7.76	-5.84	+.541	1.128	-2.94	-305	-2.93		-						
		+24	129		125	-7 o	- 11		+ 17		-32			1		+18.5								<u> </u>
	llou	-7.31	₹. ₹ ₹	-2.29	-227		-4.63								-3.03	2.92								L_
		+29		<del></del>	129			-24.5						7	<del></del>	+19		<u> </u>						
	1130	-5.24	₹.31				- 4.60	-1.38	-7.49						3.02	-291			<u> </u>					
		124	129	<del></del>	124			- 24			-29	<del></del>		<del></del>	+17	+19								<u> </u>
	1200						-4.5B								7	7	<u>.                                    </u>							ļ
				+29		-68		-23					7	Ţ						<u> </u>		<del></del>	<u> </u>	<u> </u>
	1125A 3		-2.32						·					T .	1	-2.91				<b></b>				ـــ
• •		+29	129	+29	+29				+18	******				1	+17				ļ					<u>                                     </u>
	1300			ļ	ļ	1		T	T		,			1	7	-2.92				ļ	<u> </u>			<u> </u>
	ارها	,		<u> </u>	<u> </u>	-68	-9	1——		+21.5				1	1	<i>+19</i>	ļ	- i		<b>!</b>			<b></b>	<u> </u>
•	13:19:41			<b> </b>		<b>—</b> —	-9.52	<u> </u>	-		1	•		1	1									₩
	7-9/				<del>                                     </del>	-63-	-8			122		1	1	1				<b> </b>		<del> </del>	ļ	<u> </u>	<b></b>	—
	1330				· Z.30		-4.53								-3.0/			ļ		<del> </del>	ļ	ļ	ļ.,	<u> </u>
		+29	+29.	+29	+29	-69	-8.5	-22	+18	+21.5	-26	18.19	72.29	+19	+17	+19	· · · ·	<u> </u>	<del> </del> -	<b> </b>	<del>                                     </del>		<del> </del>	₩
		<del></del> ;		<u> </u>			<del>                                     </del>			-		ļ	<u> </u>	ļ	<del> </del>	,			<del>                                     </del>	<del> </del>	<u> </u>		<del> </del>	╄
	ļ						1	ļ	<del> </del>	<b> </b>	<del>                                     </del>		<del> </del>	-	1	<del> </del>			1	<del>                                     </del>	1		-	+
	1	l . '	! -		i		l	1		l	l	1	<u> </u>	1	l	j	l	1	i	-[	<u> </u>		1	

Enter appropriate data system termination symbol for each test perameter to be monitored.

LAGEOS THEROM-OPTICAL TEST PAGE 21 OF PA

## TEST PARAMETER DATA RECORD

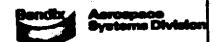
	Time [0-24Rr	6	1	8	9	lo.	te	12	13	i v	15	16	12	17	10	21	22	2.3	24	25	•	•		
8/13/74	1330	-12.44	-12.60	-12.60	-12.56	- 2.32	-2.71	.2.29	.2.30															
"714			-17.5	=	- 314	F	128	२५	29								·							<u> </u>
	1400	-12.17	-12.18							-					·	·								
<del></del>	<u> </u>		-12.23				425	129	129								<b></b>							
	1430	-9.59	-11.02															ļ						
					- 182			·									<b> </b>							
	1500	-184	-9.78															<u> </u>						
			-8.1		105	92									ļ									
	1534	-6.62	8.41														<u> </u>						<u> </u>	
			- 6.90		-61°	w																		
	,,,,,,		-6.76	-4.12	-5.93					· .			<del>,</del>						<u> </u>		•			<del> </del>
		+10			-28										<u> </u>		ļ.,,	ļ ——		1				ـــــ
	630		-8,02			-			4		245				-				ļ					<u> </u>
	: '	+46	+ 1	137	1550					-41B	-366					1.199	1.0(3					-		—
										. می ا	+ 7	0	23	26	-1			24	23	25				ـــــ
		2 61	-3.72	-1/4	2 (						- 35	3.50											<b> </b>	↓
	,,,,,,		-3. E.							1 # 8	-2(1	-118	-633	-240	1566	1140	1.036		-		<b></b> -	ļ	<u></u>	┿
	1500	-7 22	-3.54	3.22	334				ÿ.26			<b>‡ 8</b> .			1				125		-	<u> </u>		┿
[		TEU	+47	+ 2.J	150				85.5		46.5		;	, ·		1.08.7	1.025	2.4	2.46	2.42				<del> </del>
			3.365	1		2.14	2.24	2.14	2.25	3.08						96			9 11 1	4.1	<del>                                     </del>	<del> </del>	<del> </del>	┼
	1900					86	84	26	85.5	5.55	71	2.87		2.35	Γ	7.077	+.022	3.35	2.47	2,88	-	<del> </del> -	<del> </del>	+
							- 50	7.15	67.	91	<del>- ( '</del>	2/3	<u> </u>	24.,	**	<del> </del>		<del> </del>		<del> </del>		_	-	+
!							<del></del>							<del>                                     </del>	<del> </del>	<del>                                     </del>	<del>                                     </del>	ļ			<del>                                     </del>	<del> </del>	├	+

\* Enter appropriate data system termination symbol for each test parameter to be monitored.

•	•				ď				,				Ben	94	Aero	tems !	e Xivlak	,	VERN	n-ap	nede.	1	72324		<del></del>	···
,				9	5 5			. P		ÿ	A Pex	ď							72	ST			<u> 2</u>	<u> </u>		
			MINDOW.	MANIBUR	MANIMU	PAMEL	PRUIEL	TC F WR	TC FUTUB	L X TEST	× ×	* × ×	M MBC	X RET	YPLCE	<b>STAKIA</b> L	ATRADA	2 0 mg	K. PPER. R. Lide	Y Res						
E5T # 21	ate	Time [0-24Hr	2	4	Ŋ	- 0	11	12	13	14	15	ما ا	18	19	20	21	22	23	2-4	25		•	•	•		
421	data	a. a.	-2.86	-326	-3.25	-5.60	-5.62	-5.58	-5.58	-4.27		<u>- 4.2i</u>	-5,12	<u>-5,28</u>	-4.16	090	+.033		-5.12	-5.40						
,	8/14/14	2100	+20	+13	+13	-28	-28	-27	-27	ـ4	-7	-3	-19		- 2		•	-19	-19	- <b>24</b>						4~
Ą		2130	-2.66	_292		-5.70	-5.71		-5.69	-5.52	-5.4)	-5.39	-5.10			+.037	4.634		<u>-S.\$7</u>	-5.72						ز ]
	:		123	+19	+19	-29	-30	-29	-29	-26	-24	-24	-28	-28	22			-27	-27	-30			:		<u> </u>	1
		2200	-2163		1	-2.72	-5.74		-5,72	-6.21	-595		-5.82	ĺ		4.136	+ 043		-5,78					<b> </b>	( )	
			+24	+21	121	-30	-30	-30	-30	-39	-34	-36	-32	- 32	-36	1 - 4-		-30	-31	-32				<b> </b>	<u> </u>	
	,	2230	-2.62	-275	<del></del>	<u>-5.73</u>	-515	-S72	<u>-5.73</u>	-661	-6.26	6.44	-594	-590		1.242	1.051	_C.82		-591			·	<b> </b>	···	ł
	<u> </u>	-	124	122	+22	-30	-30	-30	-30	-46	-40	43	-34	-33	-45			-32	-33	-33		-	·	<b>├</b> -		ł
	•	2300	-2.43	-2.75		-5.76	-5.77	-5.74	-5.75	- 6.87	- 6.94	-6.68	-6.02	-5.95	-	₹30 <b>3</b> 0	4.056	-5.67	-6.50	-5.58			· · · · ·	<del>                                     </del>		ł
*	<b> </b>	-	+ 24	+22	122	-30	-30	-30	-30	-51	-43	- 48	-35	-34	-5/		(2)	-33	-35	-35				<del>                                     </del>		1
1	1	2336	_	-2.76	2.76	-5.76	5.78	5.74	- 5.77	-54	-45	-6.83	-6.07 -36		-7.10 -56	+.362	7.037	-34	-6.06 -36	-6.0Z -35	-	·, · · · ·	•	<del> </del>	<del> </del>	ł
	67	<del> </del>	124	122	+22	-30 -5.78	-31 -5.79	-30	-30 -5.17	-7.a	-6.61	-6.40	-6.07	-35	-7.23	4 281	+.0\$7	- 5.17	-6.01	-32			-	<del>                                     </del>	├	1
•	8/15/14	000/	-2.64	2.77	+22	<del>                                     </del>	-31	- 30	-3/	-55	-46	-52	-37	-35	-58	7.501	1.037	-34	-37	-36			· ·	<del>                                     </del>	├──	┨
		<u> </u>	+23	+21	27	-31 -5.77		-5.76	-5.77	-7.14	- 6.65	-6.96	-6.11	-6.02		1.Vob	1.057	-5.59	-L 13	6.06		•		<del> </del>	<del>                                     </del>	1
	ŀ	0030	<b>—</b> —	12/	+ 2/	-30.5	-305	- 30	-30-5	-56.5	-47	-53	-37	-35	-60	7.700	7.03 /	-34.5	-37	-36	-		<del> </del>	<del> </del>	<del>                                     </del>	1
	ļ		+23	-2.80	2.79	-30.3	-5.80		1	-7.17	1.12	-4.98	-6.12	-6.03		t.40Z	400	-6.00	/ 14	- 1 47			<del> </del>	┼	<del>                                     </del>	┨
	'	0100	+23	+21	+21	-31.0	-31.0	-5.1 <u>5</u>	-30.5		-47	-53.5		-35	-61.5		1.097	- 35	-275	-36				<del>†                                    </del>	┼	1
		<del> </del>	-2.66	-2.81	-2.80	-5.78	1	-5.75		7.19	-6.67	7.00	-6.13	-6.04		1.428	+.059	-601	-6.18	-608			<del>                                     </del>	┼──	+	┨
		0130	23	21	21	-31	-31	-30	-30	-57.5	-48	.53.5	-37.5	-35.5	-62.0	<del></del>	+1.0	-35	-37.5	-31.5			_	<del> </del>	<del>                                     </del>	1
		<del>                                     </del>	-2.67	<del></del>	<b></b>	3,77	-5.79	<del></del>	-5.77	+	-6.69	+	-6.13	-6.03	<del>                                     </del>	+ 429	1.061	_6.01		-6.07				+	<del>                                     </del>	1
Ŋ	Start	0137	23	21	21	-30.5	-3/	-30	-30	-57.5	-yr	-53.5		-35	-62.5		+1.0	35	-37.5	-36				1	<del>                                      </del>	1
्र -99	and	-						-5.75	4-5		<del> </del>			-6.03		+.420		-6.01	-6.14	_			<del>                                     </del>		1	7

<sup>•</sup> Enter appropriate data system termination symbol for each test parameter to be monitored.

ORIGINAL PAGE IS POOPER



LAGGOS THARANI-CONCAL TEST

III. 171574455	REV.#0.	<u>()</u>
73	· •	PAG

00

## TRET PARAMETER DATA RECORD

		Time	m nd	MAN.	MAN	PAVAL	PANGL	TC FIXT.	TE FIXT.	FALE	AAEX	7 708	UP RING	RETUG	FACE	AJ-A×	AT-PAD	LOW RING	ZIN4	ROT.		•	•	•	
	ate	(0-24Rx	2	4	5	10	11	12	13	1 .			18	19	20	2/	22	23	24	25					L
			-2.66	-216	-2.46	-2.32	-234	-2,30	-2,35	-6.53	- 5.15	-6,21	-3.18	-2.85	-6.81	7/24	1./3/	-3./6	-3,27	-3.06					L
t Y	2-/2-79	0300								-45					-50										
Ţ	]		-2.65	-2,51	-2.58	-2,28	-2.29	-8.13	-2,26		-4.90	-581	-3.06	-2.76	-639	4.15	+./33	-3.03	-3/2	-2,97					L
		0330								-39	ļ	ļ	ļ		-42	<u> </u>							<u> </u>		
			-2.45	-2.60	-2.60	-2,25	-2.26	-1,22	-2,24	-6.01	-4.75	-5.67	-101	-2.71	-6.02	41.07	4./38	-2.28	-306	-2,92					
		0400	23	24	24	30	29.5	305	30	-35	-12.5	- 21	16	22	-34.5	+/9.8	+2.6	#7.5	14.5	19					
			-2.64	-2.59	-7.59	-2,25	-2,27	-2,21	-2,23	-5.86	-4.65	**************************************	- 5.17	***	-3:3	7.01	7./35	-2.90	-3.03	-2 (r)					Γ
		0430	+23.5	+24	+24	30	29.5	30	30	-32	-10.5	44	#	22	-2-3	44	+2.5	are	47	19					Γ
			-2,64	-2.58	.2.58	-2.26	-2.27	-2.2/	-2,24	-5.76	-4.51	-5.43	-2.96	-2.70	-5.75	r.976	1,129	-2.9/	-3.4	-2.89					Γ
		0500				27,5				L.			18				+2.4		17	19					Γ
			-2.4	-2.57	-2.57	-2.24	- 2.26	-2.21	-2.24	-5.76	-4.55	5.37	-2.94	-2.69	-5.65	1.953	+.135	-2.50	-2.99	ージ・よつ					Γ
		0530	123.5	24	24	30	29.5	30	30	- 29.5	-9.0	-23	+ /2	122	-285	+1.7. 3	+2.5	+19	+17	+19.5					T
			-2.64	-2.57	-2.57	-2.27	-2,23	-1.22	-6.25	-5.44	-4.54	-5.84	-2.29	-2.69	-5.40	1.956	1.133	-2.89	-2.98	-4.88					Τ
		0600	23.5	24	24		29.5							1		r	+2.4	1	17	19					T
			-2.64	-2,57	-257								-2.74	-			,		-2.77	-2.27			<del> </del>		T
_		0630	23.5	24	24			34.5		-28		- 22					+ 2.5			+19.5			· ·	<u> </u>	1
1			-2.64	-2.57	.2.56	-2.25	-22	-222	-2.12	-5.69	-4.53	-5'31	-2.44	-2.69	-5.57	+ 926	+./34	-2.89							t
	•	0635	23.5	24	245		129.5							२२		+168		19	118	19.5					T
		0656	-245	-2.55	-2.55	-225	-227	-2.22	-2.22	-5.58	-418	-527	-2.93			1.901		-297	-2.99						t
•		001-	235	25	25		129.5			-27		- 215		23			+2.2					-	1		T
					т.													-							t
														•							1	1			十
i																					•	1			†
							1			1		T	T			1	1	† <del></del>	1	<del>                                     </del>	1	<u> </u>	<del>                                     </del>	<del>                                       </del>	╈

Enter appropriate data system termination symbol for each test parameter to be monitored.

Pendix Aerospace Systems Division LAGROS TAGRANI- OFFICEL TAST 100. 172574455 | REV.10. (

°C

THET PARAMETER DATA RECORD

AT AT

																	4/								
Γ		Time	WIND.	MAU:	MAL	PO NO.	PARH	TC F/17.	TE FIYT	X AKE	X. APEX	X *	NA PARE	RING	PACE !	γ • ΔΤ-ΑΥ	AT-API	XXXX	XNG.	E N			•	•	T
þat	L.	0-24Hz	ス	4	5	10	11	12	13	14	15	16	18	19	20		22	23		25			<u> </u>		
			- 2,63	-2.40	-140	+.524	1.495	+.4/8	+,388	-5.43	-3.51	-5.02	-1.27	124	<i>- 5</i> .52	+ 1.54	+.172	242	- 1.22	- 1.06	,				l
8-1	5-74	0730	24	27	27	74	73	72	7/15	-25	9	-17	46	53	-23	+27.5	5 6	5z.	46	49			<u> </u>	,	
			-2.63	-2.01	-2.01	1,156	t/1.53	1/1.59	tN55	-4.62	-2.57	-4.10	1.088	<i>†.31</i>	-4.44	11.69	t.278	+.427	1.111	t. 2/3					
	- [	0800	24	34	34	89	89	90	89	-11	25	-/	79	73	-7)	1291		72	67	69					Ι
			-2.62			11.59	+1.57	11.64	11.61	- 3.60	-1.81	-3.00	1.387	+.69Z	- X 20	11.34	1.330	+.702		,					T
		0900	24	40	10	90	90	9/	90	+9	37	126	7Z	26	+14	+22,3	+5.50	77	22	72					T
			-263	-1.56	-1.56	+1.57	+1.56	+1.67	11.64	-3,20	1		1.47.3					+,773	ه ويحدد	1.44G					T
		0930	2.4	41	#1	+50.5		+ 91									15.43								T
			-26 Z	-1.51	-1.51			1				1					1.378								1
1	ŀ	1000	24	4.2	47.	91	21	92	21.5	12.5	425	2.8	24	22	20.5	120.8	t5.3	28	74	23		chri	7	ens	Į
Γ		:	-2.61	-161	-1.62	547	- 386	-, 257	:3/1	-314	-2.12	-270	- 109	- 767	-201	1.770	1.2/2	2/4	- 9/7	1.02	/	· · · · · · · · · · · · · · · · · · ·		from t	_
1		1030	24	40.5	40.5	60.5	59.5	61	61	15	32	23	51.5	53,5			+3.53		51	49.5	•				T
		_	-2.61	1.79	-1.79	423	:465	- 384	- 9/2	-466	-2.57	-3.27	-1.19	-1.01	-3.51	+.846	1.164	-1.04	-617	-625					T
1		1100	24	37	37	59	58.5	59.5	59	6.5	24	/3	47	49.6	9	1/4.3	+2.78	49	47	46	ļ				T
		1/30	-7.60	-1.86	-1.86	430	- 470	385	-+11	-3.99	-2.83	-3.57	-1.26	-1.05	-3,52	1.918	1.165	-110	-1.23	-1.28					Τ
	·l	7100	24	36.5	36.5	59	58.5	59.5	59	+0.5	20	7.5	45.5	99	3.5	+15.6	+2.80	48	96	45.5					T
		1200	-2.60	-1.92	-1.43	- 116	- 470	- 375	.417	-9.19	-2.98	-3.79	-1.31	-1.08	-401	+.961	1.167	1.14	-1.27	7.31	_				T
L		1200	24	35.5	35.5	59	58.5	59.5	59	- 2.5	17.5	4	45	48.5	70.5	116.3	+283	47.5	45.5	45					T
Г		1230	-2.58	-2.15	-2.15	398	:438	-,34/	. 388	-4.29	-3.04	-2.87	-1.31	-1.07	-4.10	+.99/	+.169	-113	-127	7.30			1		I
L		1230	24	31.5	315	59.6	58.5	60	60	- 4	16.5	2.5	45	48.5	-/.	112.1	+2.91	47.5	45.5	45					T
Г		1300	-2,68	-Z, Z3	- Z.23	42/	469	375	:401	-4.36	-3.09	- 3.96	-1.33	-1.08	-4.16	+1.00	+.170	-1.16	-1.29	-1.32					T
		1500	24	30	30	57	58.5	60	59.	- 5.5	16	1.0	45	48.5	-z	117.2-1	t2.93	47	45.5	15					J
Γ		1420	-2,58	- 7.77	- 2.29	- 127	- 466	-371	407	-1.10	-3.12	-4.00	-1.34	-1.09	-4.Ze	11.01	1.170	-1.16	1.30	-/.32			٠.		7
		1330	1	29	29	59	58.5	60	59	-6	15.5	0	-14.5	48	-3	17.5	+2.93	47	45	45	1	1		T	7

Enter appropriate data system termination symbol for each test parameter to be monitored.

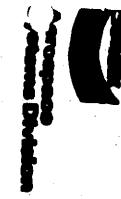


TEST

	•	1		+	91. L	l	X		7207	PARAME	770. PA	ta rec	ORD	· y		ام			1	· .				
	į	1.1	•	160	LOCK	FACE	MAL	726	Ning.	Part.	Fees	ATA	ATAN	Lo Come.	Ene	Ref.							·	
ate	Time [0-24Hr	10	"	12	13	14.	15	16	18	19	20	21	22	25	24	25	•	•			•	•	•	
	1400	-,426	-166	- 577	- 405	- 1.43	-3,/3	-1,02	-1.54	-1.09	-4.22	+1.01	+.169	-1.16	-1.50	-/.32						,		T
5724	7700	59	58.5	60	59.5	-6.5	15.5	+0.5	44.5	48	-3_	+17.4	1291	42	45	45			·					
Traf	14:12.	-,419	456	- 379	406	-442	-3.11	<u>-403</u>	-1.34	-1.11	-4.23	+1.04	+.169	-1.1	-1.31	-1.32								
1251	.41	59	58.5	59.5	59.5	-6.5	15.5	0	44.5	480	-3.5	117.9	12.91	47	45	45								Г
17474	1/4.	<b>4</b> 2€	l 47a	ם בחר". ו	1- 415	L 4.39	2 . 2	レクカフ	L.I 3.4.	I1.1Ω	1 4 21	11 000	1 11 11	1.4 1.4 1.1 1.1 1.1 1.1	1 1 7			ļ	ļ					
	-	59	58.5	N.G.	59	-6.0	16.	.5	44.5	48.	-3.	H7.05	+2.76	47	48	45			<u> </u>					L
8-11-74	8:55:55 0#	-1.76	-1.76	-2.50	-1.76	-1.91	1.78	4.86	-1.83	H BZ	-191	+.066	+.044	-1.78	-1.82	-1.83			<u> </u>	· .			<u> </u>	L
	o£	100	100	13.	100	96	100	97	98	98	96	+1.1	1.73°	100	98	98				<u> </u>		ļ	<u> </u>	L
		<u> </u>	ļ	ļ		·			ļ	<b> </b>	<b>-</b>	ļ :		ļ	ļ	ļ		<u> </u>	ļ	<del> </del>			<u> </u>	L
	<del> </del>	<u> </u>	<del> </del>		<del> </del>				<del> </del>	<del> </del>	<del> </del>	├		<del> </del>	<del> </del>	<del> </del>			<del> </del>	<b>├</b>	<del>                                     </del>	ļ <u> </u>	<u> </u>	Ļ
1		<del> </del>	<del> </del> -	├──	<del> </del>	-			<del> </del>	<del> </del>	<del>                                     </del>			ļ	<del> </del>	<del> </del>	<del></del>	ļ	ļ	-		<b> </b>	<del>                                     </del>	╀
	1	<b> </b> -		-	<del>                                     </del>	<u> </u>	<del>                                     </del>	<del> </del>	<del> </del>	<del>                                     </del>	<del> </del>	├	<del> </del> -	<del>                                     </del>	<del> </del>	<del> </del>	<i>-</i>	<del> </del>		<del> </del>	├	<b> </b>	<del> </del>	╀
		}	ļ		<del> </del>				├──	-	<del>  '</del>	<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del> </del>		<del> </del>	<del>                                     </del>	<del> </del>			<b>├</b> ──	Ł
		<u> </u>		<del> </del>	-		<del></del>		1		<del> </del>	<del>                                     </del>		<del>                                     </del>	+	<del> </del>	-	├	<del> </del>	┾	<del> </del>		├	╀
		<u> </u>	-					<del> </del>	<del> </del>	<del> </del>	-	-		<del> </del>				<del> </del>	<del> </del>	-	<del> </del>		├─	╀
			-	-	<del>                                     </del>			-	<del> </del>	<del> </del>	<del> </del>	╁	<del>                                     </del>	<del> </del> -	<del> </del>	<del> </del>		· ·	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>		<del> </del>	╀
•	1				<u> </u>			<del> </del>		╁┈┈	<del>                                     </del>	<del>                                     </del>			<del>                                     </del>	<del> </del>			┼──	<del>                                     </del>		<u> </u>	┼	╀
	1				<u> </u>					<del>                                     </del>	<del>                                     </del>	<b>†</b>		<del> </del>	<del>                                     </del>	1		<del>                                     </del>	1	<del>                                     </del>	<del>                                     </del>	┝∸	_	+
	1						1			1	1	<u> </u>				<b> </b>			+	<u> </u>	1		<del>                                     </del>	t
								İ		·				•		·			1	<del>                                     </del>	1	<del> </del>	<del>                                     </del>	†
	· .	·													Ì			1	1		1		<del>                                     </del>	†
																				1				t
																1			T		Τ-		<b>†</b>	十

\* Enter appropriate data system termination symbol for each test parameter to be monitored.

	15.				
#	Reference Paragraph	Variation Description	BxA T.C.		Prog. Mgr.
/	10.1 Sht31	RADIONATERS to DAS 32 & DAS 34.  DAS 32 IS ISOLATION Channel.  TC =1 ASSNEWAS to FFDI Ambrest.	3M	ean	
2	7.17.3	Add "Repeat 7.10.1 & 7.10.2		Eas	JmB.
3	AFER	AN ADDENDUM I TEST NATIONS	91	EOB.	Jones
4	6.2.// 8.13 8.18 9.6	Add " PER STA 1036		Eak	
5	7.25	Delute this prescaph	SA	Eas	JmB
0	8.0 b.	Change Gendrast temperature change to 15% & example to read "+ 2.0°C exodient coes beyond 1.7 or 2.3°C"		Ear	v v .
7	8.0	Délate check-off blowles for Référence retrocaflactor photos	M	tak	Jms



11.0 VARIATION SHEET THERMAL-OPTICAL TEST

(6

TP2374455

M70 9 July 1974

•	Reference Paragraph	Variation Description	BxA T.C.	Therm Eng,	Prog. Mgr.	] =
8	8.4.2.1 8.7.13 8.12.2 8.15.2 8.17.2 9.3.1 9.5.2	Add step: "Obtain ANTFOI VERIFICATION photo USING the REFERENCE RETRORAFILITOR.  Number the photo of enter number in Test  Data Sheat."	THM.	eas	Jmis	VARIATION SHEE
9	Test Data Sheets 1, 4,9,10,12, 13,14	Add data block the FFDI vacification photo wabur.	Whn	eus	Jans	L
70	8.20	Add prengerph:  Inspect the Test Acticle Assembly for visual evidence of descendation due to previous testing. The good of the six retropeflectors tessen the #2 mounting screws and re-torque to the specified wature. To round be replace of any "frozen" screws, Lorsanne torque shall not exceed and mark screw heads so that	Mh.			
11	9.8	3.5 IN Lb., MARK SCREW heads so that Add para Graph:  I respect the Test Article Assembly for  VISUAL EVIDENCE of decado from due to  previous testing. Very that the  Retroreflector #2 mounting screw tightening  tagger has not decreased from the  specified value.	M	tal	Juis	

LAGEOS

THERMAL-OPTICAL TEST

TP2374455

oats 9 July 1974

r,		c
ß		VAKIATION SHEET
13		וט אטו
ß	bracket	7 (2015)
3.		
B		
3		

THERMAL-OPTICAL	
TEST	
	THERMAL-OPTICAL TEST

OPTIC.	COURT
Ą	
TEST	

PAGE 47/8 OF 48

**EATE** 9 July 1974

#	Reference Paragraph	Variation Description	BxA T.C.	Therm Eng.	Prog. Mgr.
12	9.1	Change to exad: "Vacify that extraoration E in the Test Article Paval has been REINSTALLED IN the 100 decree accentation. See Figure 9.	8Mm	Eaks	Jours
/3	2.7.1		Thi	Eass	Just
19	10.1 8/29			Elle	Jus
15	10.1 Shit 30	Add TC 30 \$31 ON Theread Future for PRE-TEST VERY function only.	M	Earl	Jus.
16	10.1 sht 29 \$ sht 30	Add theremocouple (Te) facilities Chronal numbers	Sh	EQ.X	gms
17	ON PAGE 6; 7.1, Item 3, 7.5, 7.6, 7.7— ON PAGE 7; 7.11 \$ 7.12- ON PAGE 8; 7.18, 7.19, 2/21 VALUATION 1/EM 3 PAGE 9; 7.24	DELETE AS LISTED.  BELETE AS LIS	A m	€0 <b>.8</b>	JmB
18		Add PAGES 8A, 8B &8C	STA	col	JmB
19		Add PAGE 27A, DWG Z 374458 X2 ECN	Som	Kası	Jms
20	_	Add DWGS 237 AAGG W/X3 ECN & 237 A459 AS FIGURES 1/4/2 RESPECTIVELY - PAGES 288, C, D	A m	Ray	graps.

			<del></del>	-	
#	Reference	Variation Description	BxA	P.	Prog.
	Paragraph		T.C.	Eng.	Mgr.
2/	Addendus I 2.6	Change collect to Dwg 2374466-X3.	Soft	8081	gmB
2 z	10.2	Add Test Sequence - As Run Summary	Ah	East	Jours.
23	PAGE 29 10.1	TC#17 LEAD WIRE INACCESSIBLE IN INSULATION BLOWKET. DELETE REQUIREMENT FOR TC#17, RETROX LOWER MOUNTING RING, THERMAL DATA	8/h 8-6-74 0400		
24	Paracra pin #8.5.2	CHANGE / X10-6 TORR TO 2 X 10 TORR	(7 & 8/4/74 1035	Kay	8/6/74 1045
25	PARA, 8.7	PERFORM TEST NO. 4 OUT-OF-SERVENCE, BEFORE TEST NO. 3	Mh	દળ જ	gmB 8/6/14 1140
26	8.7.2	Add sheets 144,148,196. Dalate poes. 8.6.7, 5/113; 8.6.8 Horu 8.6.4, 9/114; And 8.7.3 & 8.7.4, 5/14. Ref. TOR 04007	Whi.	10.1 2/8/7	Brug 14/5/8
21	sht 29 10.1	ROUNECT THERMOCOUPLES 15,16 for INSTRUMENTS INSTEAD OF DT MERSUREMENTS.  REF. TOR 04006	Ma	80 <u>N</u> 8/8/74	Just spalm
28	8.0 ¢ 3h+32 10.2	SEQUENCE of tosts prof be placed at the discretion of the Test Conductor with concurrence of the LAGEOS PROGRAM MOR & Thermal Engle. As-RUN SEQUENCE to be LOGGED ON Sht 32.	Mn 8/8/24	<b>EB</b> L 818/74	92-03

LAGEOS
THERMAL-OPTICAL TEST

ACCOUNT OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PAR

11.0

VARIATION SHEET

(06)

REV. NO.

TP2374455

9 July 1974

#	Reference Paragraph	Variation Description	BxA T.C.	Therm Eng.	Prog. Mgr.
29	8.12	ADD 8.12.3 SHUT DOWN IR LAMP	Wh	EVA	92.8 8.9-11
30	10.2 Outs Sheet 18	Repart operations of Test No. 2 10 order to provide browned doto office interruptive test for the wackers.	The	S. S.	gms
31	FIE 84 8642424 642 10.2 6644 37	TEST No. 5 Change Test Article temperature to +60°C and delete solve radiation. Take optical data for 15 view angles.	SPA	& DF	Jours
32	FIG 812 Sheet 26 AND 10.2 DATA LOG 3 8.16.1	Add Test No.19 Thermal vacuum Add paeaceaphs 8.16.2 & 8.16.2.1	Mh	ean	Jus
	FIG. 8A (SMEET 2G) & SECT. 10.2 (DATA LOG)	TOTAL LASER FIELD ANGLES FOR TEST # 11: "WAS" 8** "15" 15***	M 8-13-74	to.U	gan B
	Umpistion Item 10	DELETE VARIATION Item 10.	9/A 8-13-24	Œ03	graß
	8.21 9.22	Add prescent:  Inspect the Test Article Assembly for visual endance of decemberion dup to previous testing. Remove the #2 striviless scenus and replace with #2 pluminum screws, (AS 35202-8. Torque to 1.4 +0.7 in. lb.		श्वम	
36	F16 9, 24188	RE-IDENTIFY C RETED CONFIGURATIONS to ACREE with FIGURE 84.	30%	Cas	gnes

THERMAL-OPTICAL TEST

LAGEOS

VARIATION SHEET

TP2374455 PAGE 147 OF 48

**SATE 9** July 1974

c.	9	
	THERM	

AL-OPTICAL TEST LAGEOS

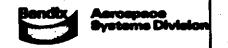
TP2374455 BATE 9 July 1974 48

#	Reference Paragraph	Variation Description	BxA T.C.	Therm Eng.	Prog. Mgr.	11.0
37	FIG. 84 4 9.2.1	Add 10.2 DATA LOG, Add MOA. 9.21,2.2.2	Mh	EOD	Jus	V.A
38	FIG. 8A \$	Add 10-2 Data Los	Sh	eass	Jus	VARIATION
39	FIG. 2 A; 10,2 TEX 10, 13 \$ Tast No. 14	Change VIEW ANGLES from 8 to 15 total for work Test, # 13 & #14.	Mh	Eals	gmb.	N SHEET
40	P.4GA	MSFC RAN PHOTOMETRIC MEASUREMENTS USING 1/2 ANNULUS AND GO PIE SHAPED MASKS TO DETERMINE DISTRIBUTION OF LASER RETURN ENERGY. THIS DATA IS FOUND ON R 46A.	Mh	Eas	gus	
41	FIG.8A 9.5.3	ADD TEST NO. 22 THERMAL- VACUUM AT FOOC +60°C ADD 10.2 DATA LOG 3/15/5/1990	BM 8-15-14	Earl	Jus	
42	FIG. 8A; 9.6.1 d Data Sheets 23424	Add Tests 23 924. Obtain optical data for for rateos D.E.F and A.B.C respectively at 1sothernal/publicat conditions.	8-15-74	لامة	Just	
		MOOA ST MOVA TWINDING				

### QUALITY ASSURANCE DEPT. TEST DISCREPANCY REPORT

					- <u> </u>	1040
237445		LAGEO!	5 700 7	3 SERIA	L NO.	08067
THERMS	4-10/06/	5 PROGR	AM NO. 6 LOC. PA	RA NO.	PART NO.	ŖΕ
FIXTURE A	RE REAL	sing much	colden to	DAN ANY 1	= mpenen/v	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			SO, THERM			
GIVING A	N ERRON	BOUS REA	DING.		:	en en en en en en en en en en en en en e
	÷	¥		ORIG	MATO Pher	MC.
MARY OF TROUBL	ESHOOTING/RESC	DLUTION	bient con	11+0	,	
Omered 7	TERMINE	la trans	antum 1	+ (100000		
PRIVE TO TENT S  PORTY S  LATA .  S/14/76  FORT  OPERATOR 5  BXA FACILITY 6	CONTRACT- PURCHASED FL	obtaining of a sacred to	CAUSE OF	ANOMALY:	CLASS	ELUS ANTA
Delve 7.  Teducy  Realys  Lata.  Staffs  PERATOR  S  EXA FACILITY  DEFECT  FOR	CONTRACT- PURCHASED FU TEST FIXTURIN ERROR	SERVED TEST E	CAUSE OF LOWN	ANOMALY:  S REVERSE  ACTORS OF	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CL	ELECTION OF DE CR CRITICA MA MAJOR
Delve 7. Tenuey Postys: Leta. S/14/76 PERATOR SA FACILITY 6 PEST 7	CONTRACT- PURCHASED FL TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI	JUNCTIONAL TEST E	CAUSE OF LOWN	ANOMALY:  S REVERSE  ACTORS OF	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CL	ELECTION OF DE CR CRITICA MA MAJOR
PANYS  Lata.  SIATOR  SEST DEFECT  FEST 6  TEST 7  TEST 7	CONTRACT- PURCHASED FU TEST FIXTURING ERROR  FACILITY OPER	JUNCTIONAL TEST E	CAUSE OF LOWN	ANOMALY:	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CL	ELECTION OF DE CR CRITICA MA MAJOR
PARTY SALATAR SPECTUP 7 TEST PROCEDURE B DDE 0	CONTRACT PURCHASED FU  TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED T  OTHER (EXPLA	JINCTIONAL TEST E NG DESIGN RATION BEROR SCREPANCY TO DR)	CAUSE OF LOWN	ANOMALY:  S REVERSE  ACTORS OF	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CL	CR CRITICA MA MAJOR MI MINOR PA PAPERV
PARTY TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP TO SET UP	CONTRACT PURCHASED FU  TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED T  OTHER (EXPLA OF THE ABOVE) RWK OR	JINCTIONAL TEST E NG DESIGN RATION BEROR SCREPANCY TO DR)	CAUSE OF LOWN	ANOMALY:  S REVERSE  ACTORS OF	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CL	ELECTION OF DE CR CRITICA MA MAJOR MI MINOR PA PAPERV  87
PROCEDURE B ODE O CENTER ONE C DISCREPANCY REPORT  WORK  TEST OPERATOR  5  CENTER ONE C ODE ODISCREPANCY REPORT  WORK  CT	CONTRACT- PURCHASED FL  TEST FIXTURING ERHOR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED TO OTHER (EXPLA OF THE ABOVE)  REPAIR EQUIP. CONTINUE	JINCTIONAL TEST E NG DESIGN RATION BEROR SCREPANCY TO DR)	CAUSE OF A SALANS	ANOMALY:  SETTING  LOCATION CODES  COMPONENT TEST  SUBASSEMBLY TEST  EXPERIMENT TEST	CLASS. RE-	CR CRITICA  MA MAJOR  MI MINOR  PA PAPERW  67  CK 63 ABOVE)  RMAL-VACUUM LA  ATTION LAB  BRATION LAB
PARTY TEST OPERATOR 5  BXA FACILITY 6  BXA FACILITY 6  BXA FACILITY 7  TEST 7  TEST 7  TEST 7  TEST 8  DOE 0  (ENTER ONE CONTERPORT REPORT CT	CONTRACT- PURCHASED FU  TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED T  OTHER (EXPLA  F THE ABOVE)  RWK OR REPAIR EQUIP. CONTINUE TEST	JINCTIONAL TEST E NG DESIGN RATION BEROR SCREPANCY TO DR)	CAUSE OF A SA = ET = ST = TL =	ANOMALY:  S. REVARS  ANOMALY:  S. REVARS  Extors  LOCATION CODES  COMPONENT TEST  SUBASSEMBLY TEST	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CCASIN  CCA	CR CRITICA  CR CRITICA  MA MAJOR  MI MINOR  PA PAPERW  BRAL-VACUUM LA  ATION LAB  BRATION LAB  B
TEST OPERATOR 5  BXA FACILITY OFFECT  TEST 7  TEST PROCEDURE B  ODE 0  (ENTER ONE C  DISCREPANCY REPORT  WORK REQUEST CT  CHANGE REQUEST OT OIRECTIVE  TEST OIRECTIVE  TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE  TEST TO THE TEST OT OIRECTIVE	CONTRACT- PURCHASED FL  TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED TO OTHER (EXPLAIR EQUIP, CONTINUE TEST  OTHER EXPLAIN	JINCTIONAL TEST E NG DESIGN RATION REFOR SCREPANCY TO DR)	CAUSE OF A SA = ET = ST = TL =	ANOMALY:  S REVARE  LOCATION CODES  COMPONENT TEST SUBASSEMBLY TEST SYSTEM TEST LAB  TRANSMITTER LAB	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CCASIN  CCA	MA MAJOR  MI MINOR  PA PAPERW  RAL VACUUM LAIATION LAB BRATION LAB SCREEN ROOM ATIC CHAMBER
PROCEDURE B ODE O IGENTER ONE C DISCREPANCY REPORT WORK REQUEST CHANGE REQUEST ODIRECTIVE TEST OTHER ONE C CHANGE REQUEST OTHER ONE C CHANGE REQUEST OTHER ONE C TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTHER TEST OTH TEST OTHER TEST OTHER TEST OTHER TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST OTH TEST	CONTRACT- PURCHASED FL  TEST FIXTURIN ERROR  FACILITY OPER PROCEDURE EI  HARDWARE DIS (CONVERTED TO OTHER (EXPLAIR EQUIP, CONTINUE TEST  OTHER EXPLAIN	JINCTIONAL TEST E NG DESIGN RATION REFOR SCREPANCY TO DR)	CAUSE OF A SA = ET = ST = TL =	ANOMALY:  S REVARE  LOCATION CODES  COMPONENT TEST SUBASSEMBLY TEST SYSTEM TEST LAB  TRANSMITTER LAB	CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CLASS  CCASIN  CCA	CR CRITICA  CR CRITICA  MA MAJOR  MI MINOR  PA PAPERW  6 7  CK 63 ABOVE)  RMAL-VACUUM LA  IATION LAB  BRATION LAB  SCREEN ROOM  ATIC CHAMBER  BAY AREA

special TC Tests RAF TOR OFFICE



TDR 04006 Attachnest

C

,							××	$\sim$		TEST.	PARAM	TER DA	TA REC	ORD				٠			e .				,
	ate .	Time [0-24Hz	11	12	13	14	15	16	18	19	20	51	22	23	24	25	•			_		1			•
I	8-1:74	14 55	-			-2.43	700,	.016			-7, 39	.001	.408						,				<del>  _</del>		1
ŀ	-	· · · · · ·				-2.33	.007	.018			-2,25	.005	.010		-		<del>                                     </del>				-	<u> </u>	<del>                                     </del>	<del> </del>	+
ļ							,008	,018			-2.24	1	.010						<u> </u>	:		<del>                                     </del>	<del> </del>	<del>                                     </del>	+
1				ļ	<u> </u>	-7.33			-2.44	,	-2.15	که .			2.42								<del>                                     </del>	<u> </u>	†
ŀ				<del>                                     </del>	<b> </b>	<del>  .</del>	7.40	1.51				2,30	2.34					/				1			†
I				<del> </del>	<u> </u>	<del> </del>	ļ	ļ					<i>:</i>	A	19										T
ŀ				<del> </del>	<del>-</del>	<del> </del>		2 45						2.0	ļ	(	1.0	1,5							I
١			<del></del>	1	<del> </del>		2.48					2.39		<del></del>						ļ	ļ		<u> </u>		I
ŀ	<u> </u>			<del> </del>	<del> </del>	1	2.47						2'.35			<del> </del>	<del> </del>			<del> </del>	ļ	<u> </u>		ļ	╧
l						4.34	1.43	4.71			7.74	7.30	2.33				ļ		<u> </u>	ļ	<del> </del>		<del> </del>	<del> </del>	1
Ī				Ī		28.5	26.5	28			50	29.	z 8.5				<u> </u>		<del>                                     </del>	<del> </del>	<del>  ` '</del>		┼		+
L				2.32	2.32		235				2.43	_	2.42				<del> </del>	<del></del>	1	-			<del> </del>	-	+
				83	83	80	83	80			80	81	81					<u> </u>				,	-	-	╀
L				2.16	<u>ما ۱۰</u>		2.72				240	2.36	2.35							<del>                                     </del>			<del>                                     </del>	<del> </del>	$\dagger$
L		-		විම	88			82.5				82.5										-	<b></b>		t
┞		<del></del>	:	C 100 mg			2.06				2.32	7.24	2.24					-		-			<b> </b>		t
ŀ				1.97	1.97		2.06			į	2.32	2.26	2.24	2.03	2.12	2.68					~				t
ř				1.86	1.86		91.5			90	23	86.5	84	92	<u> </u>	91									Ī
!	2-7-74	1602	<del>)                                    </del>	97			1 <b>94</b> 95			94	2.22	2.15	2,13	1.92											I
	,	-1				71617	7		707	79	261)	89	89	95.5	93	94			<u> </u>	ļ	4	-	<del> </del>	-	$\downarrow$
_		approp			<u> </u>																	<u> </u>		<del>                                     </del>	†

for each test parameter to be monitored.

## QUALITY ASSURANCE DEPT. TEST DISCREPANCY REPORT

									10	48
23744	BE NO.	REV.   1	PART NAME		DC. PARA NO.	3 SERIA	PART N	////3 <sup>3</sup>	08	F 7
THERM	194	- VACU	100 \$ 636	51/37	1 8.7					
SCRIPTION OF	ANOMAL	S RE	trorafled Rutror	tors	APPE	AR to		VE C	ent	ante.
ON	SUK	1 90-2.								· ·
			TYPRODUCIB ORIGINAL PA	ility oi age is f	THE	u*	•			
		: .	OSIGNATIA	XCXX, 100						÷
						ORIGI		eono	<u> </u>	•
C L B 7/74 C L E <b>3</b> 6	ANING	compre	S REPERENCE ANTS SHALL TED AND TES	T ARTI	CLE REAS	56m 8 L G	o PRA	. <i>Test</i> .	.dv.2. €c	WF I GUI
TEST		CONTRACT	NCTIONAL TEST EQ		USE OF ANOMA	/		-	FICATIO	******
BXA FACILITY DEFECT	/ _	TEST FIXTURIN			undagu. Unets p	rte cl	to o	rue o Elela		MAJOR
TEST SET-UP	1.1	FACILITY OPER		<b>-</b>   '.	parts proceeds a proceeds a post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the post of the po	bly, do	u to	Chas	K	MINOR
TEST PROCEDURE		HARDWARE DIS			to Add A	I. KB PERAT	Tovs	> / 444 -	PA	PAPERW
ODE TENTER		OTHER (EXPLA	IN)≖							6 7
DISCREPANO REPORT	7	RWK OR REPAIR				TION CODES	10000	IN BLOC	V 63 ABC	11
WORK		EQUIP.			CT = COMPO	NENT TEST	_AB	TV = THER	MAL-VA	DUM LA
CHANGE	ст	CONTINUE TEST.		÷	CT = COMPO SA = SUBASS ET = EXPER ST = SYSTEM	NENT TEST ( SEMBLY TEST MENT TEST I TEST LAB MITTER LAB	_AB T LAB LAB	TV = THER VL = VIBR, CL = CALIE EM = EMI/S CC = CLIM, HB = HIGH	IMAL-VAC ATION LA BRATION SCREEN F ATIC CHA	CUUM LAE LAB LOOM MBER
CHANGE AEQUEST DIRECTIVE TEST OR DISCREPANCE	от	CONTINUE TEST OTHER EXPLAIN	9)		CT = COMPO SA = SUBASS ET = EXPER ST = SYSTEM TL = TRANS	NENT TEST ( SEMBLY TEST MENT TEST I TEST LAB MITTER LAB	_AB T LAB LAB	VL = VIBR. CL = CALIE EM = EMI/S CC = CLIM.	IMAL-VAC ATION LA BRATION SCREEN F ATIC CHA BAY ARI	CUUM LAB LAB LAB IOOM MBER EA
CHANGE REQUEST DIRECTIVE	от	CONTINUE TEST OTHER EXPLAIN	9)		CT = COMPO SA = SUBASS ET = EXPER ST = SYSTEM TL = TRANS	NENT TEST ( SEMBLY TEST MENT TEST I TEST LAB MITTER LAB	_AB T LAB LAB	VL = VIBR, CL = CALIE EM = EMI/S CC = CLIM, HB = HIGH	IMAL-VAC ATION LA BRATION SCREEN F ATIC CHA BAY ARI	CUUM LAI AB LAB IOOM MBER A

### QUALITY ASSURANCE DEPT. TEST DISCREPANCY REPORT

<del>-</del> .					•					
	;				•				1 k	A da
TEST PROCED	URE NO	D. REV.	PART NAME	ا اصلا	4 101 1 4 A	3 SEF	IAL NO.	/////3	MO.	DAY YA
2374	75	5    X / °	L 19 6 E	10 5   7	OV TH	2/2 2	PART	NO	03	9777 BEV
THERM	احراء	c NAC	UM BE	36 5/	3718.7	12_				
DESCRIPTION OF	ANOM	IALY FOR	data	Pans	FFDI	15 A	e MA	duc	Lon	<b>"</b>
110	PA	MAJAIL	,				1			:
9					•		. * , v:		e <sup>n</sup> ,	
							•			
					ř		F 1			
		·			•					
								v V		
						·	tak E			· ·
	•			•		7	IGINATO	hune		
SUMMARY OF TR	OUBL	SHOOTING	LUTION	+	KAM SI	1				140
Su	عبرو	عر عمد بر	FDI	BXV B	ENT SI	nows.	NON-	WITT	CH.	
ACA	05	S bEAM.		4						
		LI	1	marka	LE IN 1 Y. Adds.	EFD.	$\mathbf{z}$		FAL	
KM-	NO	JUNIAG Z	300.00 J	بر مرس		7 -	7	1	<i>Z</i> =	
	$\mathcal{L}_{\mathcal{A}}$	رمحمط منده	es last.	TENSIT	y Adds	TIONAL	, ,900			
	, - , -		4	-			L 42.		1 /	L
RE	OC	T RETI	go A	ORA	731163	, 123/	76	, ,		1200
, ,	7	he REST	' of the	the res	guired	data			•	
v								•		•
£										•
	•	•		•						•
	<del>1  </del>				CAUSE OF ANOI	MALY:		TCL ASSI	EICATIO	ON OF DEFE
TEST OPERATOR	5	CONTRACT- PURCHASED FL	INCTIONAL TI	EST EQUIP.			la.			CRITICAL
2 BXA FACILIT	Y 6	TEST FIXTURIN	IG DESIGN		of Adv	vetue	T.		МА	MAJOR
DEFECT		ERROR	· ·				÷	•	-H	
3 TEST SET-UP	ブ	PROCEDURE ER			_]				МІ	MINOR
4 TEST PROCEDURE	8	HARDWARE DIS					-		PA	PAPERWO
6 CODE	0	OTHER (EXPLA	(IN)=		_				لنا	6 00
502 TENTER	ONE O	F THE ABOVE)						·		7
DR DISCREPAN	CY RR	RWK OR REPAIR	:		LO.	CATION COD	ES (ENTI	R IN BLOCK	63 AB	OVE)
		CONTINUE				IPONENT TES ASSEMBLY T		TV = THER		CUUM LAB
WR REQUEST	СТ	TEST				ERIMENT TE: FEM TEST LA		CL = CALIB	RATION	1 LAB
CHANGE CRD REQUEST	от	OTHER				NSMITTER L		CC - CLIMA	TIC CH	AMBER
DIRECTIVE		EXPLAIN			, E - 1 '9'E			OP - OUT O		
TOR DISCREPAN	CY (E	NTER IN BLOCK 6	9)							
6 CODE			$\neg$						S-	112
9 <b>70</b> R _	10		RYAO	A REPRESENT	TATIVE	100	WT COLL	ne pena	· ·	<u> </u>
TEST CONDUCT	)" 4		15777	A REPUBLIENT	A	160		CE REPRESE	N FATIN	/ E

### QUALITY ASSURANCE DEPARTMENT TEST DISCREPANCY REPORT

CONTINUATION SHEET TDR NO. OAOO Page 2 of 2 Test Procedure No. Date 8 Aug 74 2374455-X/

RE-Advestment of bean probable did not concert the FFDI matteration. Manufacturine's Rep. called in.

8-8-74 Action by Zreo REP.

1. RE-Advisted probable

2. RE-adverted Laser bean uniformity
3. Reduced interesty to loser monitor
4. Removed one (of two) newheal deventy letter from ca

5. Dooted all optics.

### QUALITY ASSURANCE DEPT. TEST DISCREPANCY REPORT

(114)	
1	

•								Pa	g <del>e</del> or .
					:			10	MACV
TEST PROCEDU	DRE NO.	REV. 1 PA	RT NAME	ا جا ما درا	int a	SERIAL NO	////	3 MO.	DAY YA
NAME OF TEST	756	K N 1	PROGRAM N	10. 6 LOC.	IPARA NO.	PAR	Y////// T NO.	100	REV
THERES	104-0	PTI	2 6 5 6 5	3	9.2.2.1				
SCRIPTION OF	ANOMALY TER TA	kne	the field	st 5	doto,	POINT	s, jt Nusi	was	t wa
os.	f by.	OPPR	ox mote	y +1	decen	e tiet	d'VIE	wp.	rche
	!					•	· '.		
								,	
•		,			,				
						,			
	•					ORIGINA	0/1	<u> </u>	•
÷.	<u>.</u>					SM	KUDI	WC_	
MMARY OF TR	OUBLESHOOT	NG/RESOLU	TION SENIER	4 -		-	f.f.		
Ka	r-Addu	ST VA	ERNIAE R	70 P	Roper			· P	
· Pa	at Wal	en in	c siew	To 6	bock .	5 <i>ETT</i> )	ve b	210	<b>VEN</b>
,			· I III e I		1 <i>SEDI</i>				
							1 44 .		
9.1	HTER		-		1 D _	- 1 1		7 <i>0</i>	
•			4	المدجد معد و	Te Kap	724	No.	70	
•			4	المدجد معد و	Te Kap	724	No. I	eta	Loc
RE BA	y con	sh . truva	NEASURE test.	المدجد معد و	Te Kap	724	No. 2	eta	Loc
RE	y con	sh . truva	4	المدجد معد و	Te Kap	724	Mo. I	eta	Loc
RE	y con	sh . truva	NEASURE test.	المدجد معد و	Te Kap	724	Mo. I	et n	206
RE	y con	sh . truva	NEASURE test.	المدجد معد و	Te Kap	724	Mo. I	et p	Loc
R. A. A. A. TEST	d con	sh struck	NEASURE test.	Ida	OF ANOMALY:	TE	Lei as	SIFICATIO	ON OF DEF
TEST OPERATOR	S CONTINUES TEST	sh struck	AEDSURA TEST. 20 A.	Ida	OF ANOMALY:	TE	Lei as	SIFICATIO	ON OF DEF
REST.	5 CONTINUEST ERRO	RACT HASED FUNC	AEDSURA FEST. 20 A. TIONAL TEST EQUIP	Ida	estify	TE	Lei as	SIFICATIO	ON OF DEF
TEST OPERATOR BXA:FACILITY	5 CONTIPURCH	RACT FUNC	ASPSURE TEST. 20 A.	Ida	OF ANOMALY:	TE	Lei as	SIFICATIO	ON OF DEF
TEST OPERATOR BXA-FACILITY DEFECT TEST SET-UP TEST	5 CONTIPURCY 6 TEST ERRO 7 FACIL PROCE	RACT HASED FUNCE FIXTURING ER	TIONAL TEST EQUIPOR	Ida	OF ANOMALY:	TE	Lei as	SIFICATION CR	ON OF DEF CRITICA MAJOR MINOR
TEST OPERATOR BXA:FACILITY DEFECT TEST SET-UP TEST PROCEDURE	5 CONTINUEST ERROLL 7 FACIL PROCES 8 HARD (CONV	RACT HASED FUNCE FIXTURING ER ER ER ER ER ER ER ER ER ER ER ER ER	TIONAL TEST EQUIP	Ida	OF ANOMALY:	TE	Lei as	SIFICATIO CR MA	ON OF DEF CRITICA MAJOR MINOR PAPERW
TEST OPERATOR BXA-FACILITY DEFECT TEST SET-UP TEST PROCEDURE CODE	5 CONTINUE FACIL PROCES  7 FACIL PROCES  8 HARD (CONV	RACT-HASED FUNCE FIXTURING CR ITY OPERATEDURE ERROUMERED TO DO RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE RECEIVED TO DE REC	TIONAL TEST EQUIP	Ida	OF ANOMALY:	TE	Lei as	SIFICATIO CR MA	ON OF DEF CRITICA MAJOR MINOR PAPERW
TEST OPERATOR  BXA:FACILITY DEFECT  TEST SET-UP  TEST PROCEDURE CODE O3 (ENTER	5 CONTIPURCH FACIL PROCI B HARD (CONV O OTHE ONE OF THE A	RACT HASED FUNCE FIXTURING ER ERROURE ERROURE ERROURE ERROURE ERROURE ERROURE ERTED TO OR (EXPLAIN)	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	Ida	OF ANOMALY	TE	GIAS Top.	SIFICATION CRIMA	ON OF DEF CRITICA MAJOR MINOR PAPERW
TEST OPERATOR  BXA:FACILITY DEFECT  TEST SET-UP  TEST PROCEDURE CODE O3 (ENTER	5 CONTINUENCE 7 FACIL PROCE 8 HARD (CONV 0 OTHE ONE OF THE A	RACT- HASED FUNC  FIXTURING C  ITY OPERAT EDURE ERRO  WARE DISCR ER (EXPLAIN): BOVE)  OR IR	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	OF ANOMALY.  OF ANOMALY.  LOCATION  CT = COMPONEN	Sock-	TER IN BLO	SIFICATION CAMPA  MI  PA  CK 63 ABG  RMAL-VA	MAJOR MINOR PAPERWOOVE) CUUM LA
TEST OPERATOR  BXA:FACILITY DEFECT  TEST PROCEDURE CODE OB (ENTER REPORT	5 CONTIPURCH 7 FACIL PROCI 8 HARD (CONV 0 OTHE ONE OF THE A CY RR REPA EQUI	RACT- HASED FUNC  FIXTURING C R  STY OPERAT EDURE ERRO WARE DISCR ERTED TO O R (EXPLAIN): BOVE)  OR IR P. TINUE	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	LOCATION CT = COMPONEN SA = SUBASSEME ET = EXPERIMEN	SCODES (EN IT TEST LAB	TER IN BLO	SIFICATION LIBRATION L	MAJOR  MINOR  PAPERWO  OVE)  CUUM LAI  AB
TEST OPERATOR  BXA:FACILITY DEFECT  TEST PROCEDURE  CODE O 3 (ENTER REPORT  WORK REQUEST  CHANGE CO REQUEST	5 CONTIPURCION 6 TEST FACIL PROCI 8 HARD (CONV 0 OTHE ONE OF THE A CY RR REPA EQUI CT CONT TEST OT OTHE	RACT HASED FUNCE FIXTURING ER ERTED TO O OR (EXPLAIN) OR IR P. TINUE	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF ANOMALY:  OF AN	CODES (EN IT TEST LAB BLY TEST LAB ST LAB	TER IN BLOG  TV = THE  VL = VIBI CL = CALL EM = ELIN CC = CLIN HB = HIG	SIFICATION CR MA MI PA CK 63 ABI RMAL VA RATION L IBRATION JOSCHEEN MATIC CH H BAY AR	MAJOR  MINOR  PAPERWO  OVE)  CUUM LAI  AB  I LAB  ROOM  AMBER EA
TEST OPERATOR  BXA:FACILITY DEFECT  TEST PROCEDURE  CODE OB (ENTER REPORT  WORK REQUEST DIRECTIVE TEST PROCEDURE  CODE OB (ENTER REPORT	5 CONTIPURCH 7 FACIL PROCI 8 HARD 1 CONV 0 OTHE ONE OF THE A CY RR REPA EQUI CT CONT TEST OT OTHE EXPL	RACT HASED FUNC FIXTURING D R LITY OPERAT EDURE ERRO WARE DISCR ERTED TO O R (EXPLAIN) BOVE) OR IR INUE	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	LOCATION CT = COMPONEN SA = SUBASSEMI ET = EXPERIMEN ST = SYSTEM TE TL = TRANSMIT	CODES (EN IT TEST LAB BLY TEST LAB ST LAB	TER IN BLOG  TV = THE  VL = VIBI CL = CALL EM = ELIN CC = CLIN HB = HIG	SIFICATION  CR  MA  MI  PA:  CK 63 ABG  RMAL VA  RATION L  IBRATION  /SCREEN  MATIC CH/	MAJOR  MINOR  PAPERWO  OVE)  CUUM LAI  AB  I LAB  ROOM  AMBER EA
TEST OPERATOR  BXA-FACILITY DEFECT  TEST PHOCEDURE  CODE  J (ENTER REPORT  REQUEST DIRECTIVE TEST DIRECTIVE	5 CONTIPURCH 7 FACIL PROCI 8 HARD 1 CONV 0 OTHE ONE OF THE A CY RR REPA EQUI CT CONT TEST OT OTHE EXPL	RACT HASED FUNC FIXTURING D R LITY OPERAT EDURE ERRO WARE DISCR ERTED TO O R (EXPLAIN) BOVE) OR IR INUE	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	LOCATION CT = COMPONEN SA = SUBASSEMI ET = EXPERIMEN ST = SYSTEM TE TL = TRANSMIT	CODES (EN IT TEST LAB BLY TEST LAB ST LAB	TER IN BLOG  TV = THE  VL = VIBI CL = CALL EM = ELIN CC = CLIN HB = HIG	SIFICATION CR MA MI PA CK 63 ABI RMAL VA RATION L IBRATION JOSCHEEN MATIC CH H BAY AR	MAJOR  MINOR  PAPERWO  OVE)  CUUM LAE AB I LAB ROOM AMBER EA T
TEST OPERATOR  BXA-FACILITY DEFECT  TEST PHOCEDURE  CODE  JENTER REPORT  REQUEST DIRECTIVE TEST DIRECTIVE TEST DISCREPANCE REQUEST DIRECTIVE TEST DIRECTIVE	5 CONTIPURCH 7 FACIL PROCI 8 HARD 1 CONV 0 OTHE ONE OF THE A CY RR REPA EQUI CT CONT TEST OT OTHE EXPL	RACT HASED FUNC FIXTURING D R LITY OPERAT EDURE ERRO WARE DISCR ERTED TO O R (EXPLAIN) BOVE) OR IR INUE	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	LOCATION CT = COMPONEN SA = SUBASSEMI ET = EXPERIMEN ST = SYSTEM TE TL = TRANSMIT	CODES (EN IT TEST LAB BLY TEST LAB ST LAB	TER IN BLOG  TV = THE  VL = VIBI CL = CALL EM = ELIN CC = CLIN HB = HIG	SIFICATION CR MA MI PA CK 63 ABI RMAL VA RATION L IBRATION JOSCHEEN MATIC CH H BAY AR	ON OF DEF CRITICAL MAJOR MINOR PAPERWO OVE) CUUM LAF AB I LAB ROOM AMBER EA
TEST OPERATOR  BXA:FACILITY DEFECT  TEST SET-UP  TEST PROCEDURE  CODE OB (ENTER REPORT REQUEST DIRECTIVE TEST OR DISCREPANCE TEST OR DISCREPANCE TEST OR DISCREPANCE	5 CONTIPURCH 7 FACIL PROCE 8 HARD 1 CONV 0 OTHE ONE OF THE A CY RR REPA EQUI CT CONT TEST OT OTHE EXPL CY (ENTER IN	RACT HASED FUNCE FIXTURING ER TEDURE ERROUNDE ERROUNDE BOVE) OR (EXPLAIN) BOVE) OR (EXPLAIN) BOVE) OR (EXPLAIN) BOVE) OR (EXPLAIN) BOVE)	ASASURA TEST. 20 A. TIONAL TEST EQUIP DESIGN	CAUSE	LOCATION CT = COMPONEN SA = SUBASSEMI ET = EXPERIMEN ST = SYSTEM TE TL = TRANSMIT	CODES (EN IT TEST LAB ST LAB ST LAB TER LAB	TER IN BLOG  TV = THE  VL = VIBI CL = CALL EM = ELIN CC = CLIN HB = HIG	SIFICATION CAN MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA MI MA	ON OF DEF CRITICAL MAJOR MINOR PAPERWO 7 OVE) CUUM LAB ALAB ROOM AMBER EA T



# LAGEOS THERMAL-OPTICAL TEST

HO.		186	/. <b>HO</b> .
TP23	74455	<u>.L</u>	
PAGE .	48	or <u>.</u>	48
DATE	9 Ju	ly l	974

12.0 TEST SIGN-OFF SHEET

CT. Store 8/19/74
Environmental Object Test T-V Engineer

Bavironmental/Quality Test Conductor

E.a. Stranholm 8-19-74

Jacker 8-19-74
LAGEOS Program Manager



Aerospace Systems Division

# LAGEOS Thermal-Optical Test

Addendum I

(119)	TP2374455					
	Page Al of	2				
	Date 9 July 1974	ļ				

1.0 This addendum specifies the LAGEOS Test Article and Fixture assembly operations. Hardware items included are: Test Article Panel, PN 2374464; Thermocouple Fixture, PN 2374466; Fixture Thermal Assembly, PN 2374460-23; LAGEOS Retroreflectors (6); and ALSEP Retroreflectors (2).

### 2.0 ASSEMBLY OPERATIONS

2.1 Clean the Test Article Panel, Thermocouple Fixture, and the Fixture Thermal Assembly per Dwg. 2374465.

2.2 Attach the Thermocouple Fixture to the Fixture Thermal Ass'y. using the machine screws provided. Thermal grease is to be applied on the interface surfaces.

- 2.3 Attach thermocouples, 12 and 13, to the Thermocouple Fixture. See Figure 6. Dress leads thru the access holes.
- 2.4 Attach thermocouples, 10, and 11, to the Test Article Panel. See Figure 6. Dress leads across the block between the rows of retro cavities.
- 2.5 Bond thermocouples, 15 thru 19 and 21 thru 25, onto the ALSEP retros and mounting rings. See Figure 6.
- 2.6 Install the ALSEP retros in the Thermocouple Fixture per Dwg. 2374466-X2. Dress leads thru the gavity access holes. See Figure 6.
  - 2.7 Bond thermocouples, 14 and 20, to the front face center of the ALSEP Retros. See Figure 6. Dress leads across block to nearest edge.
- 2.7.1 When adhesive of 2.7 is dry, apply a small dot of adhesive on top of the thermocouple and emplace a 1/8 inch diameter spot of aluminized mylar with the aluminized side up.

2.8 Cut an aluminized mylar insulation blanket and fit to the assembly. The blanket is to fold into the Fixture Thermal Assembly approximately one inch on all four sides.

v \$19/17

2/1/24

2 4/3/11/ al-las

28/2/74

-8/2/74

18/2/24

1 8/2/24

L 8/5/24



# LAGEOS Thermal-Optical Test

- 1		
	TP237445	5
		_

Date 9 July 1974

### Addendum I

Aerospace Systems Division

2.9 Install the Test Article Panel into the Fixture Thermal Assembly after applying thermal grease to the interface surfaces. Secure with the 1/4 - 20 machine screws provided.

~ 8/5/19

Use CAUTION to avoid tearing the insulation blanket.

2.10 Install the six LAGEOS retros in the Test Article Panel for the Test No. 1 configuration. See Figures 8 and 9.

-9/5/19

2.11 Fit the insulation blanket loosely around the entire assembly.

- 8/5/74

3.0 On completion of assembly operations, place the assembly in a plastic bag for temporary storage protection.

NA

### APPENDIX T

# LAGEOS RETROREFLECTOR ACCEPTANCE DATA CERTIFICATES OF COMPLIANCE

ZYGO CORPORATION

Dated August 1, 1974

NOTE: Photograph Scale Factor:
1.00 MM in appendix photo = 1.04 MM in original photo.

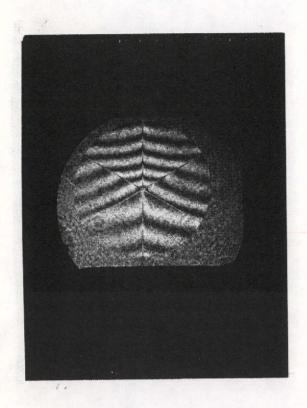


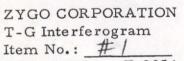
# CERTIFICATE OF COMPLIANCE

Item: C	ube Corner; LAGEOS - Phase B	
Item I. D	. No.:	
Contract	No.: T-2954	·
Applicab	le Documents:	•
1) 2)	Drawing No.: 9118-1001 Rev. B (Zygo) Specification: LAG-1 (Bendix)	-
Specifica	tions:	
1)	Material (T-19 Suprasil 1 Special)	OK
	Figure Tolerance R1, R2, R3 ( $^{\lambda}$ /10) R4 ( $^{\lambda}$ /8)	OK_
3)	Far Field Diffraction Pattern (See attached photo)	<u>OK</u>
4)	Wavefront Flatness of Each Sector (See attached Interferogram)	OK
5)	Protective Bevels	OK
6)	Physical Dimensions	OK
7)	Workmanship	OH
This is to	certify that the cube corner, I.D. No is in conecifications and drawings of ghe Bendix purchase order	nformance with r T-2954.

ZYGO CORPORATION Laurel Brook Road

Middlefield, Connecticut 06455



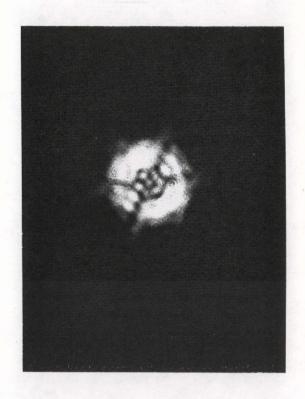


Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

(R1, R2 + R3) Chemically Silvered



ZYGO CORPORATION Far Field Diffraction Pattern

Item No. # /

Contract No.: T-2954 Cube Corner: LAGEOS Phase B

Date: August 1, 1974 Scale: 1.47 arc sec/mm

Uncoated Surfaces



### DATA SHEET

<u>Item:</u>	Cube Corner; LAGEOS - Phase B		
Item I	. D. No.:		ı
Contra	act No.: T-2954		
Applic	able Documents:		
	<ol> <li>Drawing No.: 9118-1001 Rev.</li> <li>Specification: LAG-1 (Bendix)</li> </ol>		
Data:			
	1) Wavefront Deviation of each Se (Sector 1 is at one o'clock. Go		•
	$\lambda = 632.8nm$	Sector 1	0.2 h
		Sector 2	0.15 h
		Sector 3	0,10 h
		Sector 4	0.12 1
		Sector 5	0,10 h
		Sector 6	0.15
	2) Dihedral Angles	•	
		R1-R2	2.00 arc sec
		R2-R3	0,92 arc sec
		R1-R3	1.24 arc sec
	3) Diameter of Annulus Centroid		22.0 arc sec

ZYGO CORPORATION

C. A. Zanoni

Laurel Brook Road Middlefield, Connecticut 06455



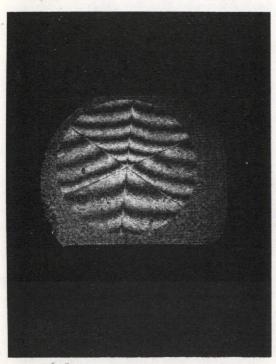
## CERTIFICATE OF COMPLIANCE

Item I.D. No.: Z  Contract No.: T-2954  Applicable Documents:  1) Drawing No.: 9118-1001 Rev. B (Zygo) 2) Specification: LAG-1 (Bendix)  Specifications:  1) Material (T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (^/10) R4 (\(\chi/8\)) 3) Far Field Diffraction Pattera (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions  OU  OU  OU  OU  OU  OU  OU  OU  OU  O	Item: Cu	be Corner; LAGEOS - Phase B	•
Applicable Documents:  1) Drawing No.: 9118-1001 Rev. B (Zygo) 2) Specification: LAG-1 (Bendix)  Specifications:  1) Material (T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (\(^{\lambda}/10\)) R4 (\(^{\lambda}/8\)) 3) Far Field Diffraction Pattera (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	Item L.D.	No.: 2	
1) Drawing No.: 9118-1001 Rev. B (Zygo) 2) Specification: LAG-1 (Bendix)  Specifications:  1) Material (T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (\(^{\lambda}/10\)) R4 (\(^{\lambda}/8\))  3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	Contract	No.: T-2954	
2) Specifications: LAG-1 (Bendix)  Specifications:  1) Material (T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (\(\lambda\)/10) R4 (\(\lambda\)/8)  3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	Applicabl	e Documents:	
1) Material (T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (\(^{\lambda}/10\) R4 (\(^{\lambda}/8\)  3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	1) 2)	Drawing No.: 9118-1001 Rev. B (Zygo) Specification: LAG-1 (Bendix)	
(T-19 Suprasil 1 Special)  2) Figure Tolerance R1, R2, R3 (\(\lambda/10\)) R4 (\(\lambda/8\))  3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	<b>Specificat</b>	ions:	
R1, R2, R3 (^/10) R4 (\(\chi/8\)  3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	1)		04
3) Far Field Diffraction Pattern (See attached photo)  4) Wavefront Flatness of Each Sector (See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	2)	R1, R2, R3 ( $^{\lambda}/10$ )	OK
(See attached Interferogram)  5) Protective Bevels  6) Physical Dimensions	3)	Far Field Diffraction Pattern	OK
6) Physical Dimensions	4)		OK
	5)	Protective Bevels	OU
7) Workmanship	6)	Physical Dimensions	OH
	7)	Workmanship	OU

This is to certify that the cube corner, I.D. No. \_\_\_\_ is in conformance with all the specifications and drawings of ghe Bendix purchase order T-2954.

C.A. Zanoni

ZYGO CORPORATION Laurel Brook Road Middlefield, Connecticut 06455



#2

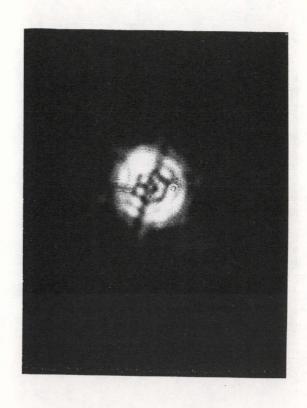
ZYGO CORPORATION T-G Interferogram Item No.: #2 Contract No.: T-2954

Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

(R1, R2 + R3) Chemically Silvered



ZYGO CORPORATION Far Field Diffraction Pattern

Item No. #7 Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

Scale: 1.47 arc sec/mm

Uncoated Surfaces



### DATA SHEET

Item: Cube Corner; LAGEOS - Phase B

Item I. D. No.:

Contract No.: T-2954

### Applicable Documents:

1) Drawing No.: 9118-1001 Rev. B (Zygo)

2) Specification: LAG-1 (Bendix)

### Data:

1) Wavefront Deviation of each Sector (Sector 1 is at one o'clock. Gount GW)

$\lambda = 632.8 \text{nm}$	Sector 1	0,20 %
	Sector 2	0-15 h
	Sector 3	$\frac{-G_1/7}{\lambda}$
	Sector 4	0.20 h
	Sector 5	O(10)
	Sector 6	0.20 h

2) Dihedral Angles

R1-R2	2,05 a	rc se	e c
R2-R3	1.54 a.	rc se	c
R1-R3	1.83 a	rc se	C

3) Diameter of Annulus Centroid

19.8 arc sec

C. A. Zanoni

ZYGO CORPORATION Laurel Brook Road Middlefield, Connecticut 06455



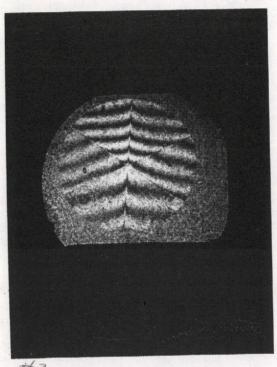
Date: August 1, 1974

# CERTIFICATE OF COMPLIANCE

Item: Cube	Corner; LAGEOS - Phase B	<u>.</u>
Item I. D. No	.: _3	
Contract No.	: T-2954	
Applicable D	ocuments:	
1) Dı 2) Sp	awing No.: 9118-1001 Rev. B (Z) ecification: LAG-1 (Bendix)	ygo)
Specification	<u>1:</u>	
•	sterial -19 Suprasil 1 Special)	OK
	gure Tolerance , R2, R3 (λ/10) (λ/8)	OK
3) Fa	r Field Diffraction Pattern ee attached photo)	OK
	vefront Flatness of Each Sector se attached Interferogram)	OK
5) Pr	otective Bevels	OK
6) Ph	ysical Dimensions	OU
7) Wo	rkmanship	<u>ou</u>
This is to certall the specif	ify that the cube corner, I.D. No. cations and drawings of ghe Bendi	is in conformance with purchase order T-2954.
•		C. A. Zanoni
		ZYGO CORPORATION

Laurel Brook Road

Middlefield, Connecticut 06455



#3

ZYGO CORPORATION T-G Interferogram

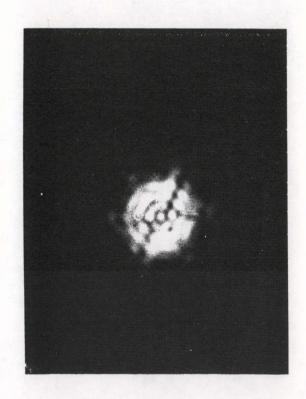
Item No.: #3

Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

(R1, R2 + R3) Chemically Silvered



ZYGO CORPORATION

Far Field Diffraction Pattern

Item No. #3

Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

Scale: 1.47 arc sec/mm

Uncoated Surfaces



### DATA SHEET

Item: Co	ube Corner;	LAGEOS	_	Phase	В
----------	-------------	--------	---	-------	---

Item I. D. No.: 3

Contract No.: T-2954

### Applicable Documents:

1) Drawing No.: 9118-1001 Rev. B (Zygo)

2) Specification: LAG-1 (Bendix)

### Data:

1) Wavefront Deviation of each Sector (Sector 1 is at one o'clock. Gount GW)

$\lambda = 632.8 nm$	Sector 1	0.15 1
	Sector 2	0.15 X
	Sector 3	0,10 h
	Sector 4	0.10 h
	Sector 5	0.10 h
	Sector 6	. 0.10 h

2) Dihedral Angles

R1-R2		1.81	arc	вес
R2-R3		1.08	arc	sec
R1-R3	•	1.42	arc	sec

3) Diameter of Annulus Centroid

17.6 arc sec

C. A. Zanom

ZYGO CORPORATION Laurel Brook Road Middlefield, Connecticut 06455



## CERTIFICATE OF COMPLIANCE

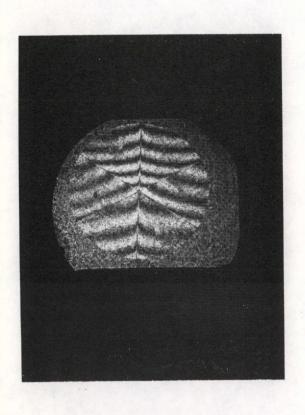
Item: Cube Corner; LAGEOS - Phase B	
Item I. D. No.: 4	•
Contract No.: T-2954	
Applicable Documents:	
<ol> <li>Drawing No.: 9118-1001 Rev. B (Zygo)</li> <li>Specification: LAG-1 (Bendix)</li> </ol>	. :
Specifications:	
1) Material (T-19 Suprasil 1 Special)	OK
2) Figure Tolerance R1, R2, R3 ( <sup>λ</sup> /10) R4 (λ/8)	OK
<ol> <li>Far Field Diffraction Pattera (See attached photo)</li> </ol>	OK
4) Wavefront Flatness of Each Sector (See attached Interferogram)	OU
5) Protective Bevels	OK
6) Physical Dimensions	04
7) Workmanship	04
This is to certify that the cube corner, I.D. No is in corall the specifications and drawings of ghe Bendix purchase order	formance with T-2954.
Carl	Janom'

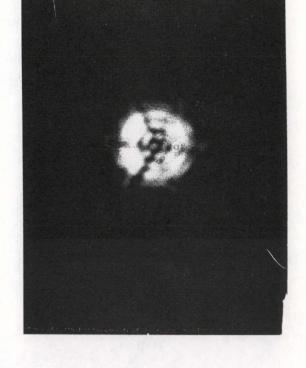
Date: August 1, 1974

ZYGO CORPORATION Laurel Brook Road

Middlefield, Connecticut 06455

# ZYGO





ZYGO CORPORATION
T-G Interferogram
Item No.: #4
Contract No.: T-2954
Cube Corner: LAGEOS
Phase B
Date: August 1, 1974

(R1, R2 + R3) Chemically Silvered

ZYGO CORPORATION
Far Field Diffraction Pattern
Item No. # /
Contract No.: T-2954
Cube Corner: LAGEOS
Phase B
Date: August 1, 1974
Scale: 1.47 arc sec/mm
Uncoated Surfaces



### DATA SHEET

<u>Item:</u>	Cube	Corner;	LAGEOS	-	Phase	B

Item I. D. No.: 4

Contract No.: T-2954

### Applicable Documents:

1) Drawing No.: 9118-1001 Rev. B (Zygo)

2) Specification: LAG-1 (Bendix)

### Data:

1) Wavefront Deviation of each Sector (Sector 1 is at one o'clock. Count CW)

Sector 1	0.20 h
Sector 2	0.10 h
Sector 3	0,20 h
Sector 4	() \lambda
Sector 5	0.15 A
Sector 6	6.70 X
	Sector 2 Sector 3 Sector 4 Sector 5

2) Dihedral Angles

R1-R2	2.00	arc	вес
R2-R3	1.60	arc	sec
R1-R3	1.57	arc	seç

3) Diameter of Annulus Centroid

20,6 arc sec

C. A. Zanoni

ZYGO CORPORATION Laurel Brook Road

Middlefield, Connecticut 06455



Date: August 1, 1974

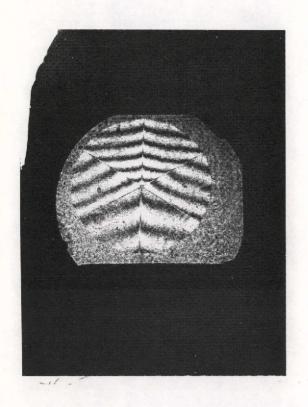
# CERTIFICATE OF COMPLIANCE

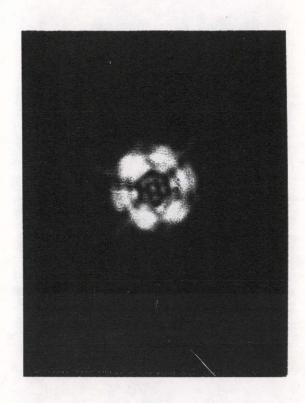
Item: Cu	ibe Corner; LAGEOS - Phase B	
Item I. D.	. No.:	
Contract	No.: T-2954	
Applicabl	e Documents:	
	Drawing No.: 9118-1001 Rev. B (Zygo) Specification: LAG-1 (Bendix)	
Specificat	tions:	
1)	Material (T-19 Suprasil 1 Special)	04
2)	Figure Tolerance R1, R2, R3 ( <sup>λ</sup> /10) R4 (λ/8)	OU
3)	•	04
4)	Wavefront Flatness of Each Sector (See attached Interferogram)	OK
5)	Protective Bevels	OK
6)	Physical Dimensions	OK
7)	Workmanship	OK
This is to all the sp	certify that the cube corner, I.D. Nois is in ecifications and drawings of ghe Bendix purchase	n conformance with order T-2954.
•	C. A. Z	Janon
		() ORPORATION

Middlefield, Connecticut 06455

Laurel Brook Road

# ZYGO





ZYGO CORPORATION
T-G Interferogram
Item No.: #5

Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974

(R1, R2 + R3) Chemically Silvered

ZYGO CORPORATION
Far Field Diffraction Pattern
Item No. #5

Contract No.: T-2954 Cube Corner: LAGEOS

Phase B

Date: August 1, 1974 Scale: 1.47 arc sec/mm

Uncoated Surfaces



Item:	Cul	be Corner; LAGEOS - Phase B		•
Item I	. D.	No.:		
Contra	ict l	No.: T-2954		
Applic	able	Documents:		
		Drawing No.: 9118-1001 Rev. I Specification: LAG-1 (Bendix)	B (Zygo)	
Data:			i .	
	1)	Wavefront Deviation of each Sec (Sector 1 is at one o'clock. Cour		
•		$\lambda = 632.8nm$	Sector 1	6,10 h
			Sector 2	0.20 1
			Sector 3	0.10 \lambda
		,	Sector 4	0.10 1
		·	Sector 5	0.16 h
٠,		•	Sector 6	0.10 X
	2)	Dihedral Angles		
			R1-R2	2,67 arc sec
			R2-R3	1.90 arc sec
			R1-R3	1,80 arc sec
,	3)	Diameter of Annulus Centroid		23,5 arc sec

ZYGO CORPORATION
Laurel Brook Road
Middlefield, Connecticut 06455



### CERTIFICATE OF COMPLIANCE

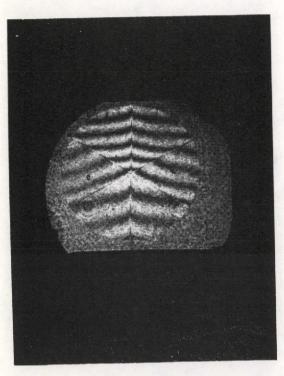
GUATH TOMIE OF COMPLIANCE	•
Item: Cube Corner; LAGEOS - Phase B	•
Item I. D. No.:	
Contract No.: T-2954	
Applicable Documents:	
<ol> <li>Drawing No.: 9118-1001 Rev. B (Zygo)</li> <li>Specification: LAG-1 (Bendix)</li> </ol>	
Specifications:	·
<ol> <li>Material (T-19 Suprasil 1 Special)</li> </ol>	04
2) Figure Tolerance R1, R2, R3 ( <sup>λ</sup> /10) R4 (λ/8)	OU
3) Far Field Diffraction Pattern (See attached photo)	OU
4) Wavefront Flatness of Each Sector (See attached Interferogram)	04
5) Protective Bevels	04
6) Physical Dimensions	OU
7) Workmanship	OK

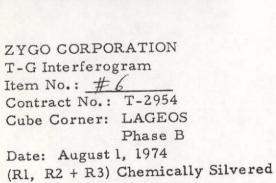
This is to certify that the cube corner, I.D. No. \_\_\_\_\_ is in conformance with all the specifications and drawings of ghe Bendix purchase order T-2954.

C. A. Zanopi

ZYGO CORPORATION Laurel Brook Road Middlefield, Connecticut 06455

# ZYGO







ZYGO CORPORATION
Far Field Diffraction Pattern
Item No. # C
Contract No.: T-2954
Cube Corner: LAGEOS
Phase B
Date: August 1, 1974
Scale: 1.47 arc sec/mm
Uncoated Surfaces



### DATA SHEET

Item: Cube Corner; LAGEOS - Phase B
Item I. D. No.: 6
Contract No.: T-2954
Applicable Documents:
1) Drawing No.: 9118-1001 Rev. B (Zygo)
2) Specification: LAG-1 (Bendix)
Data:

1) Wavefront Deviation of each Sector (Sector 1 is at one o'clock. Gount CW)

$\lambda = 632.8nm$	1	Sector 1	0.10	λ
		Sector 2	0.12	$-\lambda$
	•.	Sector 3	.0.10	_ <sub>λ</sub>
	· •	Sector 4	0.10	<b>−</b> <sub>λ</sub>
		Sector 5	0.10	_λ
	-	Sector 6 .	0.15	_ <sub>\lambda</sub>

2) Dihedral Angles

R1-R2	1,30	arc	sec
R2-R3	1,00	arc	sec
R1-R3	1.16		
		•	

3) Diameter of Annulus Centroid

18.4 arc sec

C. A. Zanghi

ZYGO CORPORATION Laurel Brook Road Middlefield, Connecticut 06455

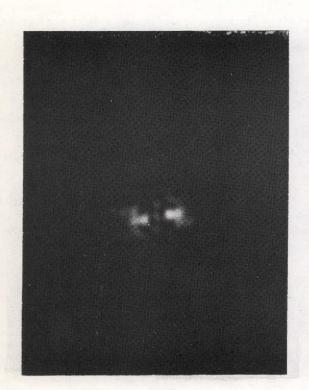
### APPENDIX U

LAGEOS Thermal/Optical Test Data -

Far-Field Diffraction Pattern Photographs

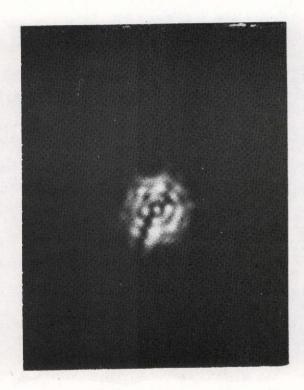
- NOTE:
- a) This data is identified by Test Number and Photograph Number; test conditions for each photograph are identified in Appendix R.
- b) The FFDI scale factor is 1.47 arc sec/mm. The centimeter scale provided on each page must be used for any length measurement.

cm | 1 2 3

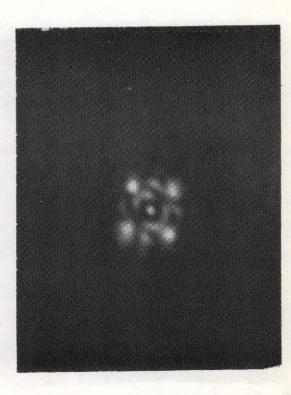


Test No. /
Retro: CALIB.

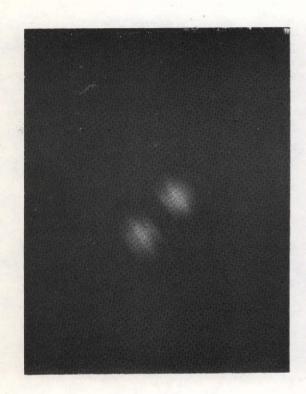
Photo No. /
Exposure Time: '/250 SEC



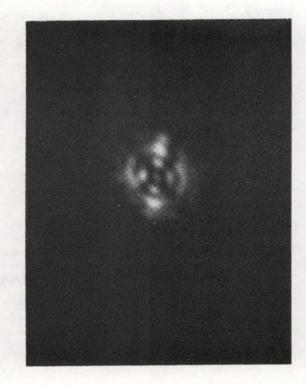
Test No. /
Retro: A
Photo No. 2
Exposure Time: 1/125 566



Test No.	1	Langue Cale	
Retro:	A		
Photo No.	3		
Exposure	Time:	1/125	SEC



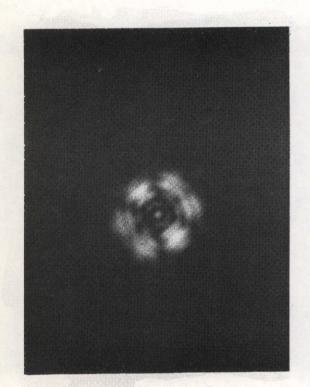
Test No. /
Retro: A
Photo No. 4
Exposure Time: 1/8 SEC



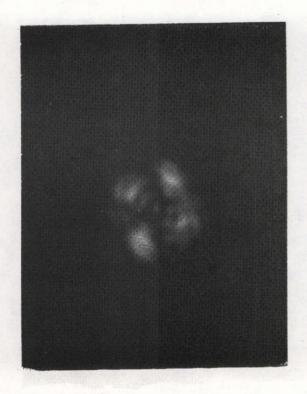
Test No. /
Retro: A
Photo No. 5
Exposure Time: 1/125 SEC



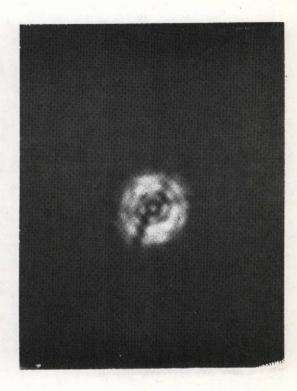
Test No. /
Retro: A
Photo No. 6
Exposure Time: '/125 Sec



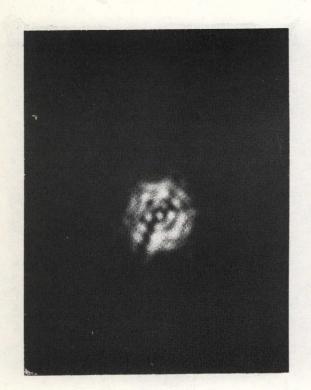
Test No. /
Retro: 8
Photo No. 7
Exposure Time: 1/125 SEC



Test No. /
Retro: B
Photo No. 8
Exposure Time: 1/30 sec



Test No.	1	
Retro:	С	
Photo No.	9	
Exposure	Time:	1/125 565

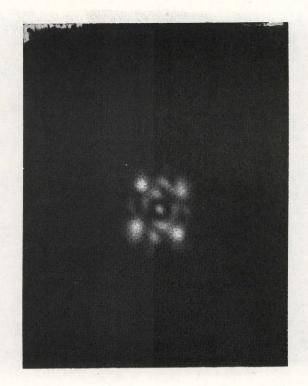


Test No. 2

Retro: A

Photo No. 10

Exposure Time: 1/125 SEC

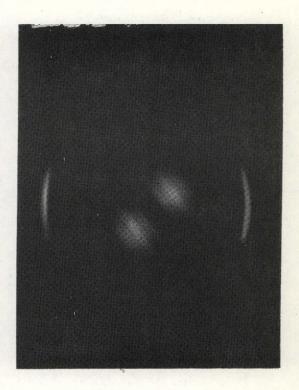


Test No. 2

Retro: A

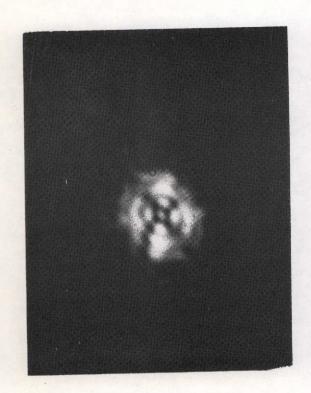
Photo No. //

Exposure Time: ///25 56c



Test No.		2		
Retro:		A		
Photo No.		12		
Exposure '	Time:	1/8	SEC	
Exposure	lime:	/8	365	

 $\mathsf{cm} \begin{bmatrix} \mathsf{III}   \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIIIIII \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIIIIII \mathsf{IIIII} \mathsf{IIIII} \mathsf{IIIIIII \mathsf{$ 

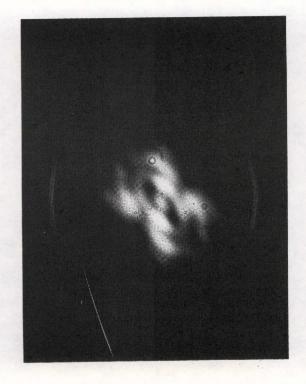


Test No. 2

Retro: A

Photo No. 13

Exposure Time: 1/60 SEC

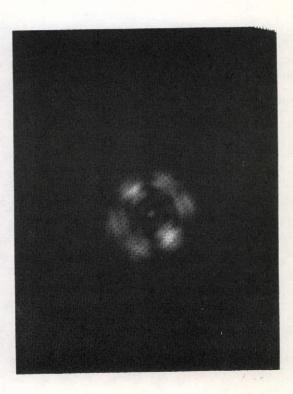


Test No. 2

Retro: A

Photo No. 14

Exposure Time: 1/15 SEC

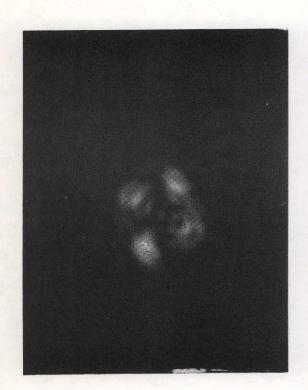


Test No.	2
Retro:	8
Photo No.	15
Exposure Time	: 1/125 SEE

C-3

LAGEOS THERMAL/OPTICAL TESTS FAR-FIELD DIFFRACTION PATTERN PHOTOGRAPHIC OUTPUT - FFDI

 $\begin{smallmatrix} \mathsf{cm} \\ \mathsf{l} \end{smallmatrix} [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} (1) \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \\ \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ] [ \begin{matrix} \mathsf{l} \end{matrix} ]$ 

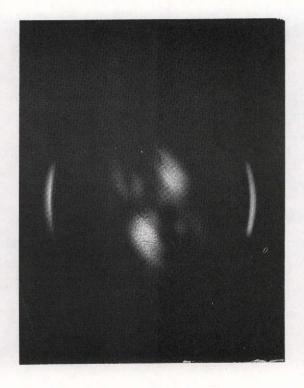


Test No. 2

Retro: B

Photo No. 16

Exposure Time: 1/60 SEC

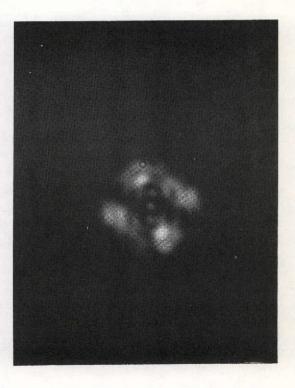


Test No. 2

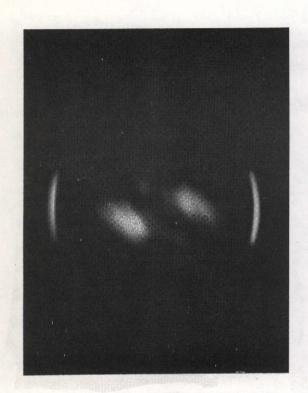
Retro: 8

Photo No. 17

Exposure Time: 1/4 SEC



Test No.	2	
Retro:	8	
Photo No.		18
Exposure	Time:	160 SEC

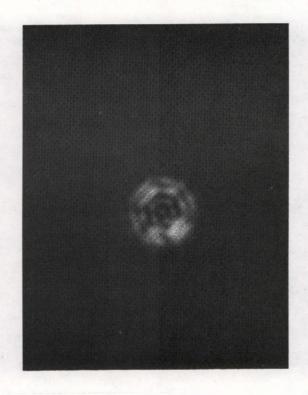


Test No. 2

Retro: 8

Photo No. 19

Exposure Time: 1/4 SEC



Test No. 2

Retro: C

Photo No. Zo

Exposure Time: 1/125 SEC



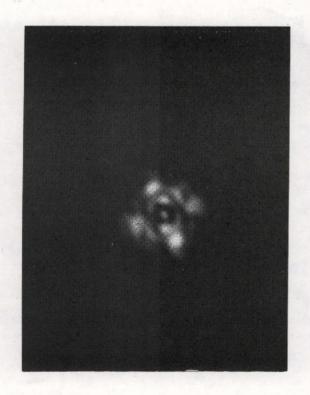
 Test No.
 2

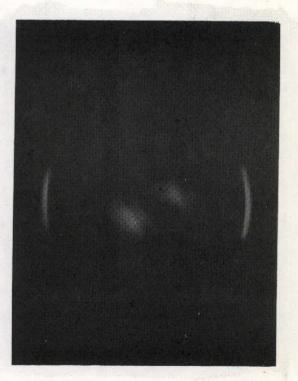
 Retro:
 C

 Photo No.
 21

 Exposure Time:
 1/30 5EC







Retro: C
Photo No. 22
Exposure Time: 1/4 SEC

Test No. 2

Retro: C

Photo No. 23

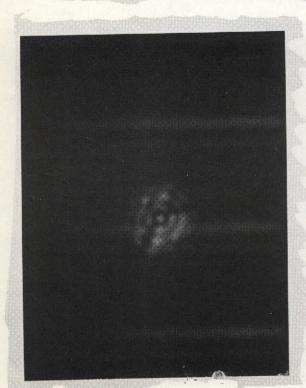
Exposure Time: 1/60 SEC

Test No. 2

Retro: C

Photo No. 24

Exposure Time: 1/8 sec

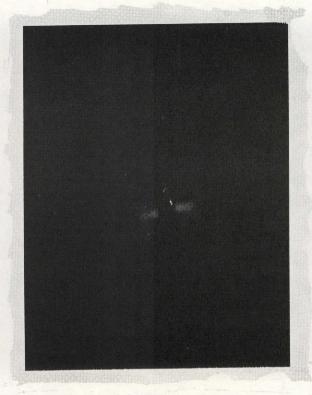


Test No. 15

Retro: A

Photo No. 25

Exposure Time: 1/125 SEC



Test No. 16
Retro: CALIB.
Photo No. 26
Exposure Time: 1/500 SEC

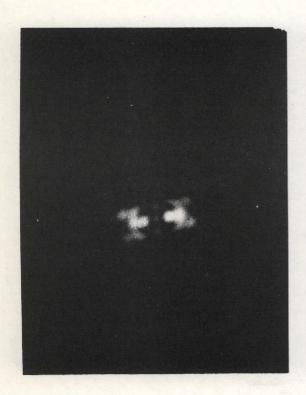


Test No. 16

Retro: A

Photo No. 27

Exposure Time: 1/125 550

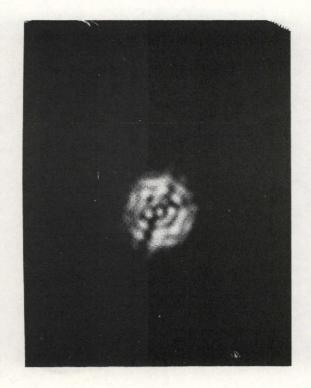


Test No. 16

Retro: CALIB.

Photo No. 28

Exposure Time: 1/500 SEC

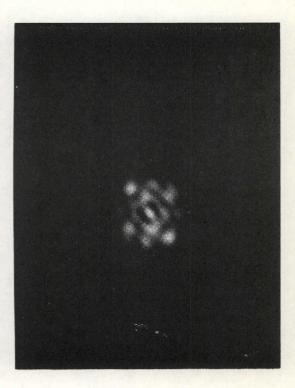


Test No. 16

Retro: A

Photo No. 29

Exposure Time: 1/250 SEC

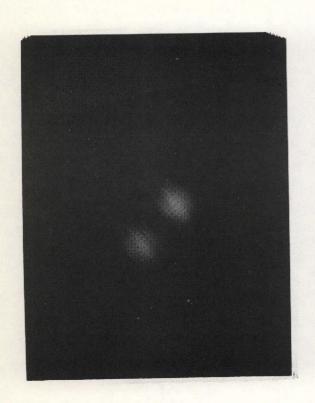


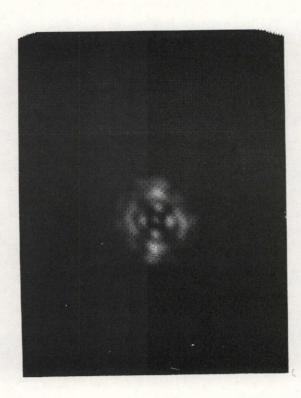
Test No. 16

Retro: A

Photo No. 30

Exposure Time: 1/250 SEC







Test No	16
Retro:	A
Photo No.	3/
Exposure	Time: 1/15 SEC

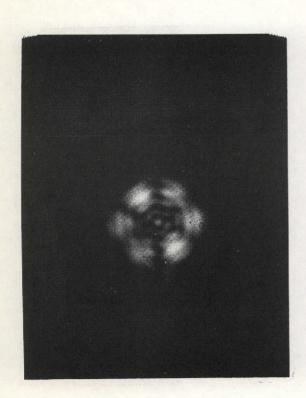
 Test No.
 16

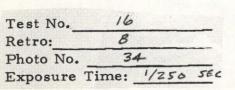
 Retro:
 A

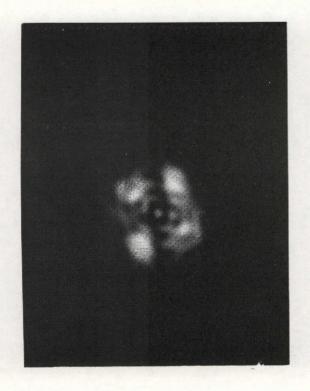
 Photo No.
 32

 Exposure Time:
 1/250 SEC

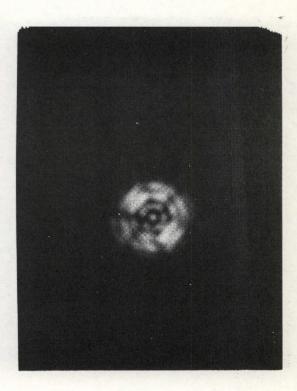
Test No. 16
Retro: A
Photo No. 33
Exposure Time: 1/60 5EC







Test No.	16
Retro:	В
Photo No.	35
Exposure T	ime: 1/125 5 € c

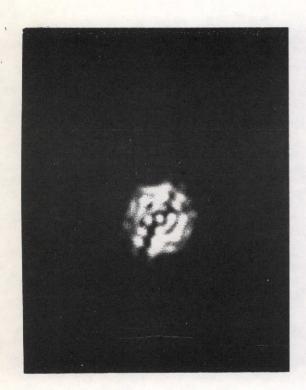


 Test No.
 16

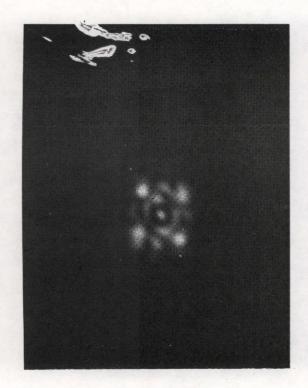
 Retro:
 C

 Photo No.
 36

 Exposure Time:
 1/250 SEC



Test No. 17
Retro: A
Photo No. 37
Exposure Time: 1/250 SEE

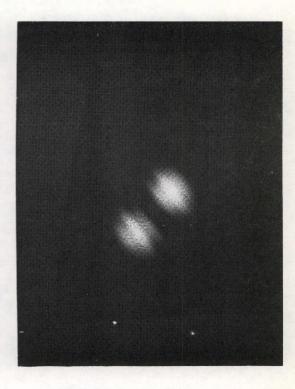


 Test No.
 /7

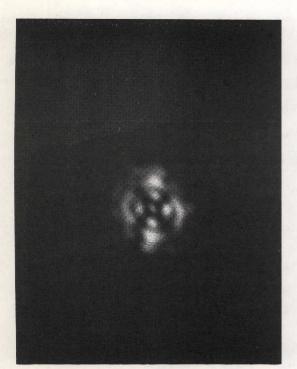
 Retro:
 A

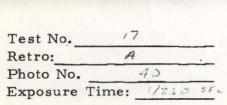
 Photo No.
 38

 Exposure Time:
 1/250 566



Test No. 77
Retro: A
Photo No. 39
Exposure Time: 1/8 SEC





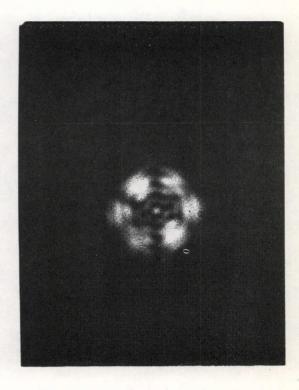


 Test No.
 17

 Retro:
 A

 Photo No.
 41

 Exposure Time:
 1/60 SEC

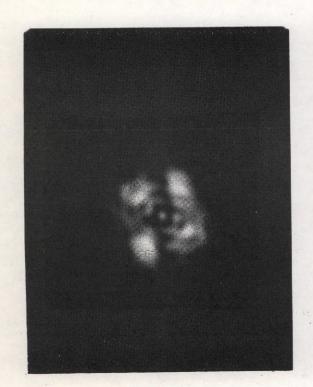


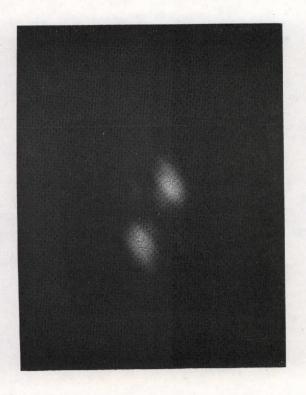
 Test No.
 /7

 Retro:
 8

 Photo No.
 42

 Exposure Time:
 1/250566







Test No. 17
Retro: 8
Photo No. 43
Exposure Time: 1/125 SEC

Test No. 17
Retro: 8
Photo No. 44
Exposure Time: 1/15 566

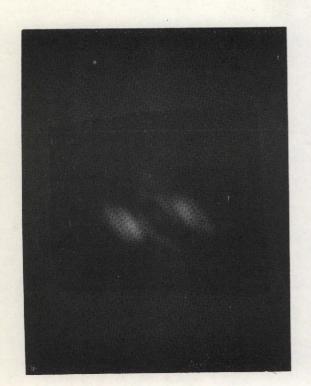
 Test No.
 /7

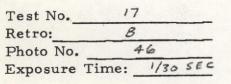
 Retro:
 8

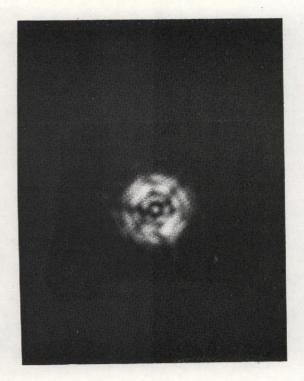
 Photo No.
 45

 Exposure Time:
 1/250 SEC

m 1 2 3





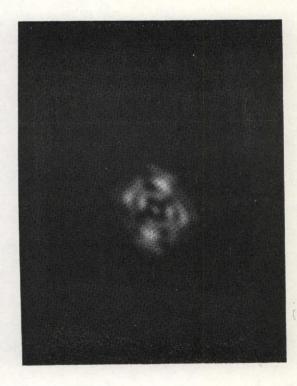


Test No. /7

Retro: C

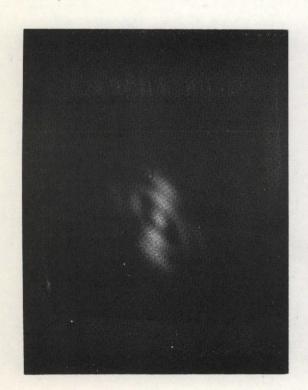
Photo No. 47

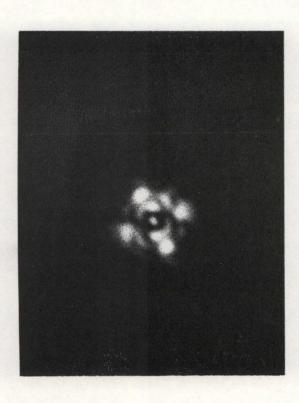
Exposure Time: '/zsasec

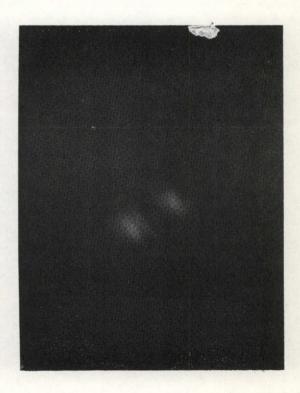


Retro: C	Test No.	17	
10	Retro:	C	
Photo No. 48	Photo No.	4	18
Exposure Time: 1/250 56	Exposure	Time:	1/250 586

# 







Test No. 17
Retro: C
Photo No. 49
Exposure Time: 1/30 SEC

Test No. /7

Retro: C

Photo No. 50

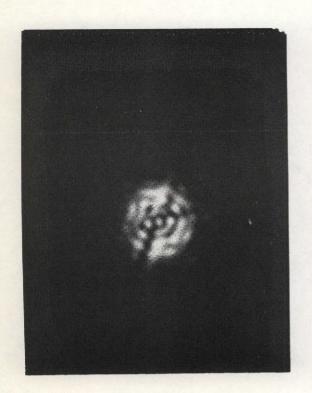
Exposure Time: 1/250 556

 Test No.
 /7

 Retro:
 C

 Photo No.
 5/

 Exposure Time:
 1/30 5EC

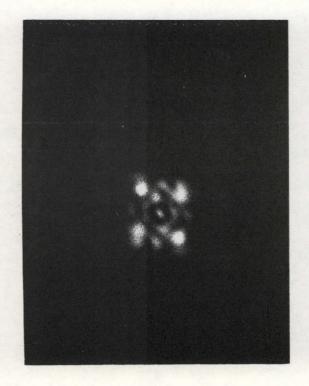


Test No. 7

Retro: A

Photo No. 52

Exposure Time: 1/250 SEC

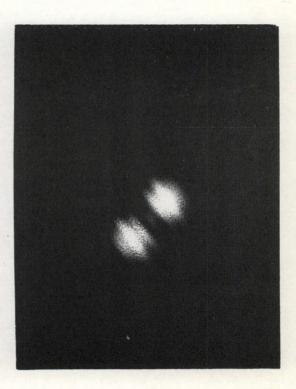


 Test No.
 7

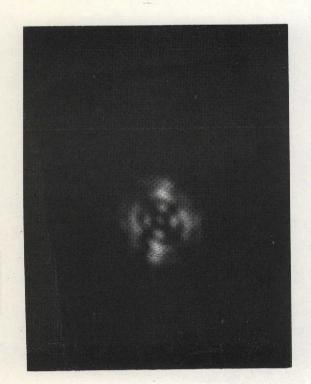
 Retro:
 A

 Photo No.
 53

 Exposure Time:
 1/250



Test No.	7
Retro:	A
Photo No.	54
Exposure	Time: 1/8 SEC

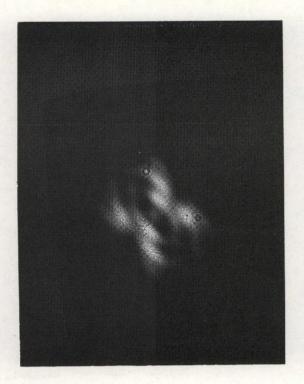


 Test No.
 7

 Retro:
 A

 Photo No.
 55

 Exposure Time:
 1/250 5EC

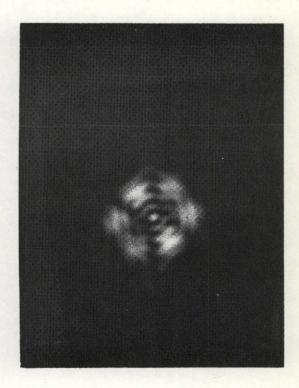


 Test No.
 7

 Retro:
 A

 Photo No.
 56

 Exposure Time:
 1/60 sec

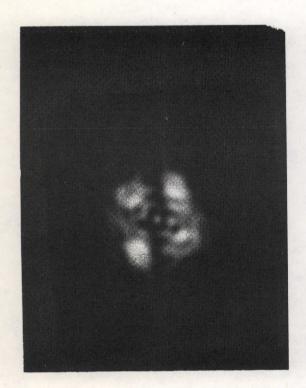


 Test No.
 7

 Retro:
 8

 Photo No.
 57

 Exposure Time:
 1/250 SEC

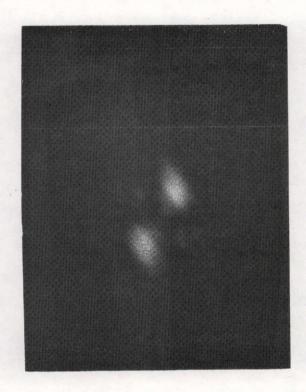


 Test No.
 7

 Retro:
 8

 Photo No.
 58

 Exposure Time:
 1/125 SEC

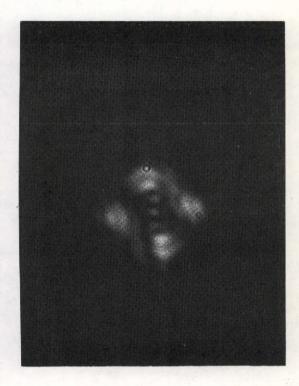


Test No.

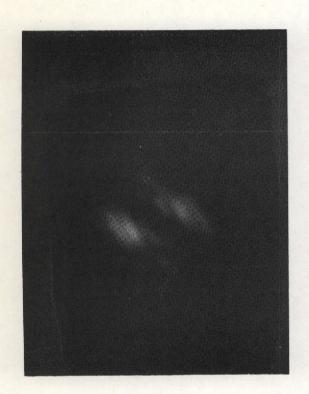
Retro:

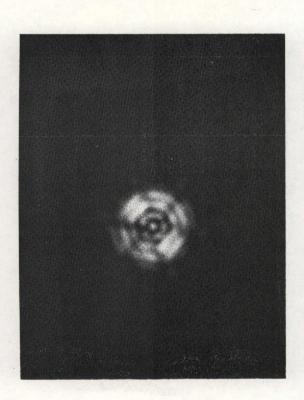
Photo No.

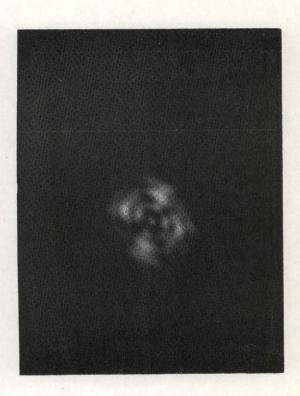
Exposure Time: 1/15 SEC



Test No.	7		
Retro:	8		
Photo No.		60	
Exposure	Time:	1/250	SEC
-	_		







Test No. 7
Retro: 8
Photo No. 6/
Exposure Time: '/30 560

Test No. 7

Retro: C

Photo No. 62

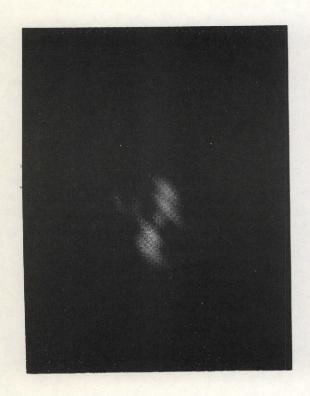
Exposure Time: 1/250 SEC

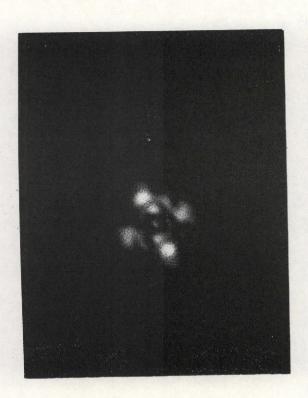
Test No. 7

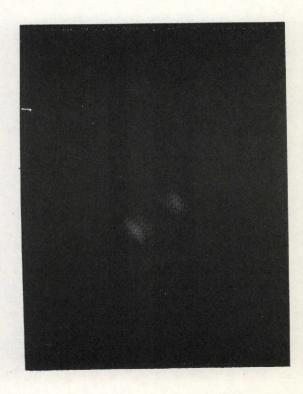
Retro: C

Photo No. 63

Exposure Time: 1/250566







Test No. 7.

Retro: C

Photo No. 64

Exposure Time: 1/30 SEC

 Test No.
 7

 Retro:
 C

 Photo No.
 65

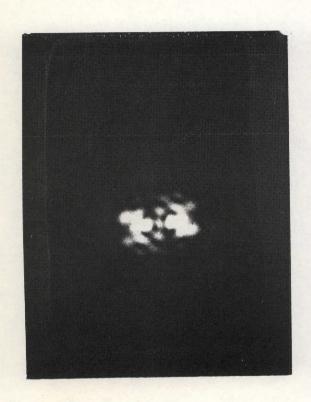
 Exposure Time:
 1/250 SEC

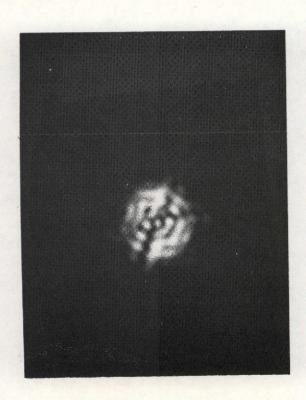
 Test No.
 7

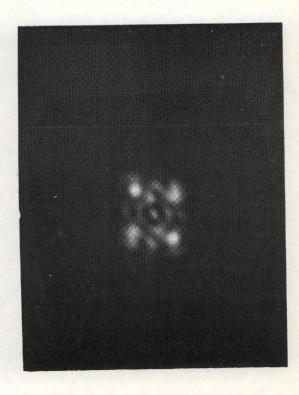
 Retro:
 C

 Photo No.
 66

 Exposure Time:
 1/30 5EC







Test No. 9
Retro: CALIB.
Photo No. 67
Exposure Time: 1/250 SEC

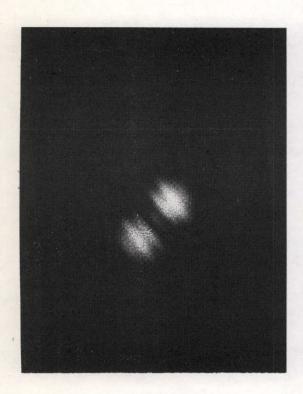
 Test No.
 9

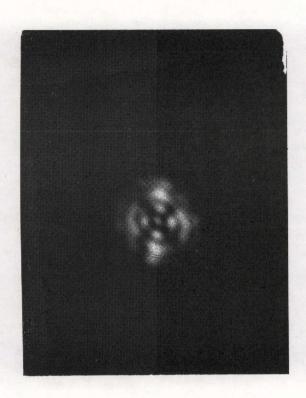
 Retro:
 A

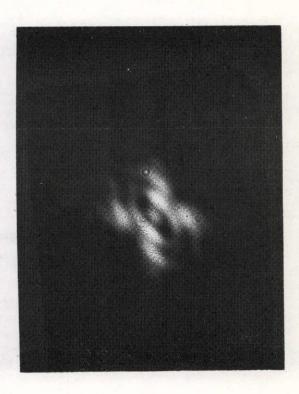
 Photo No.
 68

 Exposure Time:
 1/250 566

Test No. 9
Retro: A
Photo No. 69
Exposure Time: 1/250 SEC







 Test No.
 9

 Retro:
 A

 Photo No.
 70

 Exposure Time:
 1/8 5EC

 Test No.
 9

 Retro:
 A

 Photo No.
 7/

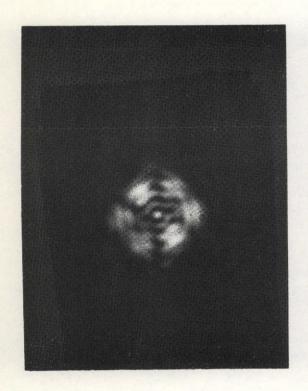
 Exposure Time:
 1/250 5EC

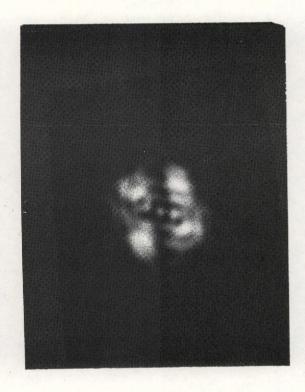
 Test No.
 9

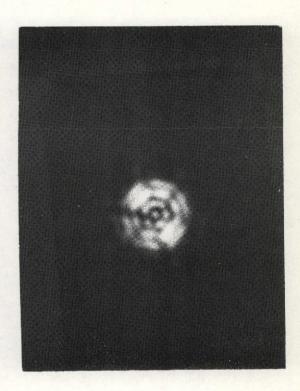
 Retro:
 A

 Photo No.
 72

 Exposure Time:
 1/60 SEC







 Test No.
 9

 Retro:
 8

 Photo No.
 73

 Exposure Time:
 1/250 560

 Test No.
 9

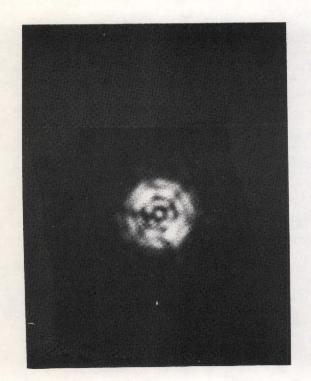
 Retro:
 8

 Photo No.
 74

 Exposure Time:
 1/125 566

Test No.	9	
Retro:	C	
Photo No.		75
Exposure	Time:	1/250 566

cm | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111

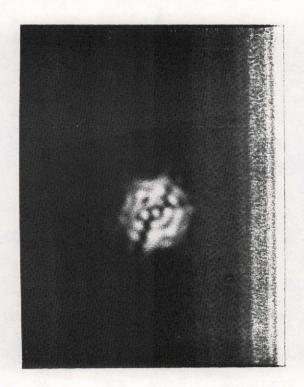


Test No. 8

Retro: C

Photo No. 76

Exposure Time: 1/250 SEE

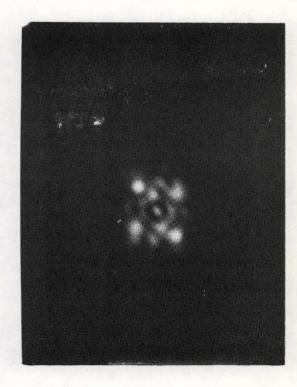


 Test No.
 8

 Retro:
 A

 Photo No.
 77

 Exposure Time:
 1/250 566

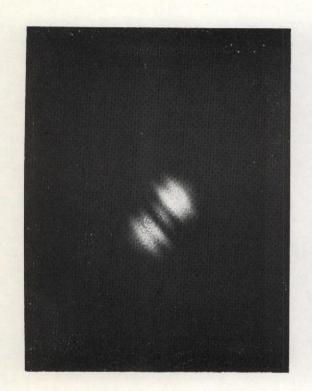


 Test No.
 8

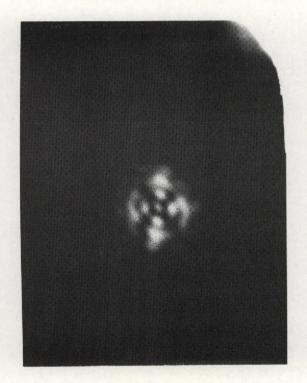
 Retro:
 A

 Photo No.
 78

 Exposure Time:
 '/250 5EC



Test No. 8
Retro: A
Photo No. 79
Exposure Time: 1/8 SEC

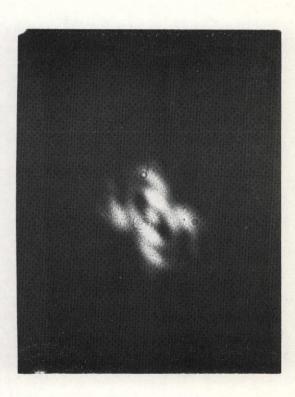


 Test No.
 8

 Retro:
 A

 Photo No.
 80

 Exposure Time:
 1/250 56c



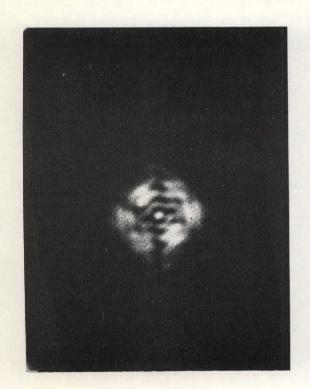
 Test No.
 8

 Retro:
 A

 Photo No.
 8/

 Exposure Time:
 1/60 SEC

# 

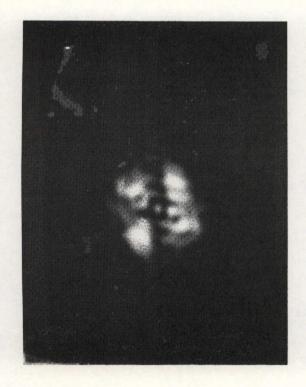


Test No. 8

Retro: 8

Photo No. 82

Exposure Time: 1/250 \$66

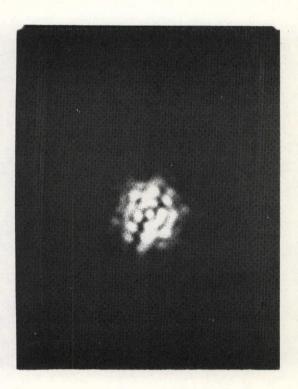


 Test No.
 8

 Retro:
 8

 Photo No.
 83

 Exposure Time:
 1/125 560

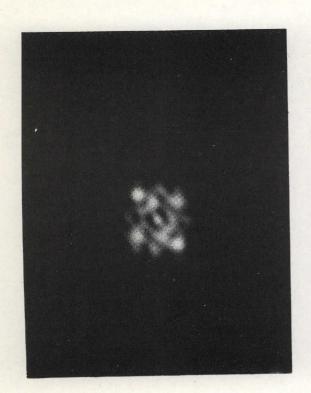


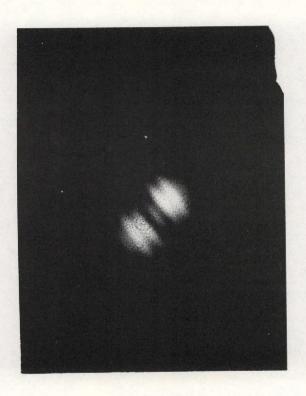
 Test No.
 4

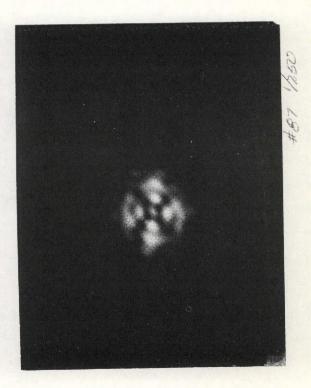
 Retro:
 A

 Photo No.
 84

 Exposure Time:
 1/250 SEC







Test No. 4

Retro: A

Photo No. 85

Exposure Time: '/250 SEC

 Test No.
 4

 Retro:
 A

 Photo No.
 86

 Exposure Time:
 1/8 566

 Test No.
 4

 Retro:
 A

 Photo No.
 87

 Exposure Time:
 1/250 56c



Test No. 4

Retro: A

Photo No. 88

Exposure Time: 1/60 SEC

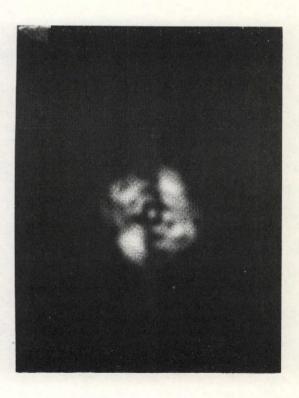


 Test No.
 4

 Retro:
 8

 Photo No.
 89

 Exposure Time:
 1/250 SEC

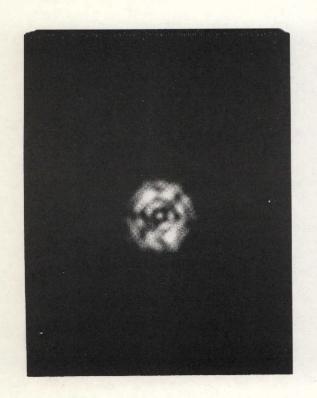


 Test No.
 4

 Retro:
 8

 Photo No.
 90

 Exposure Time:
 1/125

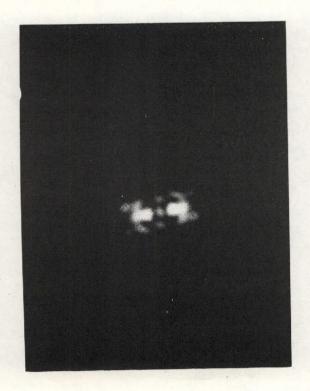


Test No. 4

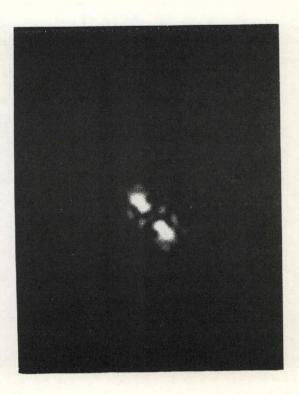
Retro: C

Photo No. 91

Exposure Time: 1/250 556

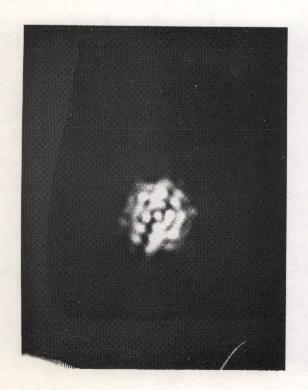


Test No.	4	
Retro:	CALIB.	
Photo No.	92	
Exposure	Time: 1/50	0 560



Test No.	6	
Retro:	CALIB.	
Photo No.	93	
Exposure		

# 

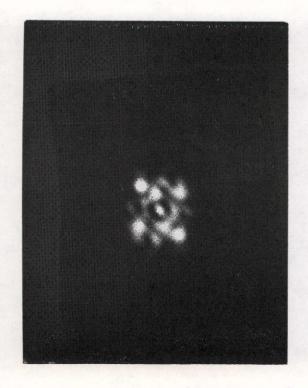


 Test No.
 6

 Retro:
 A

 Photo No.
 94

 Exposure Time:
 1/250 560

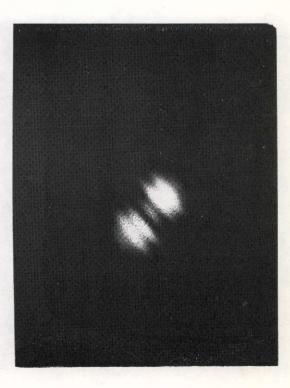


Test No. 6

Retro: A

Photo No. 95

Exposure Time: 1/250 566



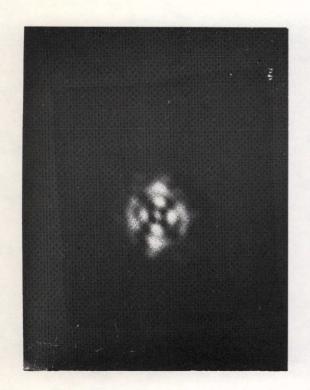
Test No. 6

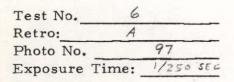
Retro: A

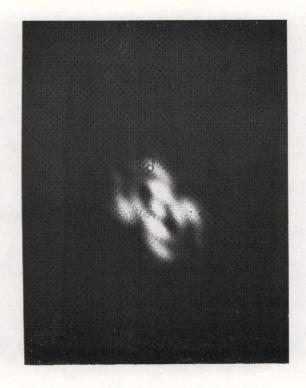
Photo No. 96

Exposure Time: 1/8 SFC

# $\mathfrak{e}_{\mathsf{m}}$





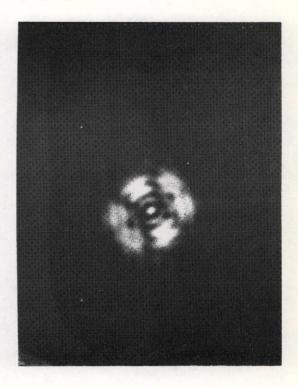


 Test No.
 6

 Retro:
 A

 Photo No.
 98

 Exposure Time:
 1/60 5 5 6



 Test No.
 6

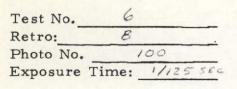
 Retro:
 8

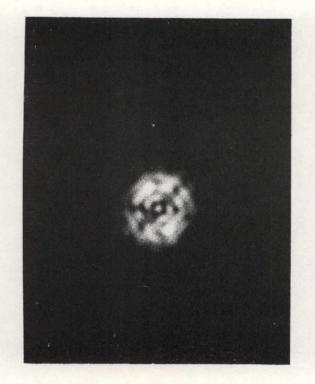
 Photo No.
 99

 Exposure Time:
 1/250 566

cm | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 1





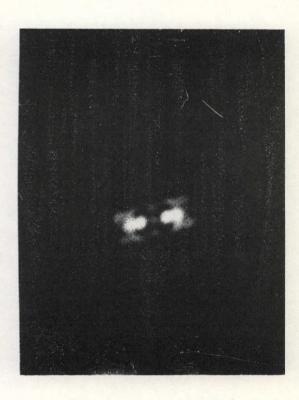


Test No. 6

Retro: 6

Photo No. 101

Exposure Time: 1/250 SEE



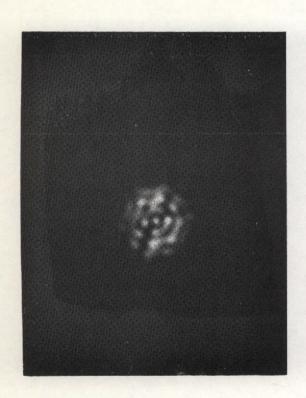
 Test No.
 3

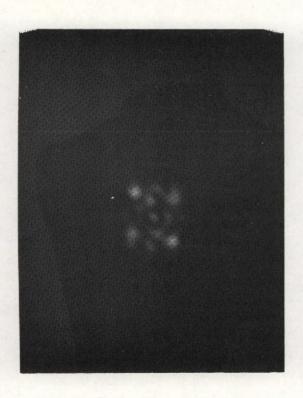
 Retro:
 CALIB.

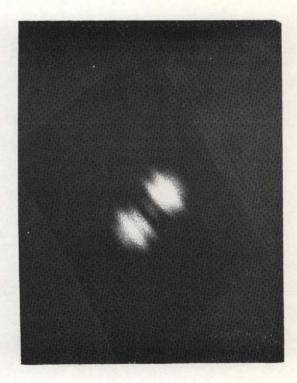
 Photo No.
 10Z

 Exposure Time:
 1/500 SEC

 $c_{\mathsf{m}}$   $\begin{vmatrix} 1 & 1 & 2 & 3 \\ 1 & 2 & 3 \end{vmatrix}$ 







Test No. 3

Retro: A

Photo No. 103

Exposure Time: 1/500 SEC

 Test No.
 3

 Retro:
 A

 Photo No.
 /04

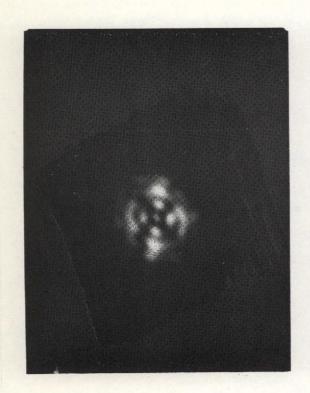
 Exposure Time:
 1/500 566

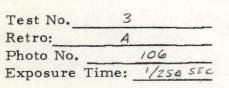
 Test No.
 3

 Retro:
 A

 Photo No.
 105

 Exposure Time:
 1/8 5 6 6





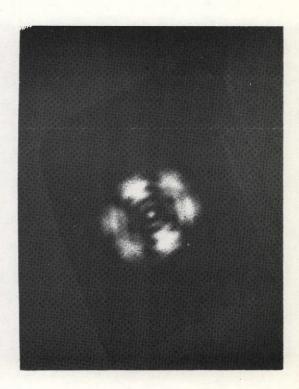


 Test No.
 3

 Retro:
 A

 Photo No.
 107

 Exposure Time:
 1/60 SEC



 Test No.
 3

 Retro:
 8

 Photo No.
 108

 Exposure Time:
 1/250 566

# 

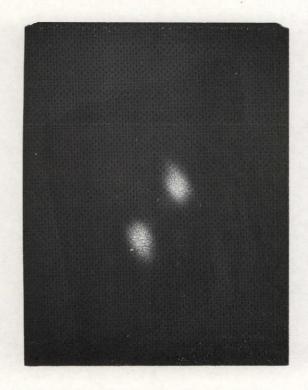


 Test No.
 3

 Retro:
 8

 Photo No.
 109

 Exposure Time:
 1/125 SEC

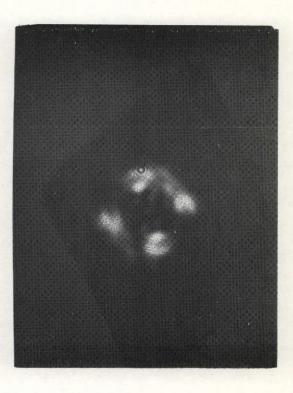


Test No. 3

Retro: 8

Photo No. 1/0

Exposure Time: 1/15  $5 \in \mathbb{C}$ 



 Test No.
 3

 Retro:
 8

 Photo No.
 ///

 Exposure Time:
 1/250 566

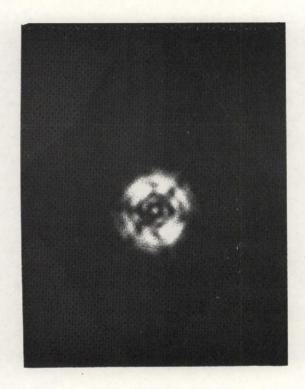


Test No. 3

Retro: 8

Photo No. 1/2

Exposure Time: 1/30 SEC



 Test No.
 3

 Retro:
 C

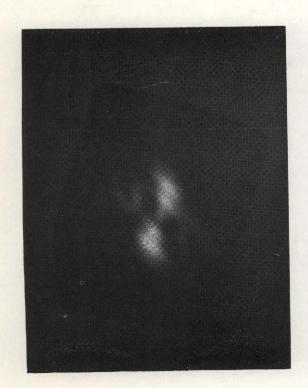
 Photo No.
 //3

 Exposure Time:
 1/250 SEC



	3
(	
	114
Time:	1/250 SKE
	Time:

# 

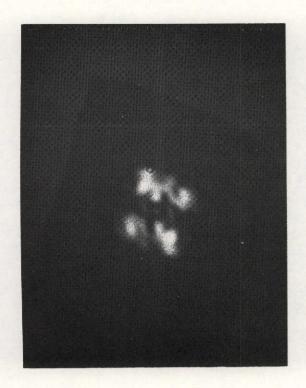


Test No. 3

Retro: C

Photo No. //5

Exposure Time: 1/30 Sec

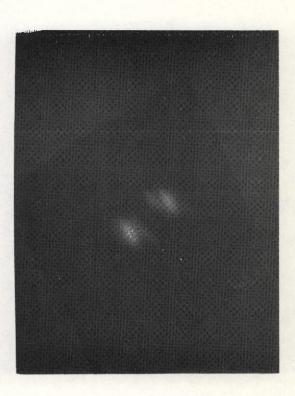


 Test No.
 3

 Retro:
 C

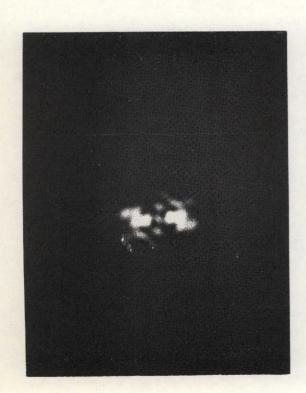
 Photo No.
 1/6

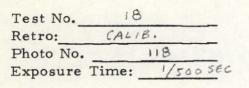
 Exposure Time:
 1/250 566

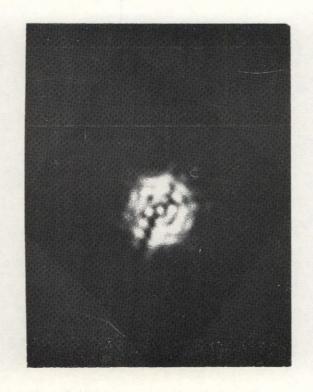


Test No.	3
Retro:	C
Photo No.	117
Exposure Time	: 1/30 SEC.

 $_{\text{cm}}$ 





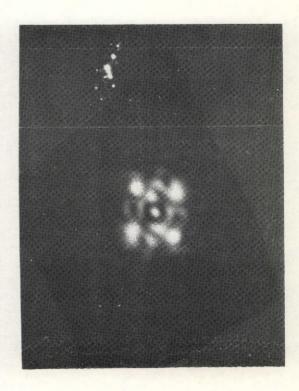


 Test No.
 18

 Retro:
 A

 Photo No.
 119

 Exposure Time:
 1/250 SEC

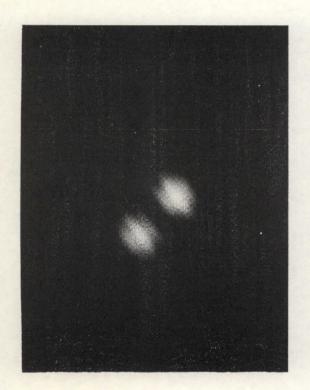


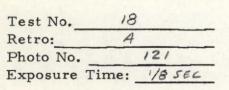
Test No. 18

Retro: A

Photo No. 120

Exposure Time: √250 S€5







 Test No.
 18

 Retro:
 A

 Photo No.
 122

 Exposure Time:
 1/250 560

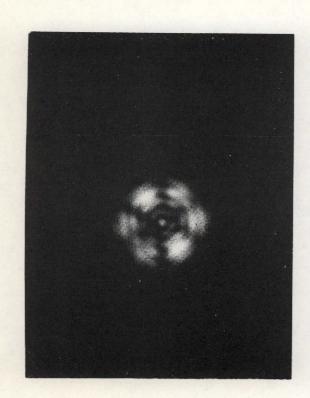


 Test No.
 18

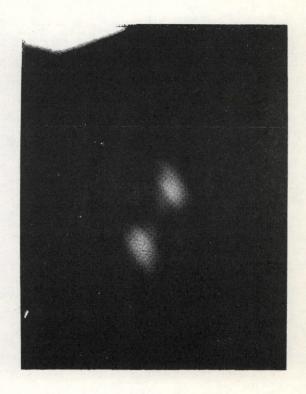
 Retro:
 A

 Photo No.
 123

 Exposure Time:
 1/60 560







 Test No.
 18

 Retro:
 8

 Photo No.
 124

 Exposure Time:
 1/250 56 c

Test No. 18

Retro: 8

Photo No. 125

Exposure Time: 1/125 SEC

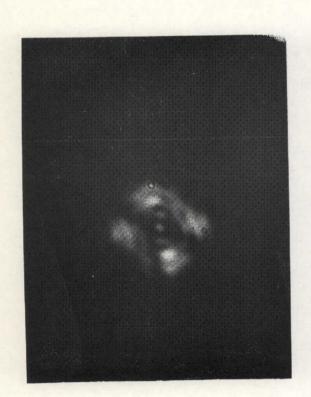
 Test No.
 18

 Retro:
 8

 Photo No.
 126

 Exposure Time:
 1/15 566

m | 1 2 3

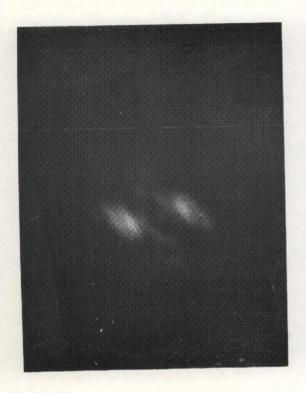


 Test No.
 18

 Retro:
 8

 Photo No.
 127

 Exposure Time:
 1/250 580

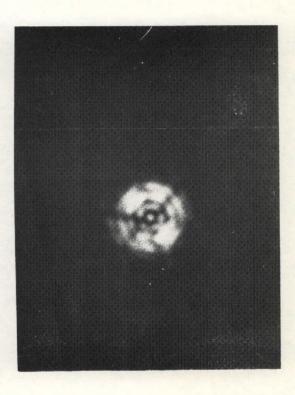


 Test No.
 /8

 Retro:
 8

 Photo No.
 /28

 Exposure Time:
 1/30 550



Test No. /8

Retro: C

Photo No. /29

Exposure Time: 1/250 SFC

cm | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 1

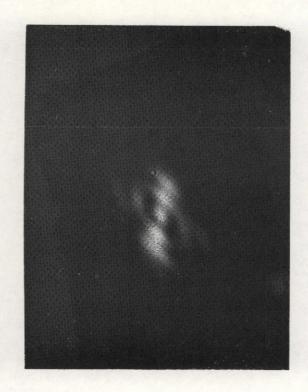


 Test No.
 18

 Retro:
 C

 Photo No.
 130

 Exposure Time:
 1/250 56c



 Test No.
 /8

 Retro:
 C

 Photo No.
 /3/

 Exposure Time:
 1/30 50c



Test No. /8

Retro: C

Photo No. /3Z

Exposure Time: 1/250 5/4

cm | !!!!| !!!| 1 2 3

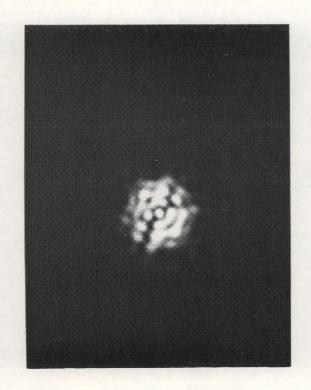


Test No. 18

Retro: C

Photo No. 133

Exposure Time: 1/30 SEC

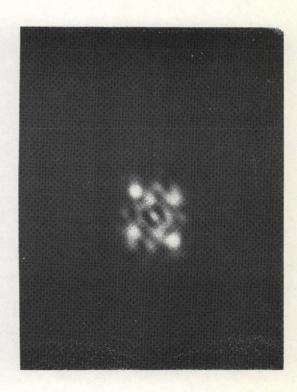


 Test No.
 5

 Retro:
 A

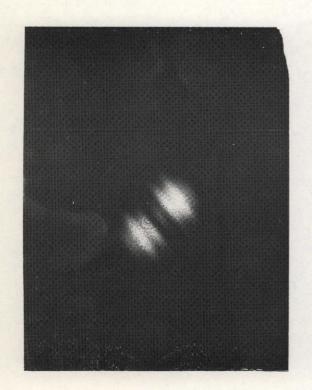
 Photo No.
 /34

 Exposure Time:
 1/25556



Test No.	5	
Retro:	A	
Photo No.	135	
Exposure Time:	1/250 865	

## cm | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 1

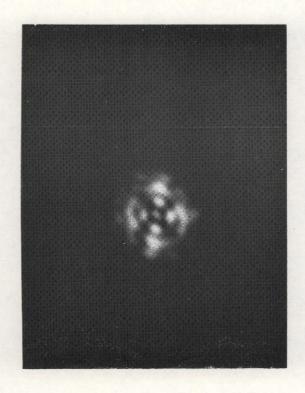


Test No. 5

Retro: A

Photo No. 136

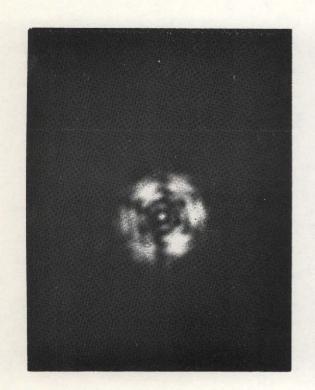
Exposure Time: 1/8 566



Test No. 5
Retro: A
Photo No. /37
Exposure Time: 1/250 SEC



Test No. 5
Retro: A
Photo No. 738
Exposure Time: 1/60 586



 Test No.
 5

 Retro:
 B

 Photo No.
 /39

 Exposure Time:
 1/250 560

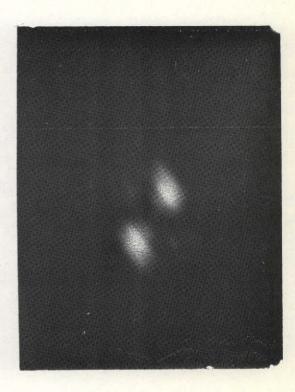


 Test No.
 5

 Retro:
 8

 Photo No.
 140

 Exposure Time:
 1/125 \$16



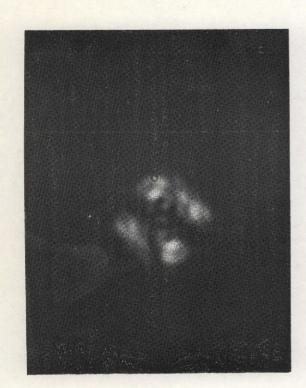
 Test No.
 5

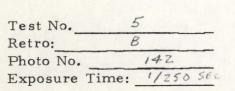
 Retro:
 8

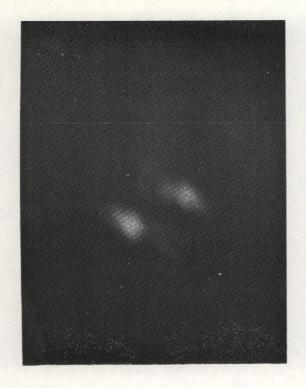
 Photo No.
 141

 Exposure Time:
 1/15 560

 $c_{m}$   $\begin{vmatrix} 1 & 2 & 3 \end{vmatrix}$ 





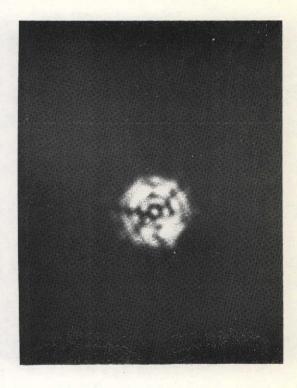


 Test No.
 5

 Retro:
 8

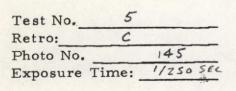
 Photo No.
 143

 Exposure Time:
 1/3 o SEC



Test No.	5	1	
Retro:	C		
Photo No.		144	D-050
Exposure	Time:	1/250	SEC





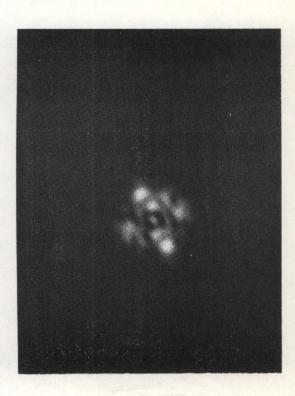


Test No. 5

Retro: C

Photo No. 146

Exposure Time: 1/30 SEC

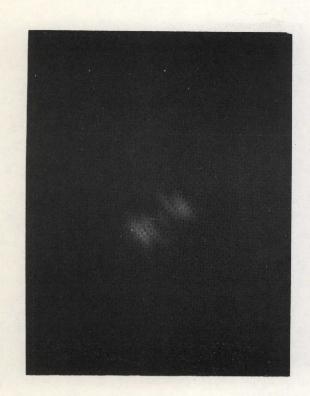


 Test No.
 5

 Retro:
 C

 Photo No.
 147

 Exposure Time:
 1/250 5EC

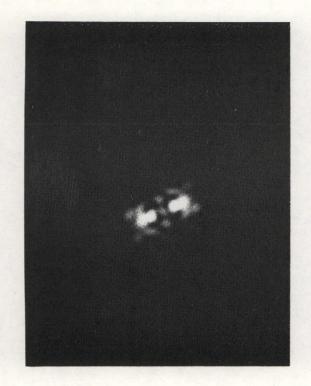


Test No. 5

Retro: C

Photo No. 148

Exposure Time: 1/30 SEC

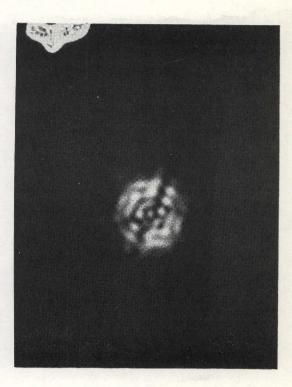


Test No. 10

Retro: CALIB.

Photo No. 149

Exposure Time: 1/500 SEC



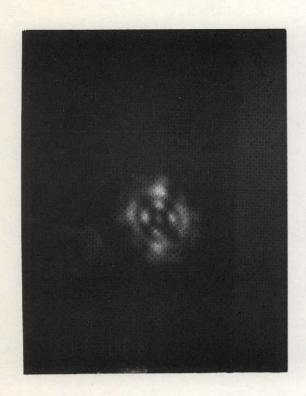
 Test No.
 /O

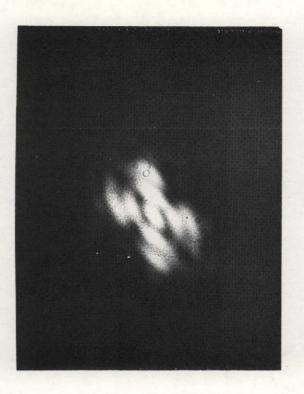
 Retro:
 D

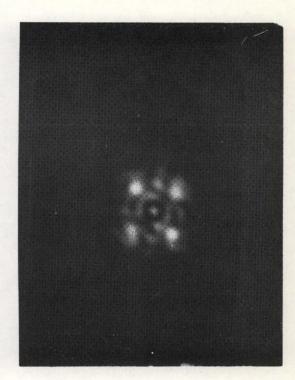
 Photo No.
 /50

 Exposure Time:
 '/zso sec

cm | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 1







 Test No.
 10

 Retro:
 D

 Photo No.
 151

 Exposure Time:
 1/250 56c

 Test No.
 10

 Retro:
 D

 Photo No.
 152

 Exposure Time:
 1/3 à 566

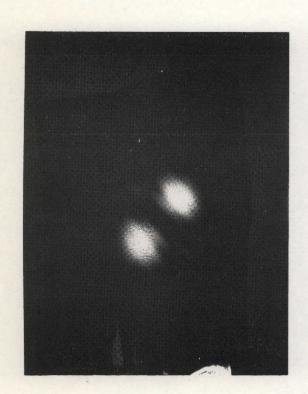
 Test No.
 10

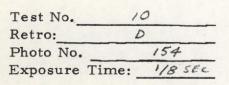
 Retro:
 D

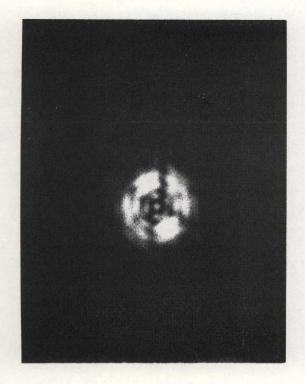
 Photo No.
 1/53

 Exposure Time:
 1/250 566

# 





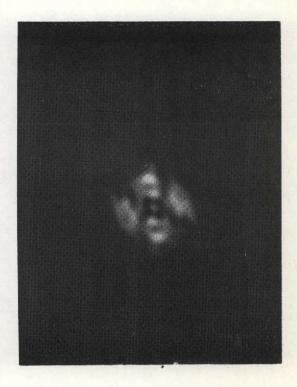


 Test No.
 10

 Retro:
 E

 Photo No.
 155

 Exposure Time:
 1/250 566

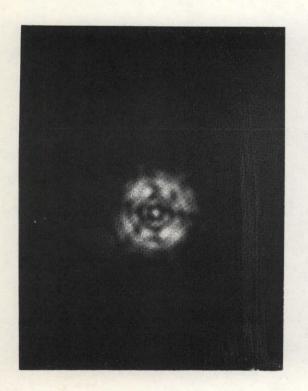


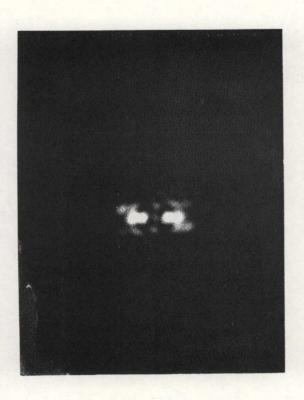
 Test No.
 10

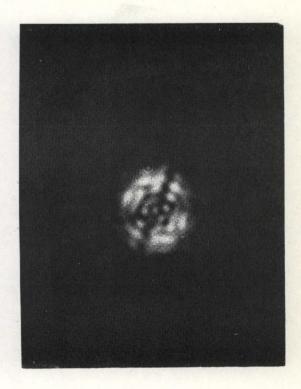
 Retro:
 E

 Photo No.
 156

 Exposure Time:
 1/250 SEC







 Test No.
 //

 Retro:
 CALIB.

 Photo No.
 /58

 Exposure Time:
 '/500 SEC

Test No.	11
Retro:	D
Photo No.	159
Exposure Time:	1/250 SEC

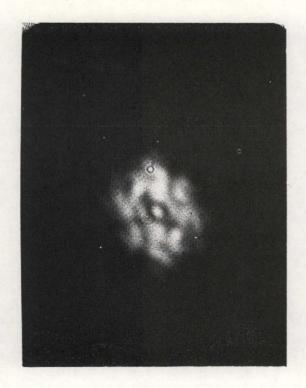


Test No. //

Retro: D

Photo No. /60

Exposure Time: 1/250 SEC

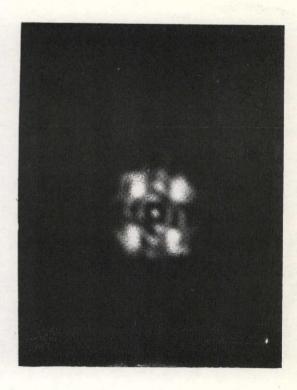


 Test No.
 //

 Retro:
 D

 Photo No.
 /6/

 Exposure Time:
 //60 SEC

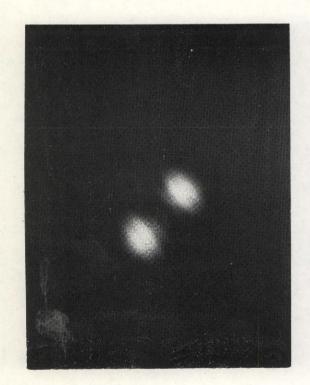


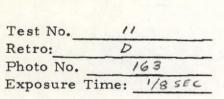
 Test No.
 //

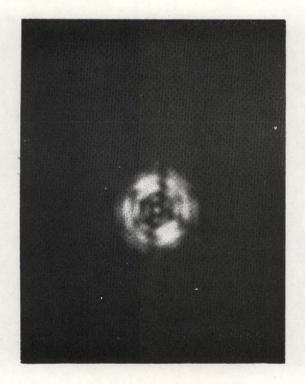
 Retro:
 D

 Photo No.
 162

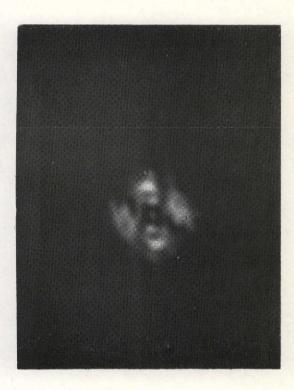
 Exposure Time:
 1/125 SEC



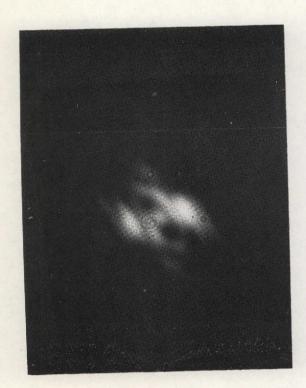


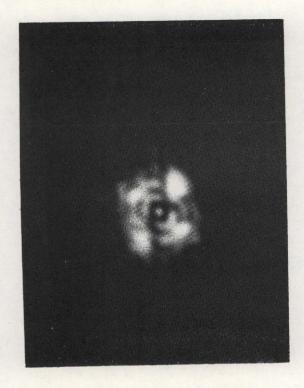


Test No.	11
Retro:	E
Photo No.	164
Exposure Time:	1/250 560



Test No.	11	
Retro:	E	
Photo No.	165	
Exposure	Time: 1/250 56 C	



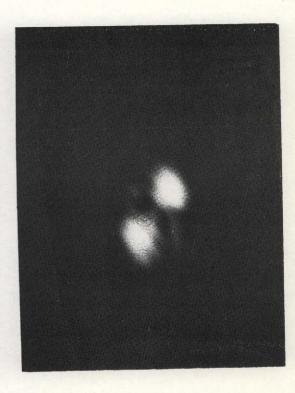


 Test No.
 //

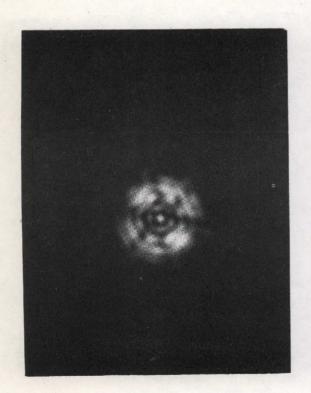
 Retro:
 E

 Photo No.
 167

 Exposure Time:
 1/125 5EC



cm | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111



Test No. //
Retro: F
Photo No. /69
Exposure Time: 1/250 SEC

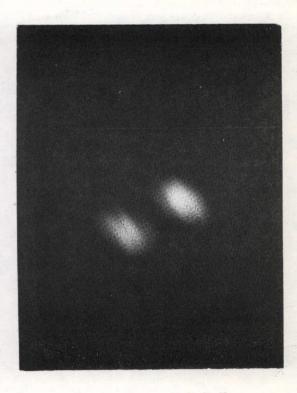


 Test No.
 //

 Retro:
 F

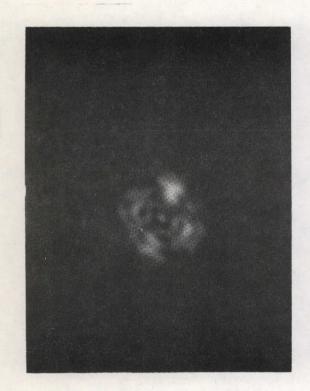
 Photo No.
 170

 Exposure Time:
 1/250 550



Test No.		11	
Retro:	-	F	
Photo No.		171	
Exposure	Time:	1/8 56	-

## cm | 1 2 3



Test No. //
Retro: F
Photo No. 172
Exposure Time: 1/25056E

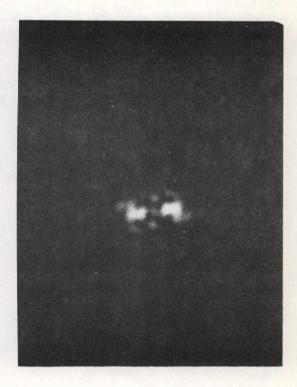


 Test No.
 //

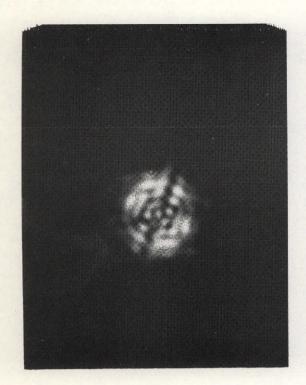
 Retro:
 F

 Photo No.
 /73

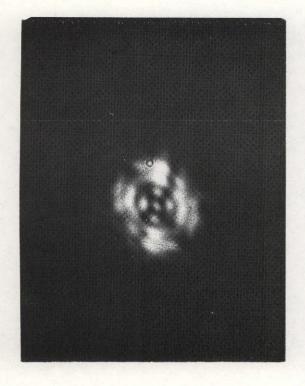
 Exposure Time:
 1/15 5EC



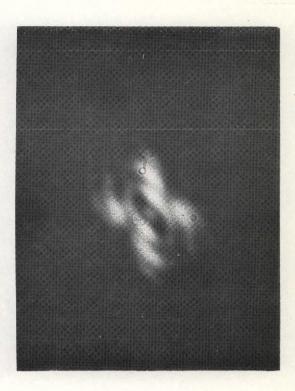
Test No.	19	
Retro:	CA	418.
Photo No.		174
Exposure	Time:	1/500 566



Test No. 19
Retro: D
Photo No. 175
Exposure Time: 1/250566



Test No. 19
Retro: D
Photo No. 176
Exposure Time: 1/250 SEC

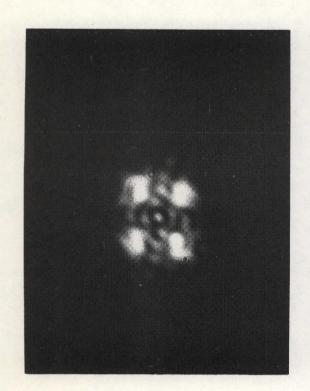


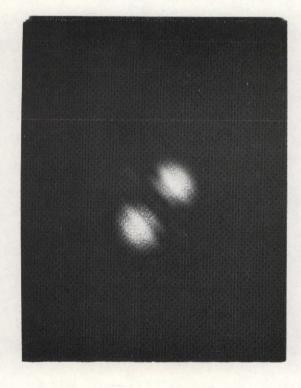
 Test No.
 19

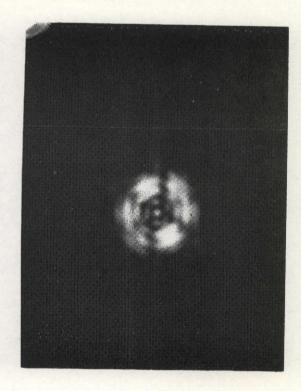
 Retro:
 D

 Photo No.
 177

 Exposure Time:
 1/60 SEC







 Test No.
 19

 Retro:
 D

 Photo No.
 178

 Exposure Time:
 1/125 566

Test No. 19
Retro: 0
Photo No. 179
Exposure Time: 1/8 55 C

Test No.	19
Retro:	E
Photo No.	180
Exposure 7	Time: /250 5EC



Test No. 19

Retro: E

Photo No. 181

Exposure Time: 1/250 56c

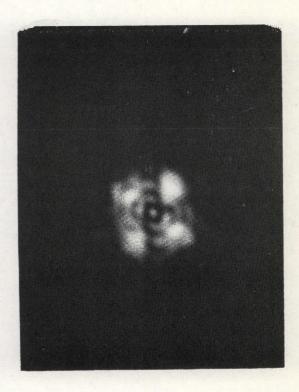


 Test No.
 19

 Retro:
 E

 Photo No.
 182

 Exposure Time:
 1/15 5EC



Test No.	19
Retro:	Ε
Photo No.	183
Exposure	Time: 1/125 5EC

## 

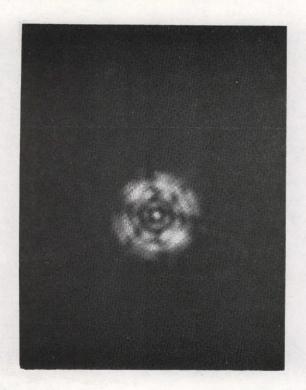


 Test No.
 /9

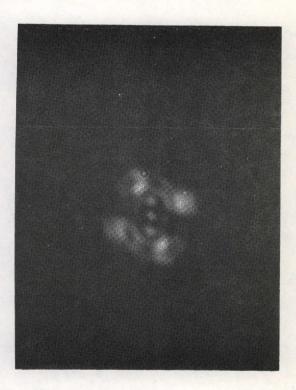
 Retro:
 E

 Photo No.
 184

 Exposure Time:
 1/8 sec



Test No. 19
Retro: F
Photo No. 185
Exposure Time: 1/250 5EC



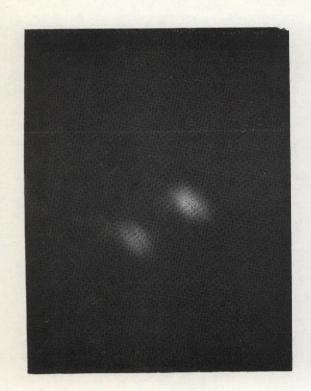
 Test No.
 /9

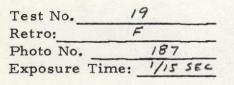
 Retro:
 F

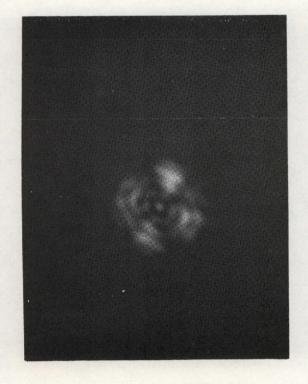
 Photo No.
 /86

 Exposure Time:
 1/250 56 c

m 1 2 3







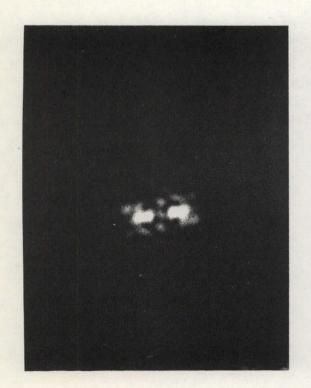
 Test No.
 /9

 Retro:
 F

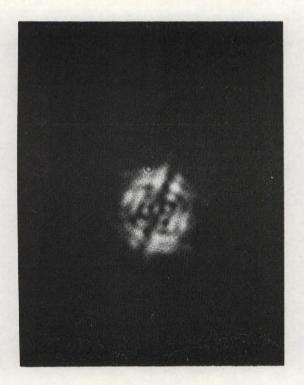
 Photo No.
 /88

 Exposure Time:
 1/250 566





Test No. /2
Retro: CALIB.
Photo No. 190
Exposure Time: 1/500 SEC



 Test No.
 /2

 Retro:
 D

 Photo No.
 191

 Exposure Time:
 1/250 560



 Test No.
 /Z

 Retro:
 D

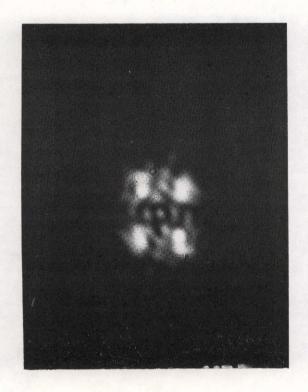
 Photo No.
 /92

 Exposure Time:
 '/2505EC

## 



Test No. 12
Retro: D
Photo No. 193
Exposure Time: 1/60 56C

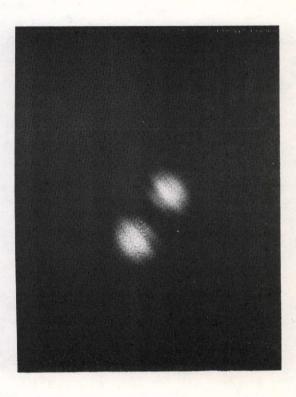


 Test No.
 /2

 Retro:
 D

 Photo No.
 /94

 Exposure Time:
 1/125 SEC



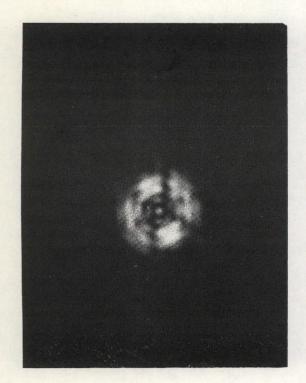
 Test No.
 /2

 Retro:
 D

 Photo No.
 195

 Exposure Time:
 1/8 sec

 $e_{\mathsf{m}}$ 

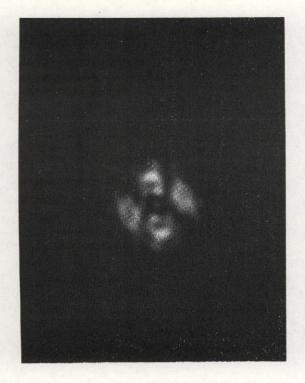


Test No. 12

Retro: E

Photo No. 196

Exposure Time: 1/250 560

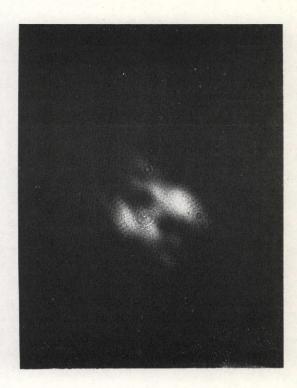


 Test No.
 /2

 Retro:
 E

 Photo No.
 /97

 Exposure Time:
 1/250 566



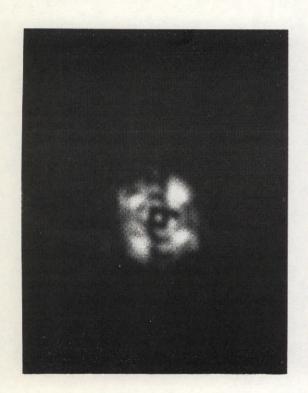
 Test No.
 /2

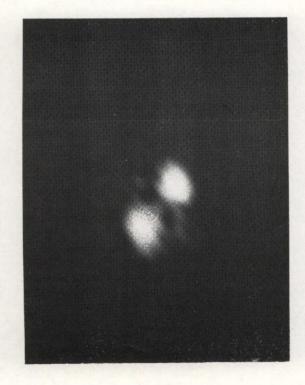
 Retro:
 E

 Photo No.
 /98

 Exposure Time:
 1/15 3EC

## 



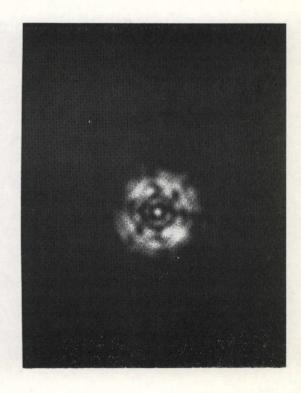


 Test No.
 12

 Retro:
 E

 Photo No.
 200

 Exposure Time:
 1/8 SEC

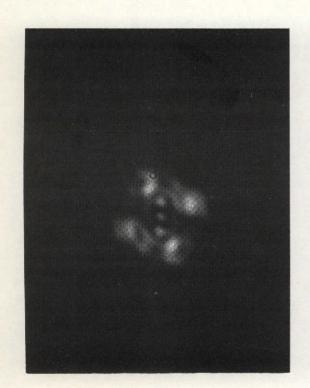


 Test No.
 /2

 Retro:
 F

 Photo No.
 20/

 Exposure Time:
 1/250 SEC

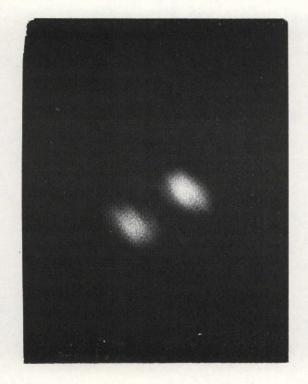


Test No. /Z

Retro: F

Photo No. 202

Exposure Time: 1/250 SEC

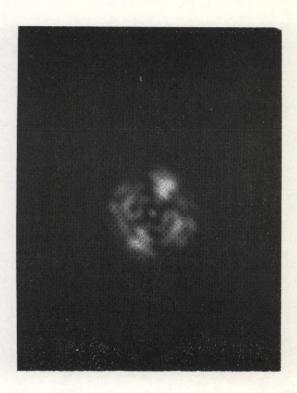


 Test No.
 /2

 Retro:
 F

 Photo No.
 203

 Exposure Time:
 1/8 sec



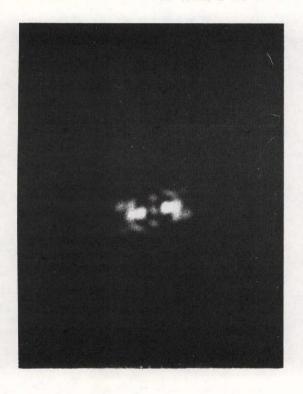
 Test No.
 /2

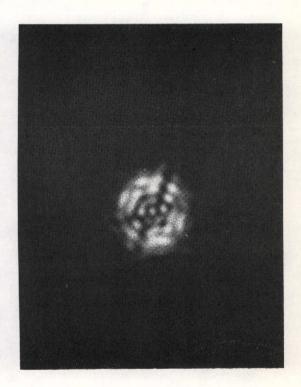
 Retro:
 F

 Photo No.
 204

 Exposure Time:
 ½50 56 c







Test No. 12

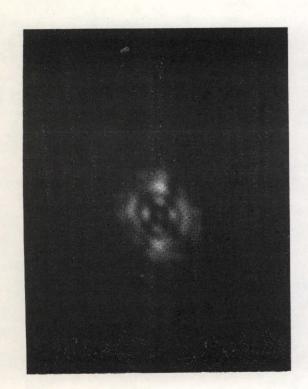
Retro: F

Photo No. 205

Exposure Time: 1/15 SEC

Test No.	20	
Retro:	CALIB.	
Photo No.	206	
Exposure	Time: //500	SEC

Test No.	20	
Retro:	0	
Photo No.	207	
Exposure Time:	1/250 SEC	

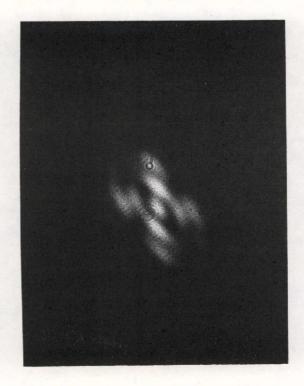


Test No. Zo

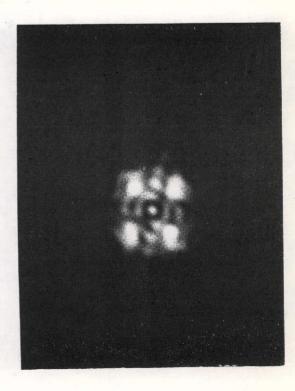
Retro: D

Photo No. Zo8

Exposure Time: 1/250 5Fc



Test No. 20
Retro: D
Photo No. 209
Exposure Time: 1/60 SEC



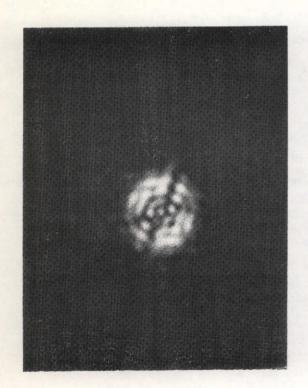
 Test No.
 Zo

 Retro:
 D

 Photo No.
 2/0

 Exposure Time:
 1/125 5EC

## 

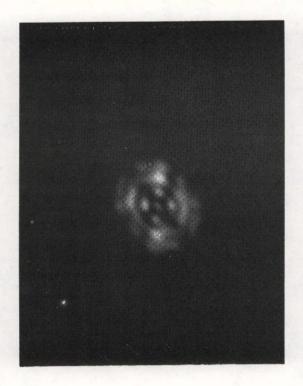


 Test No.
 20A

 Retro:
 D

 Photo No.
 2/2 \*

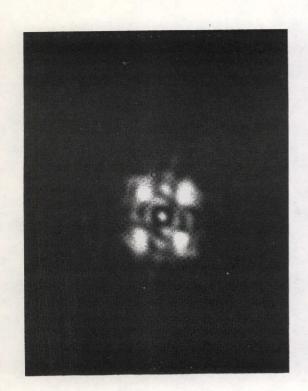
 Exposure Time:
 1/250 56C



Test No.	20 A
Retro:	D
Photo No.	213
Exposure Time:	1/250 560



Test No.	20A
Retro:	D
Photo No.	214
Exposure	Time: 1/60 560

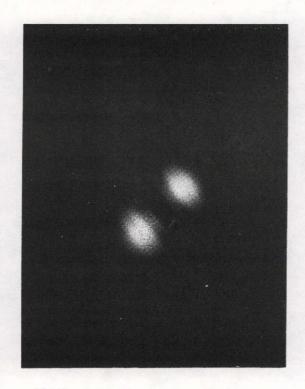


 Test No.
 20A

 Retro:
 D

 Photo No.
 2/5

 Exposure Time:
 1/125 5EC

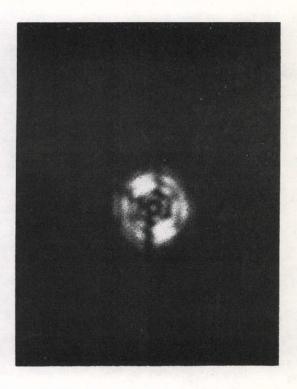


 Test No.
 20 A

 Retro:
 D

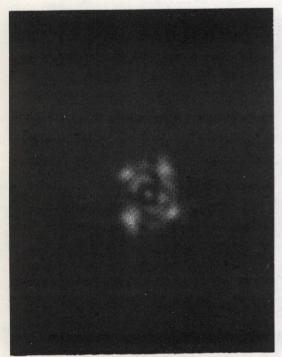
 Photo No.
 216

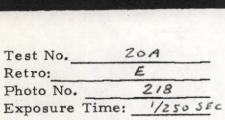
 Exposure Time:
 1/8 566



Test No.	2	OA	
Retro:		E	
Photo No.		217	100 - 10
Exposure	Time:	1/250	SEC

cm | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111 | 1111







 Test No.
 20A

 Retro:
 E

 Photo No.
 219

 Exposure Time:
 1/15 5EC



 Test No.
 20A

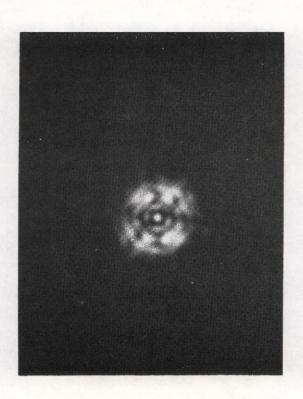
 Retro:
 E

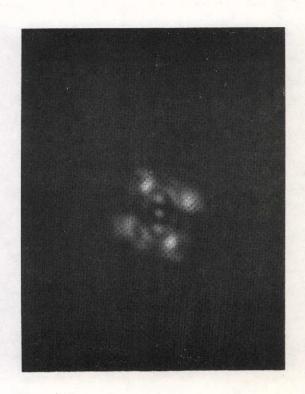
 Photo No.
 220

 Exposure Time:
 1/125 56 c

## m | 1 2 3





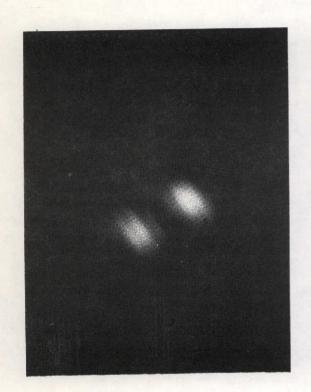


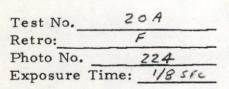
Test No.	20A
Retro:	E
Photo No.	221
Exposure Tin	ne: 1/8 SEC

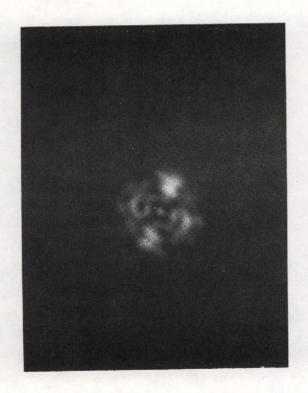
Test No.	ZOA
Retro:	F
Photo No.	222
Exposure Time:	1/250 566

Test No.	204
Retro:	F
Photo No.	223
Exposure	Time: 1/250 SEC

# 







 Test No.
 20 A

 Retro:
 F

 Photo No.
 225

 Exposure Time:
 1/250 56C

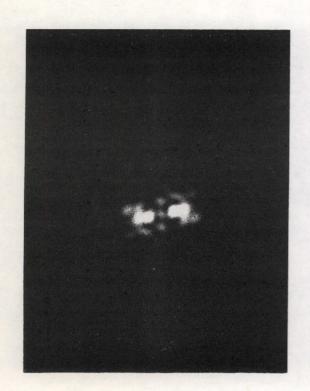


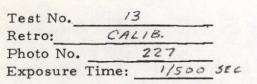
 Test No.
 ZOA

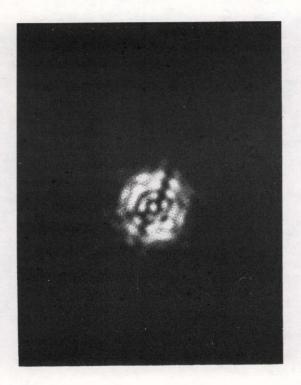
 Retro:
 F

 Photo No.
 226

 Exposure Time:
 1/15 5EC





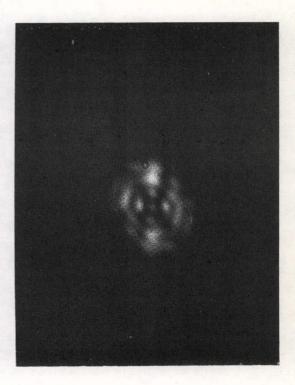


 Test No.
 /3

 Retro:
 D

 Photo No.
 228

 Exposure Time:
 1/250 SEC



 Test No.
 /3

 Retro:
 D

 Photo No.
 229

 Exposure Time:
 1/250 56C

## 

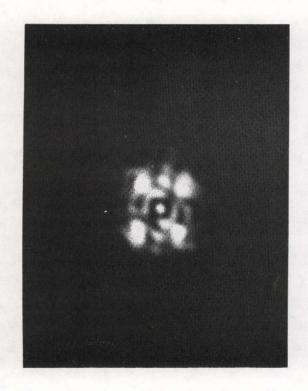


 Test No.
 /3

 Retro:
 D

 Photo No.
 230

 Exposure Time:
 1/60 560

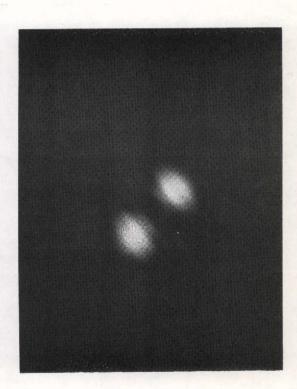


 Test No.
 /3

 Retro:
 D

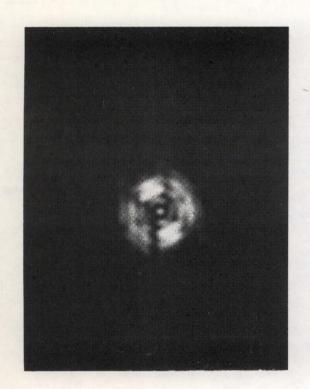
 Photo No.
 231

 Exposure Time:
 1/125 566

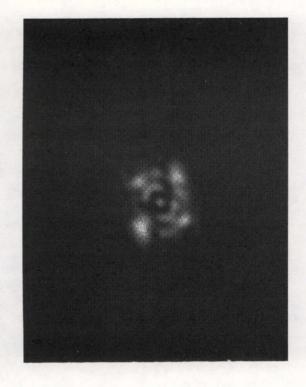


Test No.	13
Retro:	D.
Photo No.	232
Exposure Time:	1/8 SEC

## m | 1 2 3



Test No. /3
Retro: E
Photo No. 233
Exposure Time: 1/250 SEC

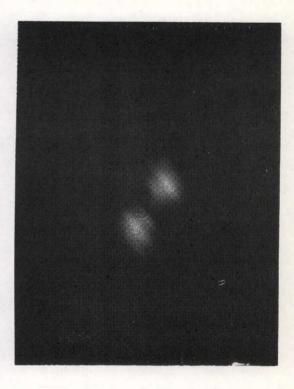


 Test No.
 /3

 Retro:
 E

 Photo No.
 234

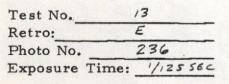
 Exposure Time:
 1/250 556



Test No.	13
Retro:	E
Photo No.	235
Exposure	Time: 1/15 SEC

## $c_{m}$ $\begin{vmatrix} 1 & 2 & 3 \end{vmatrix}$





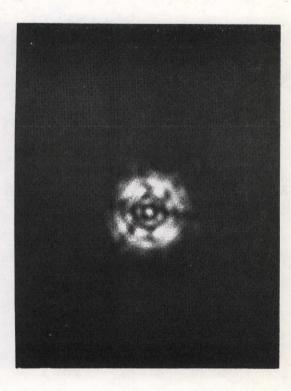


 Test No.
 /3

 Retro:
 £

 Photo No.
 237

 Exposure Time:
 1/15 5EC



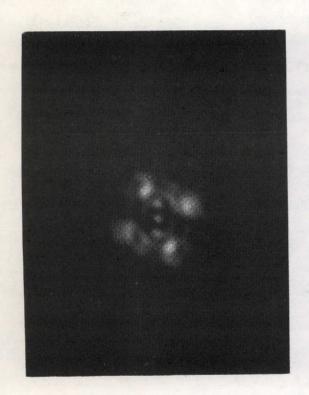
 Test No.
 /3

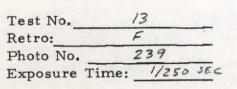
 Retro:
 F

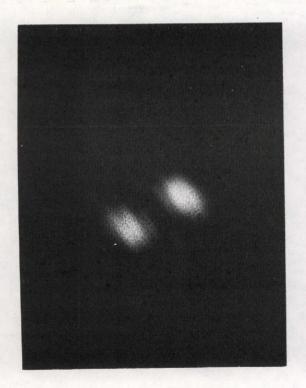
 Photo No.
 238

 Exposure Time:
 1/250 5€€

cm | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 111 | 1





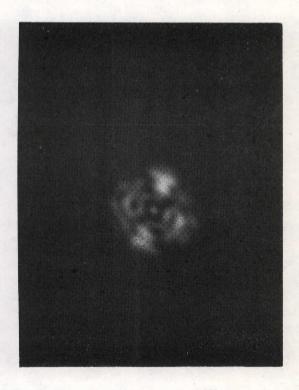


 Test No.
 13

 Retro:
 F

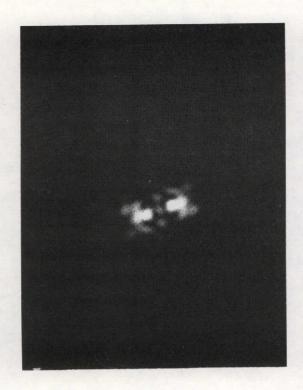
 Photo No.
 240

 Exposure Time:
 1/8 560

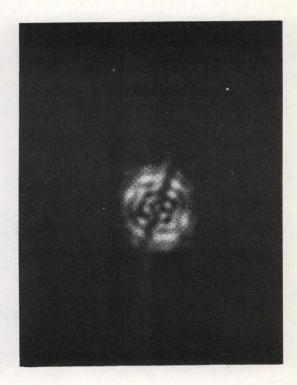




Test No. 13
Retro: F
Photo No. 24Z
Exposure Time: 1/15 566



Test No. 2/
Retro: CALIE.
Photo No. 243
Exposure Time: 1/500 SEC



 Test No.
 21

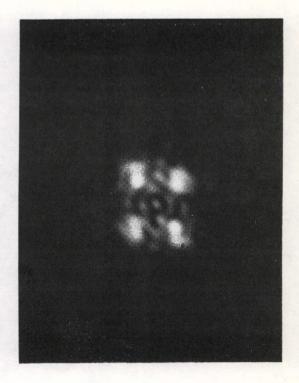
 Retro:
 D

 Photo No.
 244

 Exposure Time:
 1/250 SEC







Test No.	21	
Retro:	D	
Photo No.	245	
Exposure Time	: 1/250 SEC	

 Test No.
 2/

 Retro:
 D

 Photo No.
 246

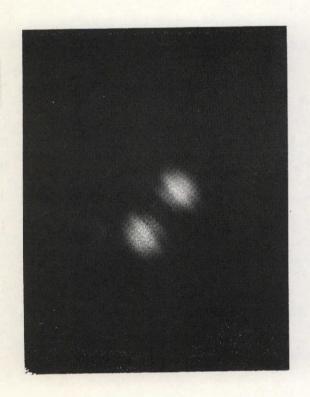
 Exposure Time:
 1/60 566

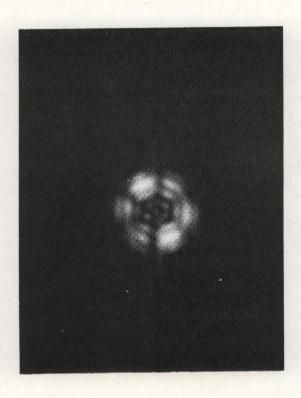
 Test No.
 2/

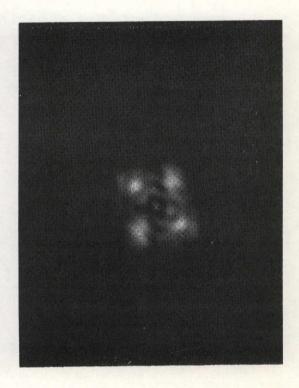
 Retro:
 D

 Photo No.
 247

 Exposure Time:
 1/125 SEC







Test No. 2/
Retro: 0
Photo No. 248
Exposure Time: 1/8 554

 Test No.
 21

 Retro:
 E

 Photo No.
 249

 Exposure Time:
 1/250 SEC

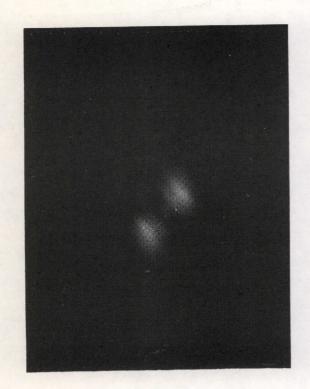
 Test No.
 2/

 Retro:
 €

 Photo No.
 250

 Exposure Time:
 1/250 560

## 

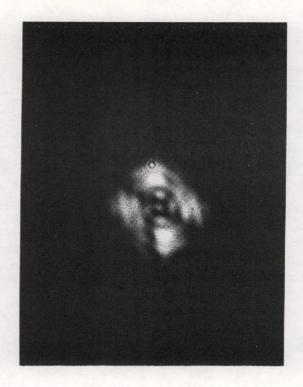


 Test No.
 21

 Retro:
 E

 Photo No.
 251

 Exposure Time:
 1/15 5EC

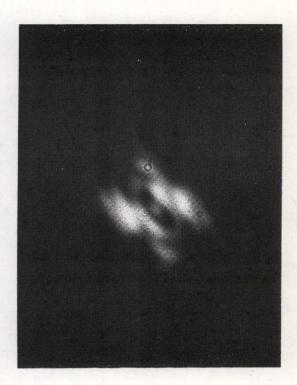


 Test No.
 2/

 Retro:
 E

 Photo No.
 252

 Exposure Time:
 '//25 566



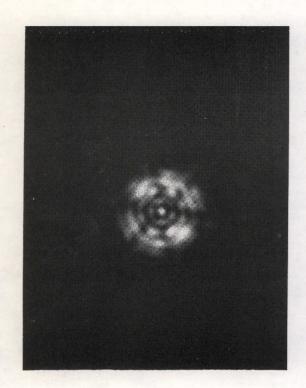
 Test No.
 2/

 Retro:
 £

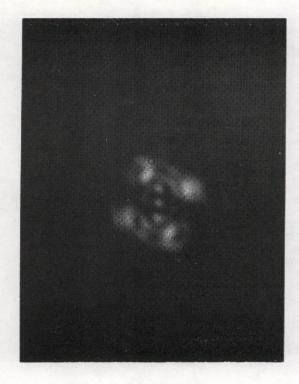
 Photo No.
 253

 Exposure Time:
 1/15 562

cm | Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling Hilling H



Test No. 2/
Retro: F
Photo No. 254
Exposure Time: 1/250 SEC

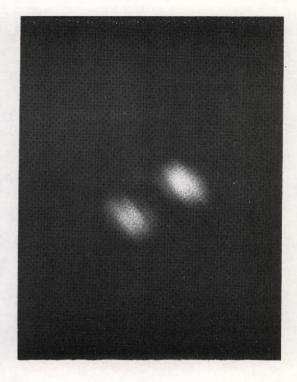


 Test No.
 21

 Retro:
 F

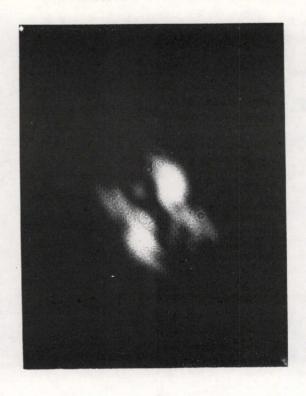
 Photo No.
 255

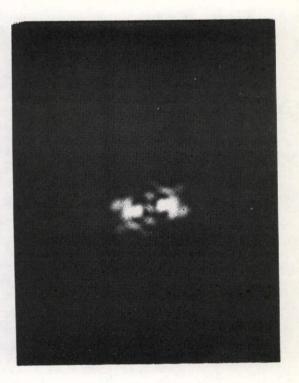
 Exposure Time:
 1/250 SEC



Test No.	21	
Retro:	F	
Photo No.	256	
Exposure	Time: 1/8 SEC	







Test No. 2/
Retro: F
Photo No. 257
Exposure Time: 1/250 SEC

 Test No.
 21

 Retro:
 F

 Photo No.
 258

 Exposure Time:
 1/15 SEC

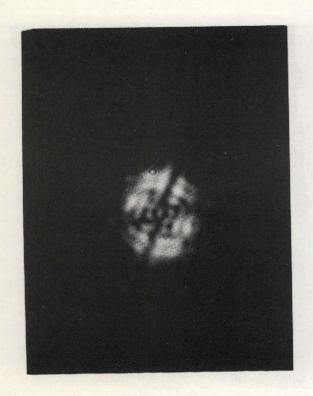
 Test No.
 14

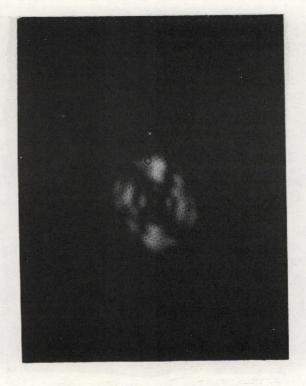
 Retro:
 CALIE.

 Photo No.
 259

 Exposure Time:
 1/500 SEC

 $rac{1}{1}$   $\frac{1}{2}$   $\frac{3}{3}$ 







 Test No.
 14

 Retro:
 0

 Photo No.
 260

 Exposure Time:
 1/250 56c

 Test No.
 14

 Retro:
 0

 Photo No.
 261

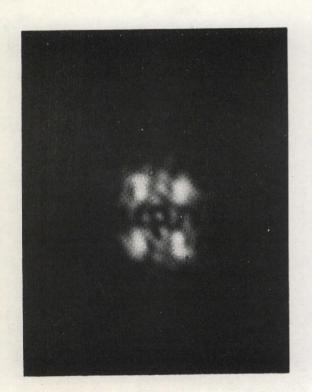
 Exposure Time:
 1/250 566

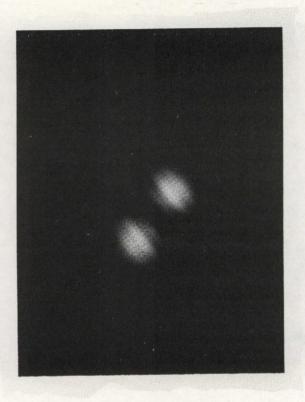
 Test No.
 /4

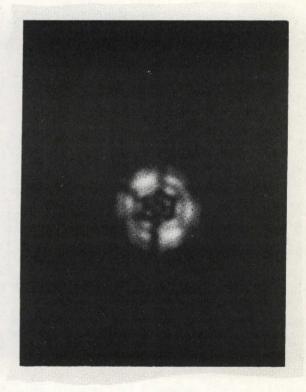
 Retro:
 D

 Photo No.
 262

 Exposure Time:
 '/60 5EC







 Test No.
 14

 Retro:
 D

 Photo No.
 263

 Exposure Time:
 1/125 5EC

 Test No.
 14

 Retro:
 D

 Photo No.
 264

 Exposure Time:
 1/8 586

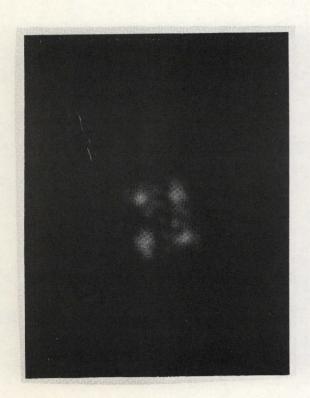
 Test No.
 /4

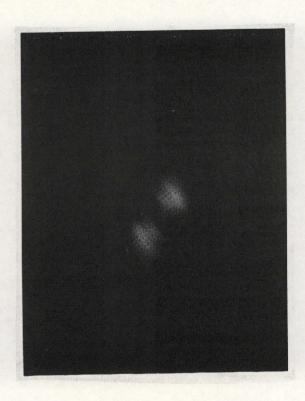
 Retro:
 E

 Photo No.
 265

 Exposure Time:
 '/250 SEC

 $\begin{smallmatrix} \epsilon_m \\ 1 \end{smallmatrix} \qquad \begin{array}{c} 1 \\ 1 \end{array} \qquad \begin{array}{c} 2 \\ 3 \end{array}$ 







Test No. 14

Retro: E

Photo No. 266

Exposure Time: 1/250 SEC

 Test No.
 14

 Retro:
 E

 Photo No.
 267

 Exposure Time:
 1/15 5EC

 Test No.
 14

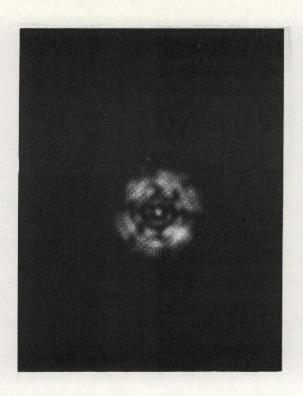
 Retro:
 E

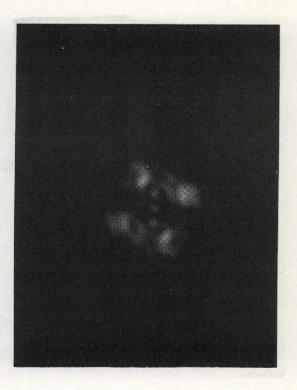
 Photo No.
 268

 Exposure Time:
 1/125 554

# 







 Test No.
 14

 Retro:
 E

 Photo No.
 269

 Exposure Time:
 1/15 560

 Test No.
 14

 Retro:
 F

 Photo No.
 270

 Exposure Time:
 1/250 5EC

 Test No.
 /4

 Retro:
 F

 Photo No.
 27/

 Exposure Time:
 1/250 586







Test No. 14

Retro: F

Photo No. 272

Exposure Time: 1/8 SEC

 Test No.
 /4

 Retro:
 F

 Photo No.
 273

 Exposure Time:
 '/250 55C

Test No. 14

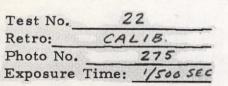
Retro: F

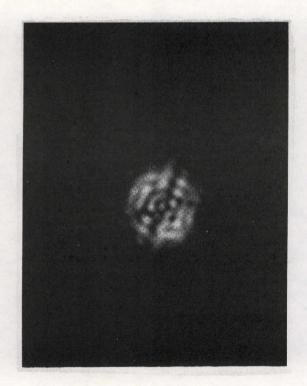
Photo No. 274

Exposure Time: 1/15 SEC

m | 1 2 3





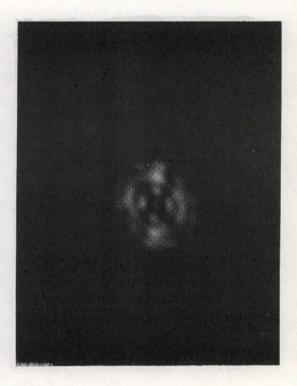


 Test No.
 22

 Retro:
 D

 Photo No.
 276

 Exposure Time:
 1/250 55c



Test No. 22

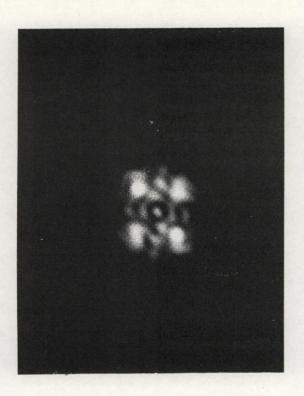
Retro: D

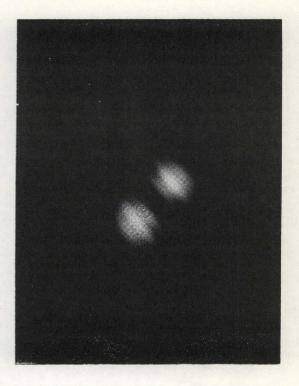
Photo No. 277

Exposure Time: 1/250 SEC

## 







 Test No.
 2Z

 Retro:
 D

 Photo No.
 278

 Exposure Time:
 1/60 SEC

Retro: D
Photo No. 279
Exposure Time: 1/125 SEC

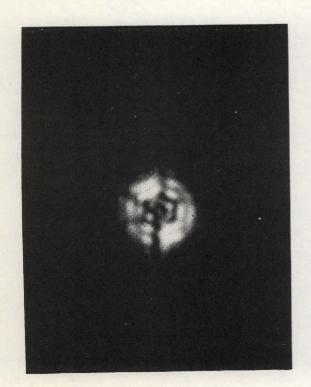
 Test No.
 2Z

 Retro:
 D

 Photo No.
 280

 Exposure Time:
 1/8 sec

## $c_{m}$

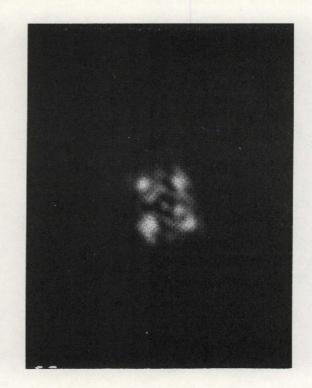


 Test No.
 22

 Retro:
 E

 Photo No.
 28 /

 Exposure Time:
 1/250 SEC

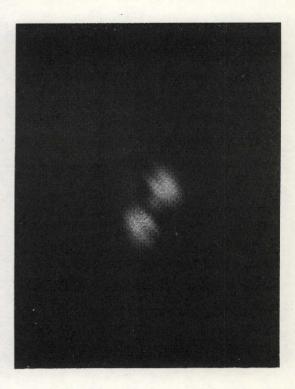


 Test No.
 22

 Retro:
 E

 Photo No.
 282

 Exposure Time:
 1/250 SEC

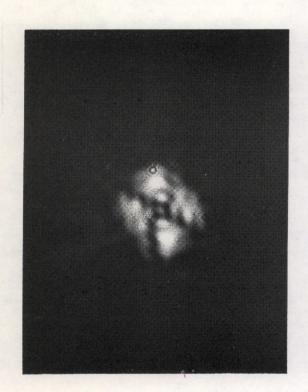


 Test No.
 2Z

 Retro:
 E

 Photo No.
 283

 Exposure Time:
 1/15 SEC



 Test No.
 22

 Retro:
 E

 Photo No.
 284

 Exposure Time:
 1/125 5EC

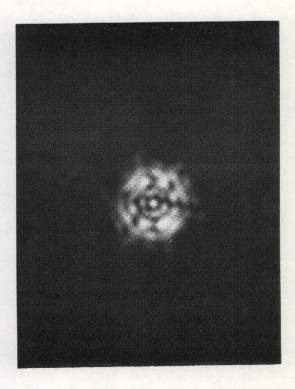


 Test No.
 22

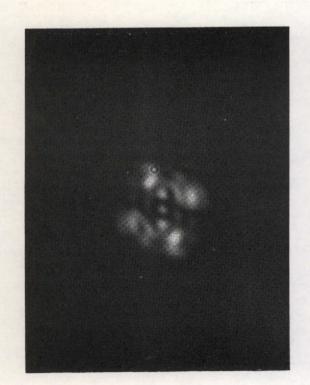
 Retro:
 €

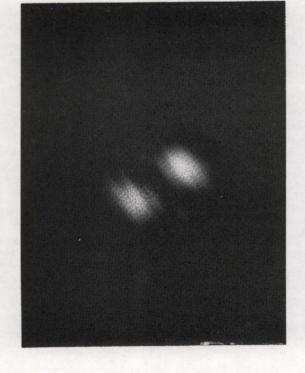
 Photo No.
 285

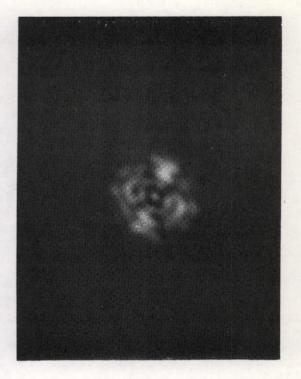
 Exposure Time:
 1/15 5€C



Test No.	22
Retro:	F
Photo No.	286
Exposure Time:	1/250 35-







Test No. 22

Retro: F

Photo No. 287

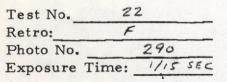
Exposure Time: 1/250 SEC

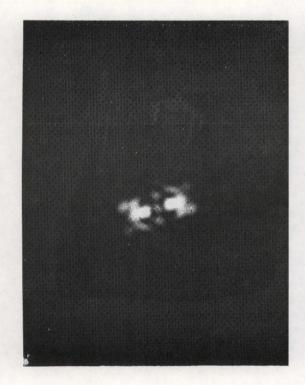
Retro:
Photo No. 288
Exposure Time: 1/8 sec

Test No.	22	
Retro:		
Photo No.	289	
Exposure Time:	1/250 SEC	

## 





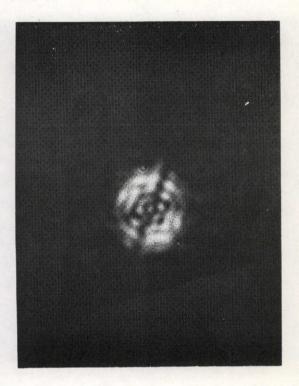


 Test No.
 23

 Retro:
 CALIB.

 Photo No.
 291

 Exposure Time:
 1/500 5EC

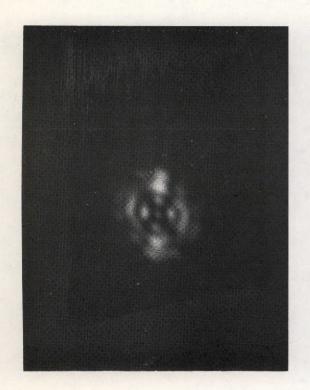


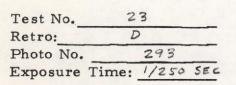
 Test No.
 23

 Retro:
 D

 Photo No.
 292

 Exposure Time:
 1/250 SEC





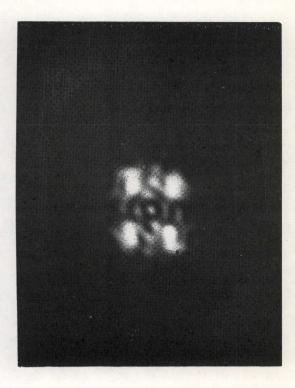


 Test No.
 23

 Retro:
 D

 Photo No.
 294

 Exposure Time:
 1/60 5 5 6



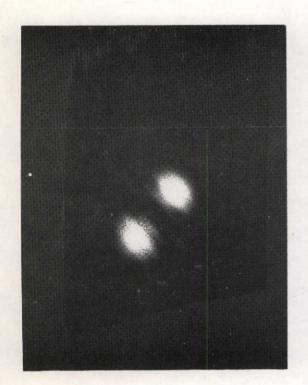
 Test No.
 23

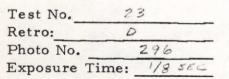
 Retro:
 D

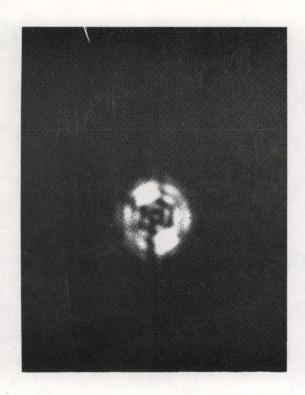
 Photo No.
 295

 Exposure Time:
 1/25 566

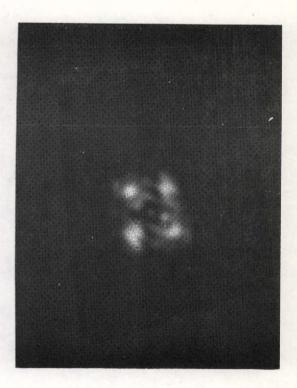
## 



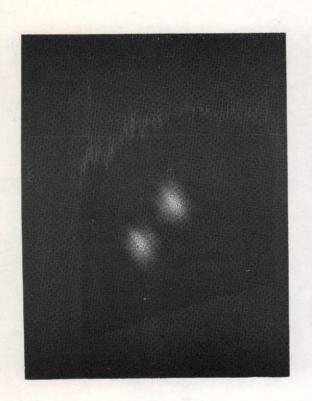


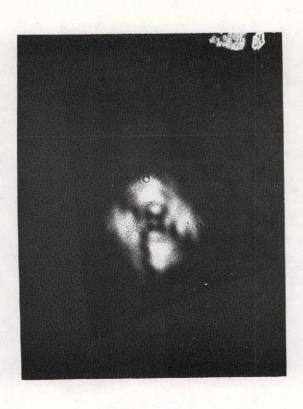


Test No.	23	
Retro:	E	
Photo No.	297	
Exposure Time:	1/250 SEC	



Test No.	23
Retro:	E
Photo No.	298
Exposure Time:	1/250 566







 Test No.
 23

 Retro:
 E

 Photo No.
 299

 Exposure Time:
 1/15 566

 Test No.
 23

 Retro:
 E

 Photo No.
 300

 Exposure Time:
 1/125 566

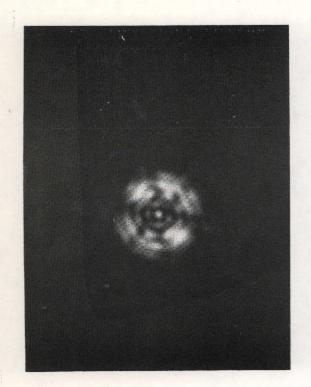
 Test No.
 23

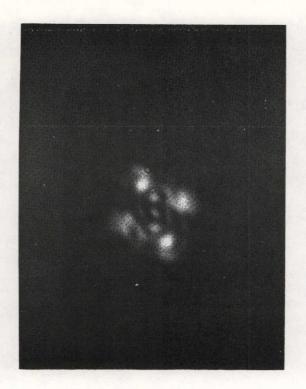
 Retro:
 £

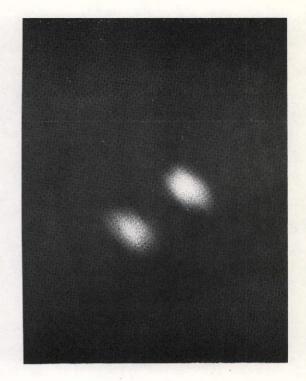
 Photo No.
 30/

 Exposure Time:
 1/15 5EC

<sub>նա</sub>լուվուվուկուկուկուկուկու 1 2 3







 Test No.
 23

 Retro:
 F

 Photo No.
 302

 Exposure Time:
 1/250 560

 Test No.
 23

 Retro:
 F

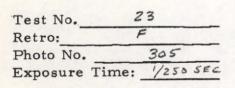
 Photo No.
 303

 Exposure Time:
 1/250 56 c

Retro: F
Photo No. 304
Exposure Time: 1/8 sec

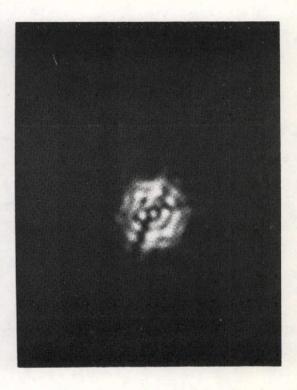
m | 1 2 3







Test No.	23	
Retro:	F	
Photo No.	306	
Exposure Time:	1/15 566	



 Test No.
 24

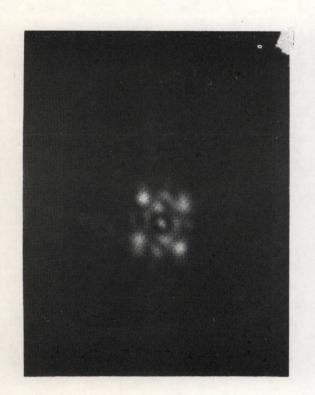
 Retro:
 A

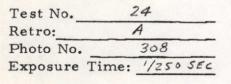
 Photo No.
 307

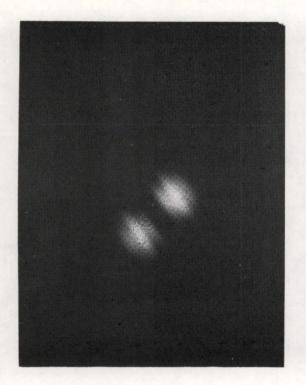
 Exposure Time:
 1/250 SEC

C-4

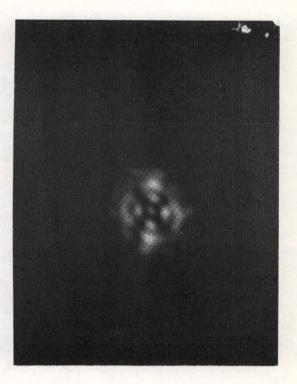
#### LAGEOS THERMAL/OPTICAL TESTS FAR-FIELD DIFFRACTION PATTERN PHOTOGRAPHIC OUTPUT - FFDI







Test No.	24
Retro:	A
Photo No.	309
Exposure Time:	1/8 586



Test No.	24
Retro:	A
Photo No.	310
Exposure Time:	1/250 566

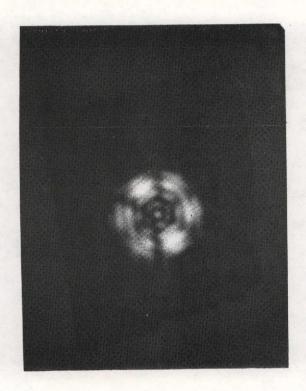


Test No. 24

Retro: A

Photo No. 3//

Exposure Time: 1/30 5EC



 Test No.
 24

 Retro:
 B

 Photo No.
 3/2

 Exposure Time:
 1/250 SEC



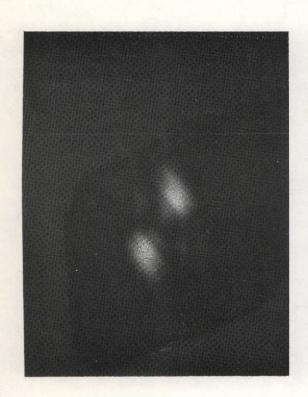
 Test No.
 24

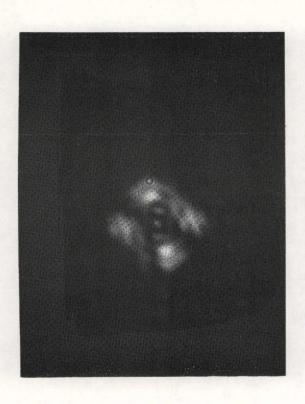
 Retro:
 B

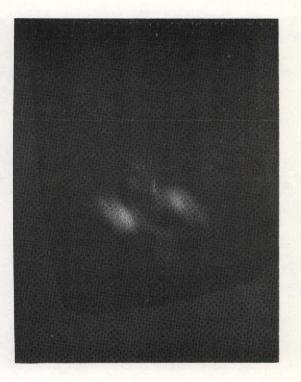
 Photo No.
 3/3

 Exposure Time:
 1/125 56c

 $\begin{smallmatrix} \mathsf{cm} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \begin{smallmatrix} \mathsf{I} \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad \qquad \\ \mathsf{I} \end{smallmatrix} \qquad \qquad$ 







Retro: 8

Photo No. 3/4

Exposure Time: 1/15 SEC

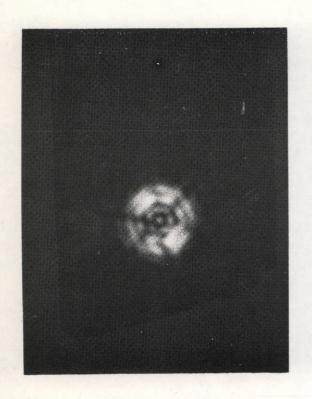
 Test No.
 24

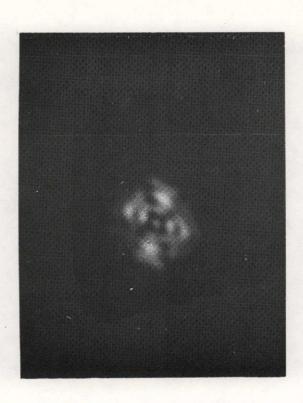
 Retro:
 B

 Photo No.
 3/5

 Exposure Time:
 1/250 5EE

Test No.	24	
Retro:	8	
Photo No.	316	
Exposure Time:	1/30 SEC	



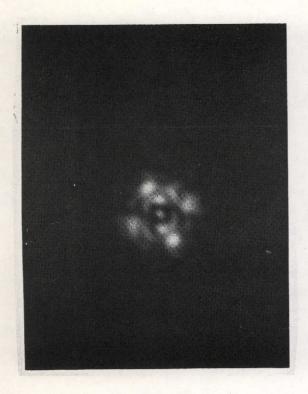


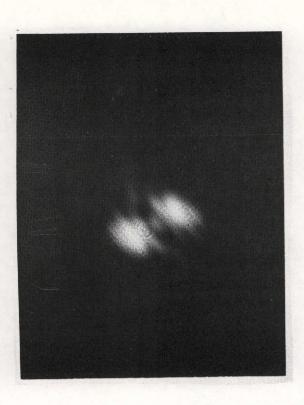


Test No	2	4	
Retro:	C		
Photo No.		317	- 35
Exposure	Time:	1/250	SEC

Test No.	24	
Retro:	<i>C</i>	
Photo No.	318	
Exposure Time:	1/250 SEC	

24
c
319
1/8 566





Test No. 24

Retro: C

Photo No. 320

Exposure Time: 1/250 SEC

 Test No.
 24

 Retro:
 C

 Photo No.
 321

 Exposure Time:
 1/8 562

Test No. \_\_\_\_\_\_

Retro: \_\_\_\_\_

Photo No. \_\_\_\_\_

Exposure Time: \_\_\_\_\_

	RELIABILITY			REVISIONS		CONFIG MGT
APPD PREDICTION				DATE	APPV'D	
			7,1	EXPERIMENTAL RELEASE ER 1922-13	7/3/70	216
			ΧZ	REVISED PER NASA/BYA T.R.R.	7/25/74	876
	'	•				
	,			APPENDIX V		

### TABLE OF CONTENTS

						Page	
			•	1.	0 OBJECTIVE	2	
		Υ —	, — <u>,                                  </u>	2.	0 APPLICABLE DOCUMENTS	2	
	오 3.				0 PARTICIPANTS REQUIRED	3	
	SERIAL N/A	N/A		4.	0 EQUIPMENT REQUIRED	4	
<u> </u>	SE			5.	0 TOLERANCES AND CONTROLS	<b>5</b>	
CATION	NO.			6.	0 TEST LEVELS	6	
APP	ITEM	N/A	-	7.	0 TEST PROCEDURE	11	
	ENG	-		8.	0 / DATA	14	
PART	_			- 9.	0 VARIATIONS	. 15	
AND	NEXT ASSY	4	ابر ا		10.	•	16
DRAWING		N/A		11.	0 TEST WITNESS SIGNATURES	17	
DRA	PART NO	2374464			REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR	e 8-14-74	
UNLE SPEC SION	CIFI	ED	DIM	EN- 196	CONTO MONINE CONTO CONTO	RPORATION — ANN ARBOR, MICHIGAN	
TERIAL:  BSGN SUPV PROJ ENGR Pringer 7/26/7/ QUAL CONT					BSGN SUPY THE LAGEOS TEST PROJ ENGR Stringer 7/26/74 QUAL CONT	ARTICLE	
DRAWING CLASS DSGN APPL			LASS	· [2]	MFG A Q/Q30 TP 2	X2	
<u> </u>	<u> </u>	ם נ	1	الطا	CUSTOMER SCALE WEIGHT	SHEET 1 of 17	



NO.	REV. NO.
TP2374457	×2
PAGE	OF
DATE	

### 1.0 OBJECTIVE

THE PURPOSE OF THE TEST IS TO VERIFY THE STRUCTURAL INTEGRITY OF THE LAGEOS TEST ARTICLE WHEN SUBJECTED TO THE SPECIFIED QUALIFICATION LEVEL VIBRATION ENVIRONMENTS. SUBSEQUENT TO VIBRATION, THE TEST ARTICLE WILL BE VISUALLY INSPECTED FOR DAMAGE (CHIPS, CRACKS, DEFORMATIONS, FRACTURES, ETC.)

THEREAFTER, OPTICAL TESTS WILL BE CONDUCTED TO DEMONSTRATE THAT THE VIBRATION TESTING DID NOT DEGRADE OPTICAL PERFORMANCE. SUCCESSFUL COMPLETION OF VIBRATION, INSPECTION, AND OPTICAL TESTS WILL ESTABLISH THAT THE LAGEOS DESIGN MARGINS ARE SUFFICIENT TO INSURE A HIGH DEGREE OF CONFIDENCE IN THE LAGEOS CAPABILITY TO SURVIVE THE LAUNCH VEHICLE DYNAMIC LOADS.

### 2.0 APPLICABLE DOCUMENTS

LAGEOS-14 (REV. B) "LAGEOS PHASE B THERMAL/
OPTICAL/VIBRATION ANALYSIS
AND TEST PROGRAM"



NO.	REY, HO.
TP2374457	X ?
PAGE3	of
DATE .	·

STM-1010

"ENVIRONMENTAL LABORATORIES RAN-

DOM VIBRATION TESTING - AUTOMATIC

EQUALIZER/ANALYZER SYSTEM

STM-1011

"SETUP AND OPERATIONS PROCEDURE

FOR SINE VIBRATION TEST"

#### 3. 0 PARTICIPANTS REQUIRED

ENVIRONMENTAL/QUALITY TEST CONDUCTOR

LAGEOS ENGINEERING REPRESENTATIVE

Bendin <sub>1</sub>
erospace Systems Division

NO.	REV. NO.
TP2374457	X2.
PAGE 4	0F
DATE	

### 4. 0 EQUIPMENT REQUIRED

ITEM	MANUFACTURER	PART NO. OR MODEL	*SERIAL NO.	*CALIB. DATE
			<del>*************************************</del>	
VIBRATION SYSTEM	LING	249	<u>13/30</u>	N/A
TEST FIXTURE - LAGEOS	BXA	2374456 .	N/A	N/A
RECORDER, X-Y	MOSELEY	20	10010	2-6-75
LOGARITHMIC CONVERTER	MOSELEY	60 D	12415	11-06.74
LOGARITHMIC CONVERTER	MOSELEY	7561	14289	08-27-74
ACCELEROMETER	ENDEVCO	2221	VR59	7-3-75
EXCITER CONTROL	LING	SCO-100	14869	10-29-74
TRMS VOLTMETER	B&K	2409	5/642	10-18-24
TAPE RECORDER	SANBORN	3900	13943	10-26-74
CHARGE AMPLIFIER	ENDEVCO	2614C	51471	11-07-74
EQUALIZER/ANALYZER	LING	ASDE-80	14296	09-23-74
LO-PASS FILTER	LING	LP-10	50950	01-08-75
DYNA-MONITOR	ENDEVCO-	2702	09633	09-07-74
DYNA-MONITOR	ENDEVCO	2702C	NOT	WED.

\*TO BE COMPLETED PRIOR TO TESTING. EQUIPMENT SUBSTITUTIONS AND ADDITIONS SHALL BE LISTED BELOW.

TOROUE WRENCH	LIVER MONT	6056	05369 09-13-74
TORDYE WRENDY			<u> 51960 12-4-74</u>
REDROCK, X-Y	Mosecey	201-24	14287 10-17-74
VIBRATION SYSTEM	MB	C-10	484 N/A



NO.	REV. NO.
TP2374457	<u> </u>
PAGE5	OF
DATE	

(3)

5.0 TOLERANCES AND CONTROLS

THIS PROCEDURE UTILIZES ENVIRONMENTAL LABORATORIES STANDARD TEST METHODS FOR OPERATION OF FACILITY AND INSTRUMENTATION EQUIPMENT.

5.1 MONITORING TOLERANCE

INSTRUMENTATION DEVICES OR SYSTEMS SHALL BE CALI-BRATED SO AS TO PROVIDE MONITORING ACCURACIES AS FOLLOWS:

a. VIBRATION DISPLACEMENT: ±5%

b. VIBRATION ACCELERATION: ±3%

c. VIBRATION FREQUENCY: ±2 HZ, 5 TO 40 HZ ±5%, ABOVE 40 HZ

5.2 CONTROL TOLERANCE

THE MAXIMUM ALLOWABLE VARIATION IN THE CONTROL
OF THE SPECIFIED LEVELS DURING VIBRATION TESTING
SHALL BE:

VIBRATION AMPLITUDE: SINUSOIDAL ±10%

RANDOM PSD ±3 DB

RANDOM G-RMS±10%

VIBRATION FREQUENCY:

±2HZ, 5 TO 40 HZ ±5%, ABOVE 40 HZ



J **O.	RET. NO.
TP2374457	× 2
PAGE6	OF
DATE	

(h)

THESE TOLERANCES APPLY TO THE CONTROL OF THE INPUT TO THE SPECIMEN AS MONITORED WITH A SINGLE ACCELEROMETER. THE SWEEP RATE FOR SINUSOIDAL VIBRATION MAY BE REDUCED NEAR THOSE FREQUENCIES WHERE THE TOLERANCE BECOMES DIFFICULT TO MAINTAIN IN ORDER TO ALLOW THE SERVO TO RESPOND.

OVER-G CUT-OFF AND NO SIGNAL DETECTION

PRIOR TO THE START OF EACH TEST, THE OVER "G" CUTOFF SHALL BE SET AT 50% OVER THE MAXIMUM SPECIFIED
LEVEL AND ITS OPERATION VERIFIED BY SIGNAL INJECTION.

THE NO-SIGNAL DETECTOR OPERATION WILL BE VERIFIED
AT THE START OF THE TEST FOR RANDOM AND SINUSOIDAL

LEVELS WITHOUT THE TEST ITEM INSTALLED.

BOTH WILL BE RESET FOR SINUSOIDAL AND RANDOM AS REQUIRED.

### 6.0 TEST LEVELS

PERFORM THE FOLLOWING VIBRATION TESTS. THE AXES

MAY BE TESTED IN ANY ORDER, AND THE SEQUENCE OF

THE RANDOM AND SINUSOIDAL SHALL BE DETERMINED BY

THE QUALITY TEST CONDUCTOR.



NO.	REY. NO.
TP2374457	. <b>X</b> 7.
PAGE 7	OF
DATE	

## 6.1 SINUSOIDAL VIBRATION

THE REQUIRED SINUSOIDAL VIBRATION LEVELS (SHOWN IN FIGURE 1) ARE:

FREQUENCY RANGE	<u>LEVEL</u>
5-12 HZ	0.3 IN. DBL. AMPL.
12-16	2.3 G-PEAK
16-22	6.8 G-PEAK
22-200	2.3 G-PEAK
200-2000	5.0 G-PEAK

ONE SWEEP (5-2000 HZ) IS REQUIRED PER AXIS, DEFINED IN FIGURE 2, AT A SWEEP RATE OF 2 OCTAVES PER MINUTE.

### 6.2 RANDOM VIBRATION

THE REQUIRED RANDOM VIBRATION LEVELS (SHOWN IN

FIGURE 3) ARE:

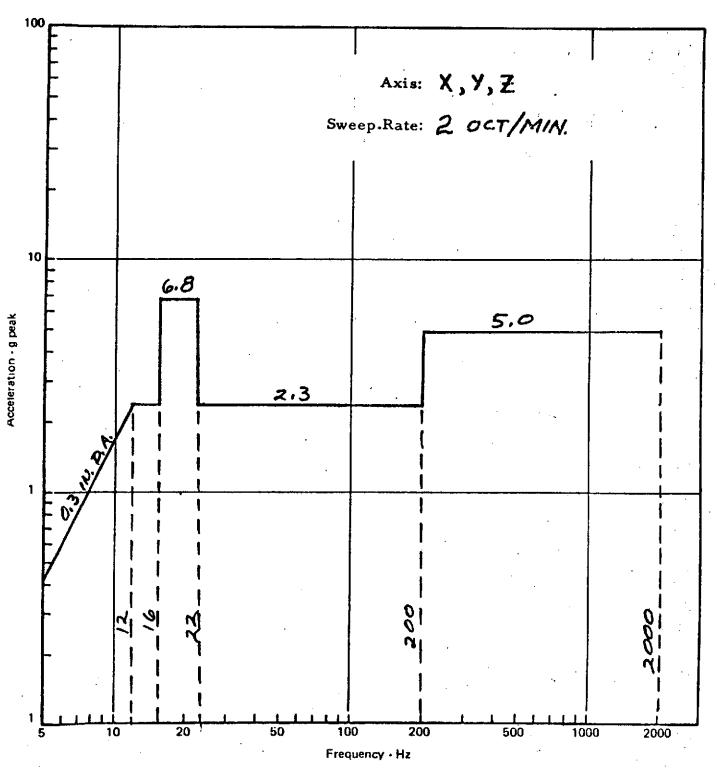
FREQUENCY RANGE	<u> LEVEL</u>
5-300	+3 DB/OCT
300-2000	0.05 G <sup>2</sup> /HZ

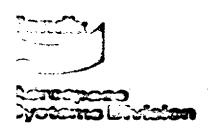
promo Cythian

lue.	C2V. HO.
TP2374457	
PAGE8	or
<b>M</b> TE	

(8)

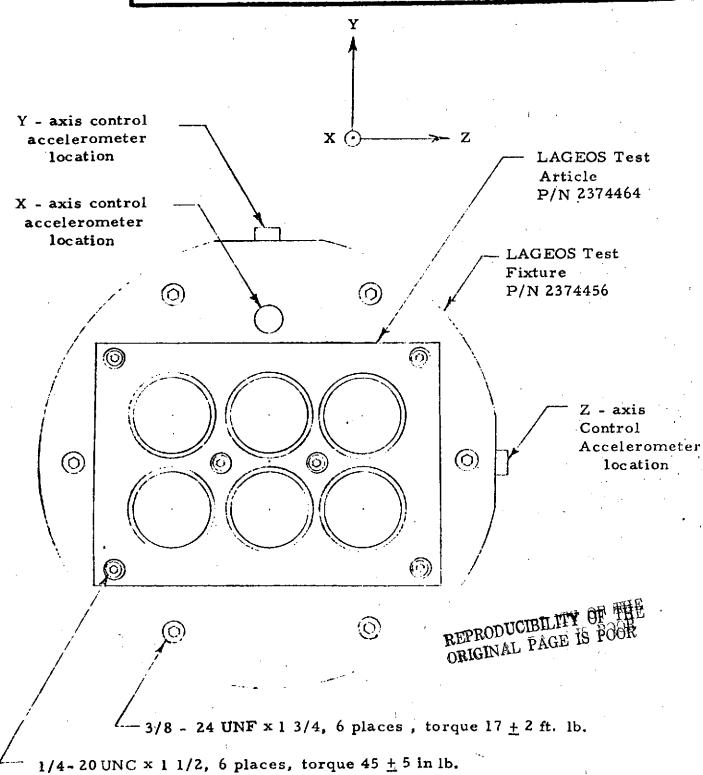
#### SINUSOIDAL VIBRATION





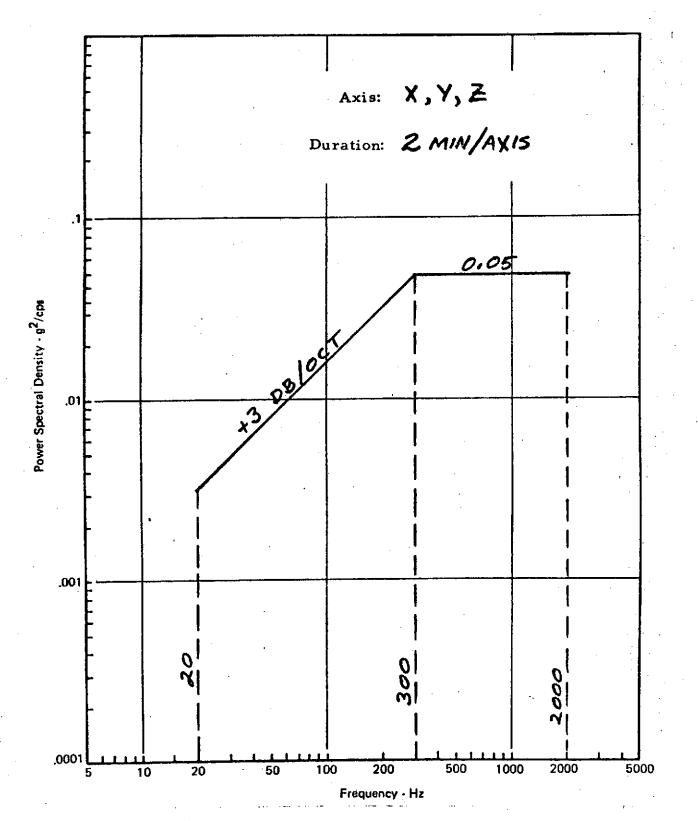
TP2374457 × "

PAGE 9 OF \_\_\_\_\_



-
Sections Program

INC.		BEV. HO.
TP23	74457	1
PAGE .	10	07
MTE		





TP2374457	×2
PAGE	OF
DATE	

THESE LEVELS WILL BE MAINTAINED FOR A DURATION OF 2.0 MINUTES FOR EACH AXIS DEFINED IN FIGURE 2.

THE CORRESPONDING ROOT-MEAN-SQUARE ACCELERATION IS 9.6 G.

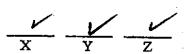
- 7.0 TEST PROCEDURE
- 7.1 VERIFY PROPER NO-SIGNAL DETECTOR OPERATION.

$$\frac{V}{X}$$
  $\frac{V}{Y}$   $\frac{V}{Z}$ 

- 7.2 INSTALLATION
- 7.2.1 REMOVE THE COVER AND INSTALL THE LAGEOS TEST
  ARTICLE ON THE VIBRATION FIXTURE USING SIX 1/420UNC-2A BY 1 1/2 IN SCREWS WITH WASHERS.



- 7.2.2 REPLACE THE LAGEOS COVER.
- 7.2.3 INSTALL THE VIBRATION FIXTURE ON THE VIBRATION
  EXCITER USING SIX 3/8-24UNF BY 1 3/4 IN. SCREWS WITH
  WASHERS.



Pendix	9
1erosp	ace SDivision

NO.	REV. NO.
TP2374457	×τ
PAGE 12	OF
DATE	7

7.2.5 PHOTOGRAPH THE TEST SET-UP AND ATTACH PHOTO-GRAPH TO DATA LOG.

$$\frac{\sqrt{x}}{x} \frac{\sqrt{x}}{y} \frac{\sqrt{x}}{z}$$

ADJUST THE NECESSARY EQUIPMENT PER STM 1011 TO 7.3 APPLY THE SINE VIBRATION OF FIGURE 1.

$$\frac{\sqrt{x}}{x}$$

SET THE OVER "G" CUTOFF TO 10.2 G-PEAK AND VERIFY 7.4 ITS OPERATION BY SIGNAL INJECTION.

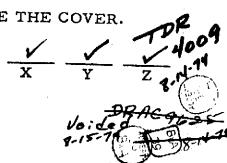
$$\frac{\sqrt{x}}{x} \frac{\sqrt{y}}{z}$$

REMOVE THE COVER AND APPLY THE SINUSOIDAL VIBRA-7.5 TION OF FIGURE 1. RECORD THE CONTROL ACCELERO-METER SIGNAL. ATTACH X-Y RECORDING TO DATA LOG.

$$\frac{\sqrt{\sqrt{x}}}{x}$$

VERIFY ACTUAL LEVELS ARE WITHIN SPECIFICATION 7.6 LIMITS. (NOTE: X-Y RECORDING FOR REFERENCE ONLY  $\frac{\sqrt{\frac{\sqrt{\frac{\sqrt{2}}{2}}}{\sqrt{2}}}}{\sqrt{2}}$ BELOW 20 HZ.)

VISUALLY INSPECT THE CCR AND MOUNT FOR DAMAGE 7.7 (WITHOUT DISASSEMBLY). REPLACE THE COVER.



sendin 1
arospace iystems Division

	но.	REV. NO.
	TP2374457	X 2
_	PAGE	OF
	DATE	

7.8 ADJUST THE NECESSARY EQUIPMENT PER STM 1010 TO APPLY THE RANDOM VIBRATION OF FIGURE 3.

$$\frac{\sqrt{\frac{\sqrt{x}}{x}}}{\sqrt{x}} = \frac{\sqrt{x}}{\sqrt{x}}$$

- 7.9 SET THE OVER "G" CUTOFF AT 14.4 RMS AND VERIFY ITS OPERATION BY SIGNAL INJECTION.  $\frac{1}{X}$   $\frac{1}{Y}$   $\frac{1}{Z}$
- 7.10 REMOVE THE COVER AND APPLY THE RANDOM VIBRATION OF FIGURE 3 FOR 120 SECONDS. RECORD THE CONTROL ACCELEROMETER SIGNAL. ATTACH X-Y RECORDING TO THE DATA LOG.
- 7.11 VERIFY ACTUAL LEVELS ARE WITHIN SPECIFICATION

  LIMITS.

  X
  Y
  Z
- 7.12 VISUALLY INSPECT THE CCR AND MOUNT SYSTEM FOR DAMAGE (WITHOUT DISASSEMBLY). REPLACE THE COVER.

$$\frac{\sqrt{x}}{x} \frac{\sqrt{x}}{y} \frac{\sqrt{z}}{z}$$

7.13 REMOVE THE FIXTURE FROM THE EXCITER.

$$\frac{\checkmark}{x}\frac{\checkmark}{y}\frac{\checkmark}{z}$$



I NO.	REV. NO.
TP2374457	ΧZ
PAGE	OF
DATE	

(14)

7.14 REPEAT PARAGRAPHS 7.1 THROUGH 7.13 FOR THE NEXT DESIRED AXIS.

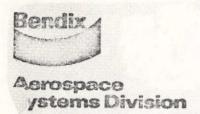
7.15 REPEAT PARAGRAPHS 7.1 THROUGH 7.13 FOR THE FINAL AXIS OF VIBRATION.

7.16 REMOVE THE MOUNTING SCREWS AND WASHERS AND
REMOVE THE LAGEOS TEST ARTICLE FROM THE VIBRATION FIXTURE.

7.17 REMOVE CCR "E" FROM THE TEST ARTICLE AND VISUALLY INSPECT FOR DAMAGE.

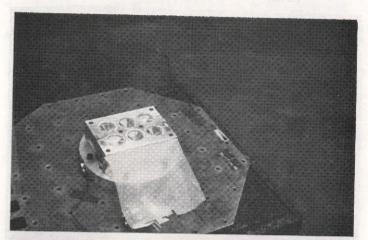
### 8.0 DATA SHEETS

- a) INSERT G-PEAK VS. FREQUENCY PLOTS (SINUSOIDAL)
- b) INSERT PSD PLOTS (RANDOM)
- c) LIST FAILURES OR OUT-OF-TOLERANCE CONDITIONS
- d) ATTACH TEST SET-UP PHOTOGRAPHS OF EACH AXIS
- e) ATTACH ADDITIONAL DATA SHEETS AS REQUIRED.

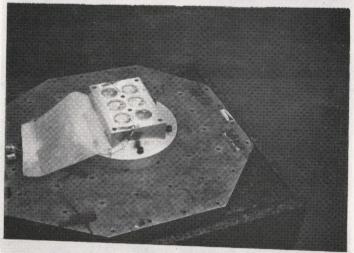


TP2374457	REV. NO.
PAGE	OF

# Test Sotup Photographs



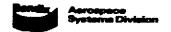
ZAxis



Y Axis



XAxis

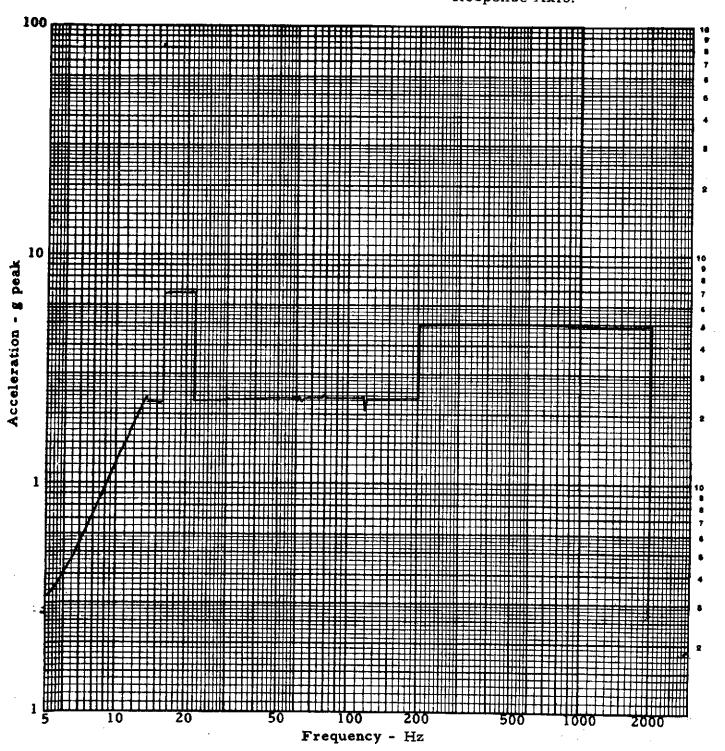


## VIBRATION LEVELS

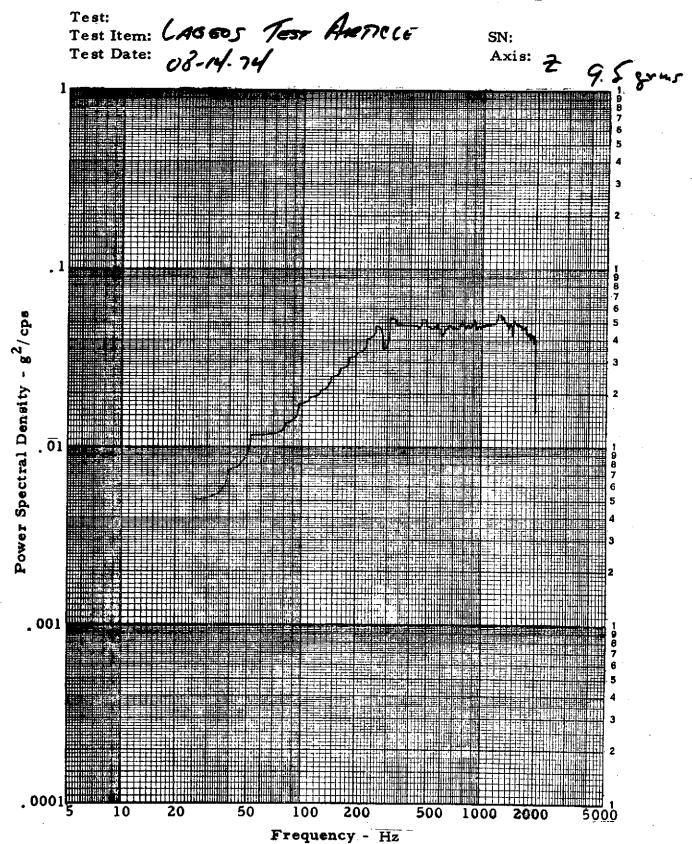


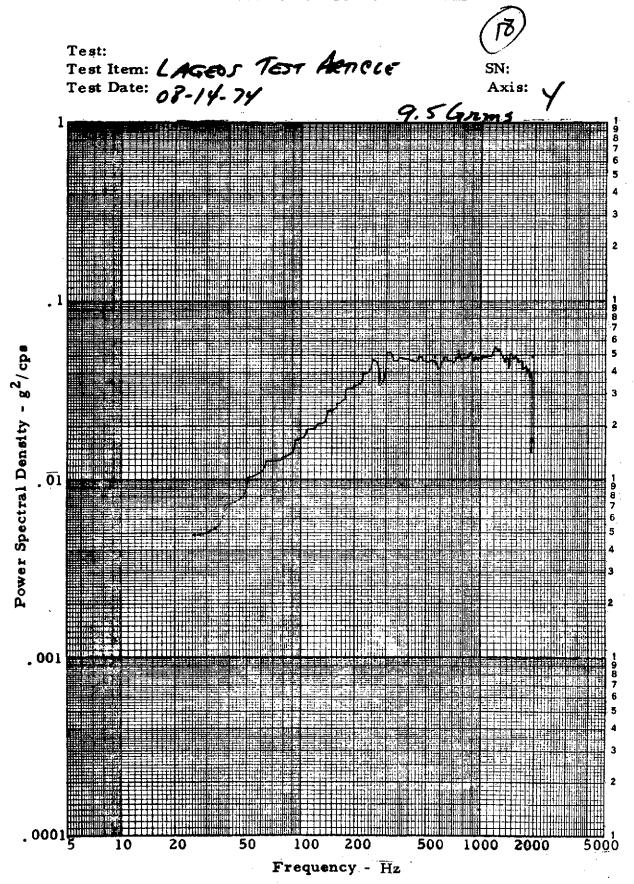
Test Item: LAGEOS TEST ARTICLE
Test Date: 08.14.74

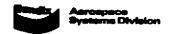
Serial Number:
Input Axis:
Response Axis:









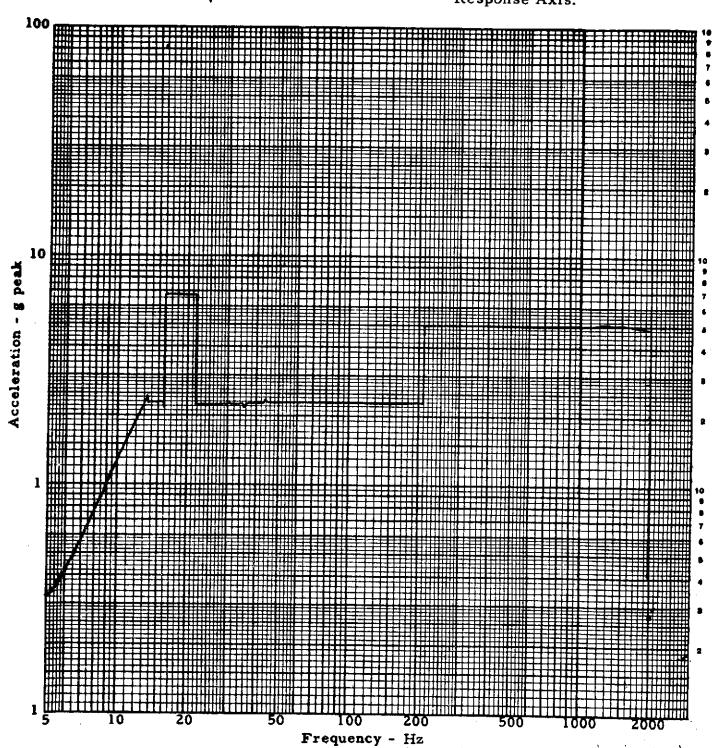


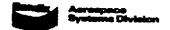
### VIBRATION LEVELS



Test Item: LAGEOS Test Article
Test Date: 08-14-74

Serial Number:
Input Axis: 2
Response Axis:





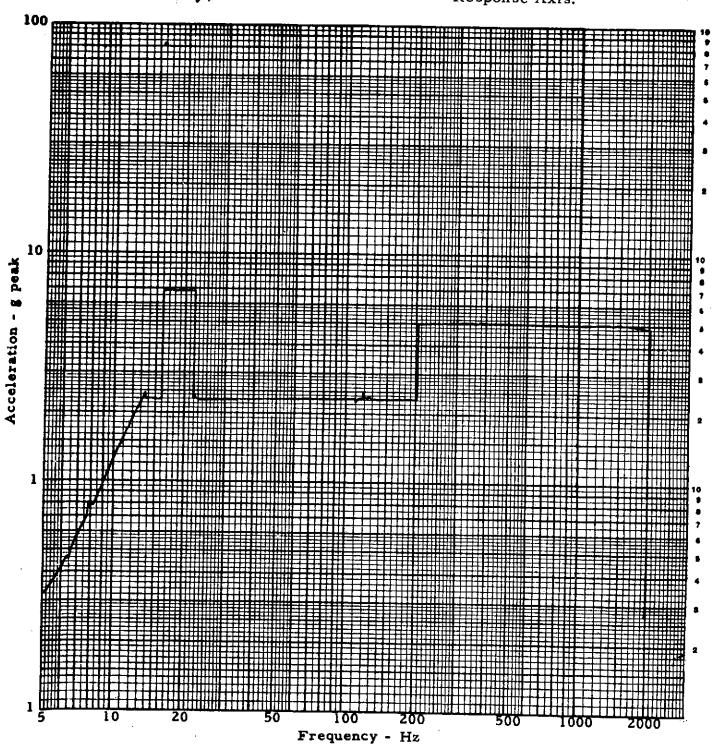
TR FIGURE

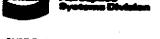
(D)

### VIBRATION LEVELS

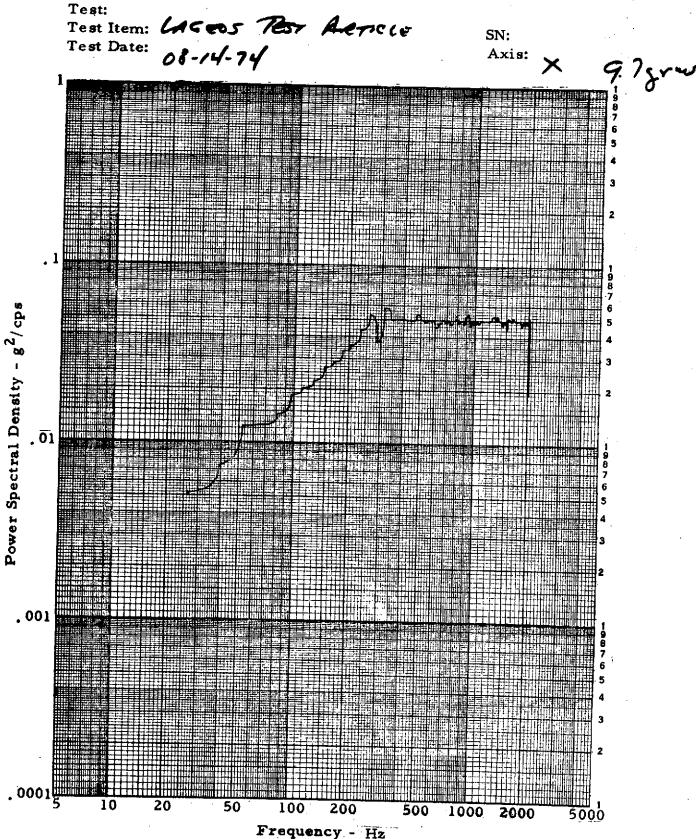
Test Item: LAGEOS TEST Article
Test Date:
08-14-74

Serial Number: Input Axis: Response Axis:











Ž

2374457

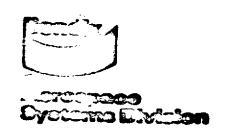
1

V-22

## QUALITY ASSURANCE DEPT. TEST DISCREPANCY REPORT

CTOR - ADJACI	NOTED ON TENT TO THE	NE "	MO. DAY YR. DB I Y T F REV
	<b>*</b> W	and	
•		ws 1.4	ss. Lb.
	CAUSE OF ANOMALY:	CLASSIF	ICATION OF DEFECT
	1		CR CRITICAL
	DEDBODICIDA AME	-	MA MAJOR
E DISCREPANCY	ORIGINAL PAGE IS I	f the Poor	MI MINOR
KPLAIN)=	-		PA PAPERWORK
Ε)			6 CODE
		ER IN BLOCK	
	SA = SUBASSEMBLY TEST LAB ET = EXPERIMENT TEST LAB	VL = VIBRAT	ATION LAB
J	ST = SYSTEM TEST LAB TL = TRANSMITTER LAB PL = P.S.E. LAB	EM = EMI/SCI CC ≈ CLIMAT HB = HIGH BI OP = OUT OF	REEN HOOM IC CHAMBER AY AREA
	•		V-23
	THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  THE SOLUTION  TH	FRACTURE NOTED ON TO THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE OF THE PER-CLOCKWISE SIDE	FRACTURE NOTED ON THE TAB  FRACTURE NOTED ON THE TAB  FRACTURE NOTED ON THE TAB  FRECOR - ADJMENT TO THE TAB  FRECORDINE SIDE OF THE  PAGE. OF THE  ANTION. OBJAIN MICROPHOTOS. RE  LATION. OBJAIN MICROPHOTOS. RE  LATION. OBJAIN MICROPHOTOS. RE  LATION. CONTINUE TEST.  LOCATION CODES (ENTER IN BLOCK ORIGINAL PAGE IS POOR)  TURING DESIGN  OPERATION  REPRODUCIBILITY OF THE  ORIGINAL PAGE IS POOR  CT - COMPONENT TEST LAB  ET - EXPERIMENT TEST LAB  ST - SYSTEM TEST LAB  ET - EXPERIMENT TEST LAB  ST - SYSTEM TEST LAB  TL - TRANSMITTER LAB  TL - TRANSMITTER LAB  TL - TRANSMITTER LAB  OF - OUT OF

GOV'T SOUNCE REPRESENTATIVE



	ma.	I	REV. PA
	TP23	74457	1.3
	PAGE .	16	07
)			

(24)

10.0 TEST DISCREPANCY REPORT LIST

		Entered By	Accept LAGEOS	DR		
4009	7.7 Z Axes	8-14-34		Doided 6		
				8-15		٠
				·		
					·	
					٠.	
						,
					·	
	•		·			
·						

Pandin
arospace Systems Division

	NO	REV. NO.		
	TP2374457	XII		
	PAGE OF			
)	DATE			

11.0	TEST	WITNESS	SIGNATURE	SHEET

TEST ITEM Lageos Phase B Test Article	
SERIAL NUMBER NA	
PART NUMBER NA	

THE ABOVE LISTED ITEM HAS BEEN TESTED AND WITNESSED IN ACCORDANCE WITH THE FOREGOING PROCEDURE.

ENVIRONMENTAL/QUALITY TEST CONDUCTOR

S-15-74

DATE

S-14-74

LAGEOS ENGINEERING REPRESENTATIVE

DATE